

Cooler Material Reliability Considerations for Bare Die Impingement Cooling in Package

Tiwei Wei

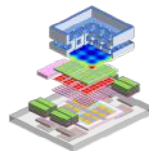
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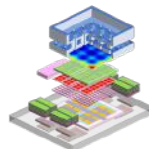


**HETEROGENEOUS
INTEGRATION ROADMAP**

Symposium on Reliability for Electronics and Photonics Packaging

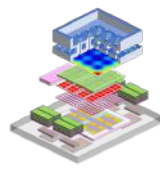
The challenge of high-density heterogeneous integration: getting the heat out, so devices can operate reliably with a long lifetime.

- The Thermal Chapter of the HI Roadmap looks out 5 to 10 years, anticipating the needed development of cooling technologies
- You can download chapters from the Roadmap (free) at eps.ieee.org/hir
- For more detailed reliability aspects of electronics/photonics packaging, consider attending the **Symposium on Reliability for Electronics and Photonics Packaging**, Nov. 16-17 (in-person and virtual):
attend.ieee.org/reppp

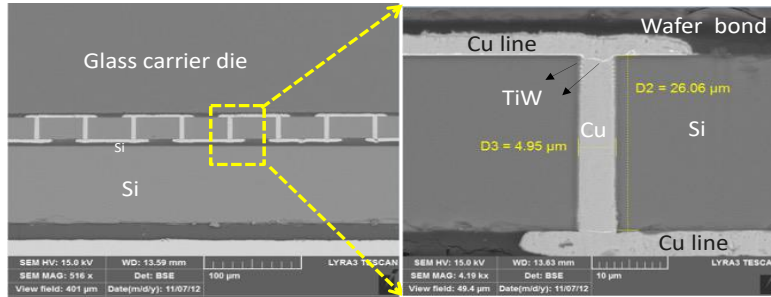


Semiconductor Packaging Laboratory
(All-in-one for Semiconductor Packaging, Heat transfer, and Assembly Lab)

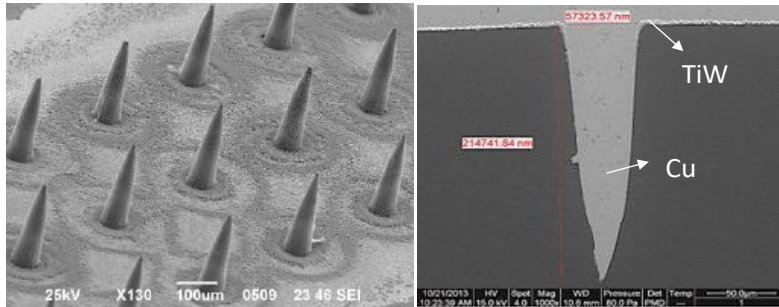
S-PACK Lab
(Advanced Packaging)



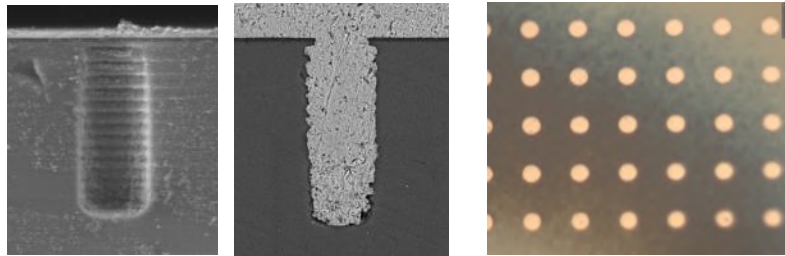
Topic 1: Materials, Processing, and Architecture Development for Semiconductor Packaging



Wei et al., IEEE EMAP, 2012: 1-5.

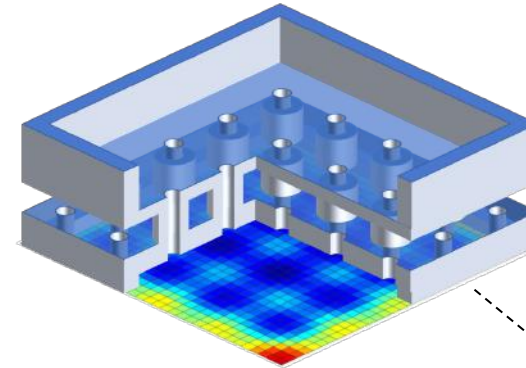


Wei, et al., IEEE EPTC 2014: 601-605.



3μm TSV from via etching and CMP

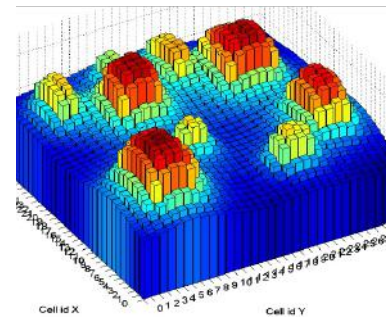
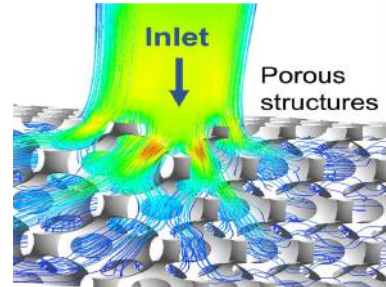
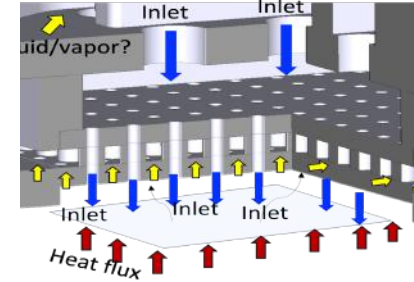
Topic 2: Chip and Package Level Electronic Cooling: Two-Phase Jet Cooling and Microchannel Cooling



Chip and Package Level Electronic Cooling: Jet Cooling and Microchannel Cooling

Surface Engineering Enhancement of Advanced Cooling Technology

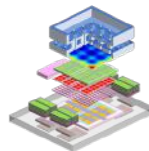
Thermal modeling analysis and management of advanced packaging



Key goal: Solving fabrication challenges in semiconductor packaging and assembly, and associated heat transfer problems

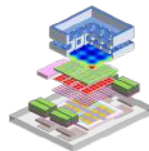
OUTLINE

- Background and introductions
- Material considerations and selections
- Exploring different cooler materials for reliability
 - Additive manufacturing polymer-based cooler
 - CTE modified polymer-based cooler
 - Glass-based cooler
 - Metal 3D-Printed Direct Liquid Jet-Impingement Cooling
 - Ceramic-based on cooler
- Other cooling reliabilities: clogging, corrosion...



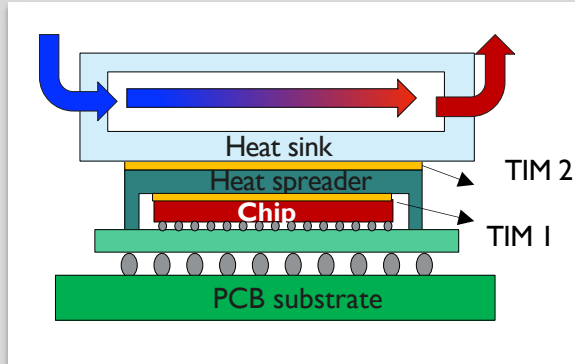
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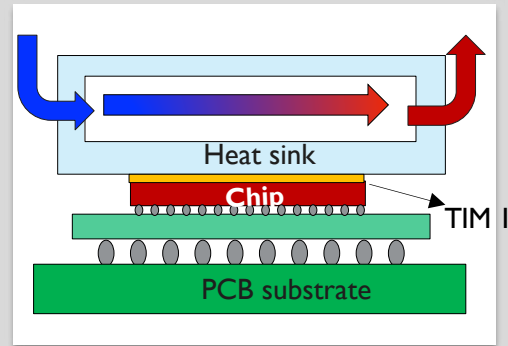


State of the art liquid cooling for high performance system

Liquid cooling with Thermal interface material:
TIM

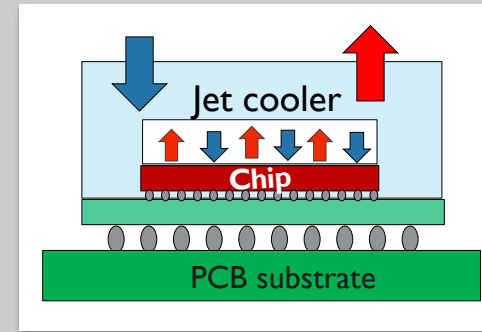


A: Liquid cooling + heat spreader (metal lid) with TIM 1 and TIM 2

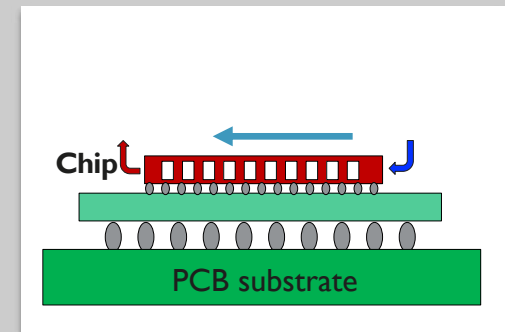


B: Directly attached liquid cold plate with TIM 1

Direct Liquid cooling on top of the chip
backside



C: Bare die backside jet cooling



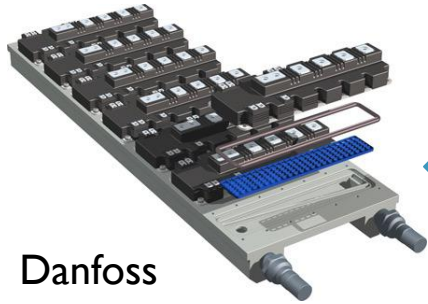
D: Embedded microchannel cooling inside the die

Direct liquid jet cooling on the chip can eliminate the thermal resistance of thermal interface material!

Bare die impingement cooling in package

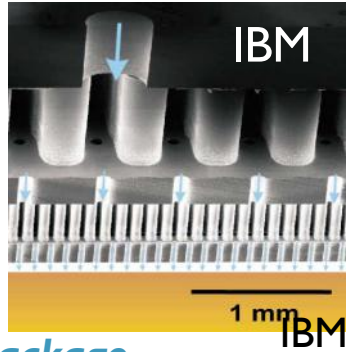
Existing technology options:

Module level cooling



Danfoss

Si processing techniques



IBM

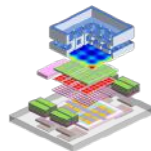
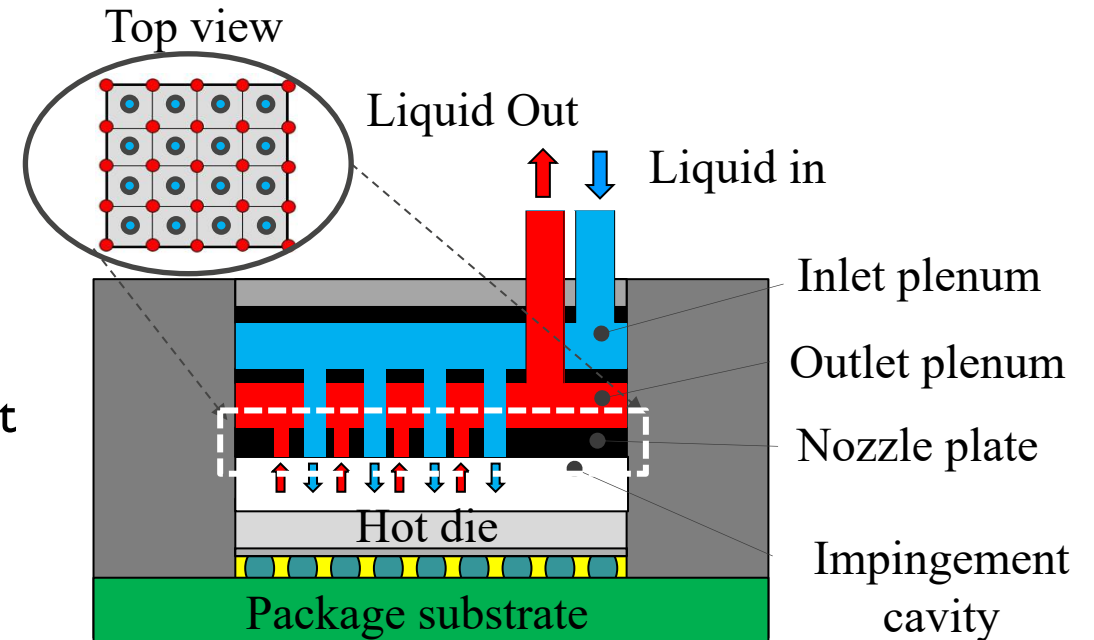
Bare die impingement in package

Advantages:

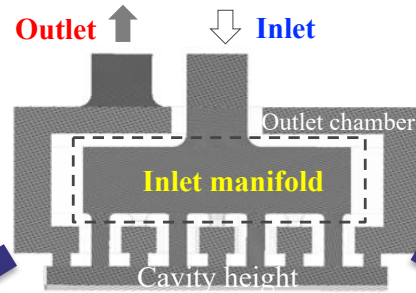
- Direct cooling → Eliminate TIM thermal resistance
- Parallel type cooling → Reduce temperature gradient
- Deliver high localized heat transfer rates → Hotspot targeted cooling
- Multiple jet array → Temperature uniformity

Our target:

- **Customizable** nozzle array to match chip power map
- **Low-cost** fabrication method: 3D printing
- Goal: one part solution - cooling integrated **in chip package**



Modeling methodologies for optimal cooler design

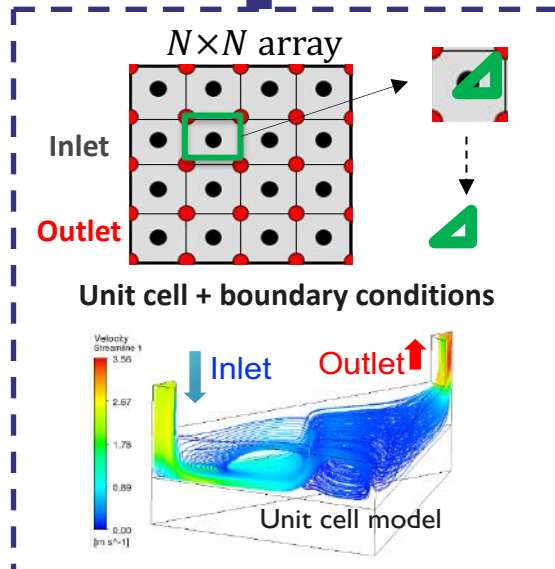


Objective: Understanding the thermal/fluidic behaviors using CFD modeling

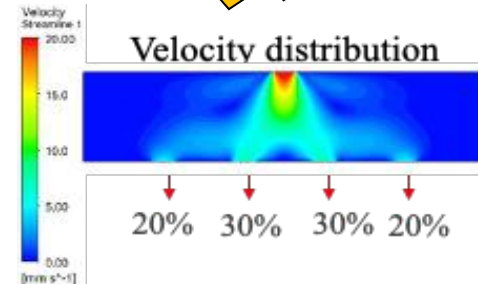
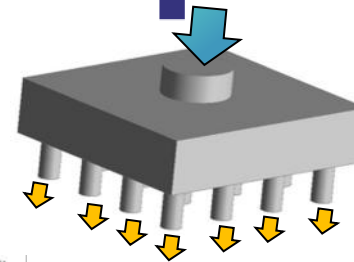
(1) Unit cell-level

(2) Manifold-level

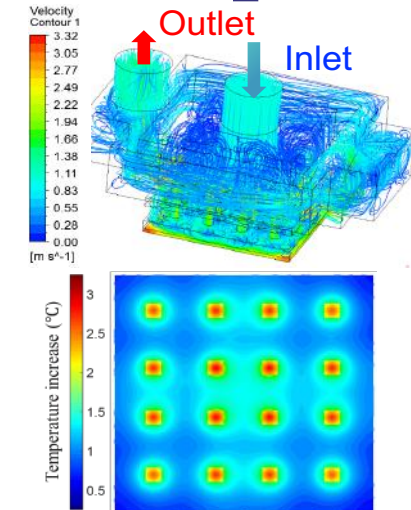
(3) Full scale cooler level



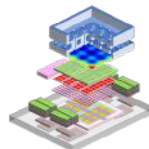
Used for extensive DOE for the nozzle pattern optimizations and dimensionless analysis



Manifold geometry optimization for better flow uniformity and lower pressure drop



Provide system level pressure and temperature distribution information for cooler design

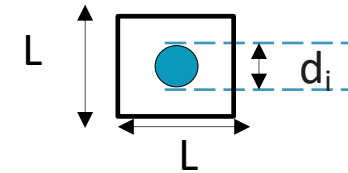
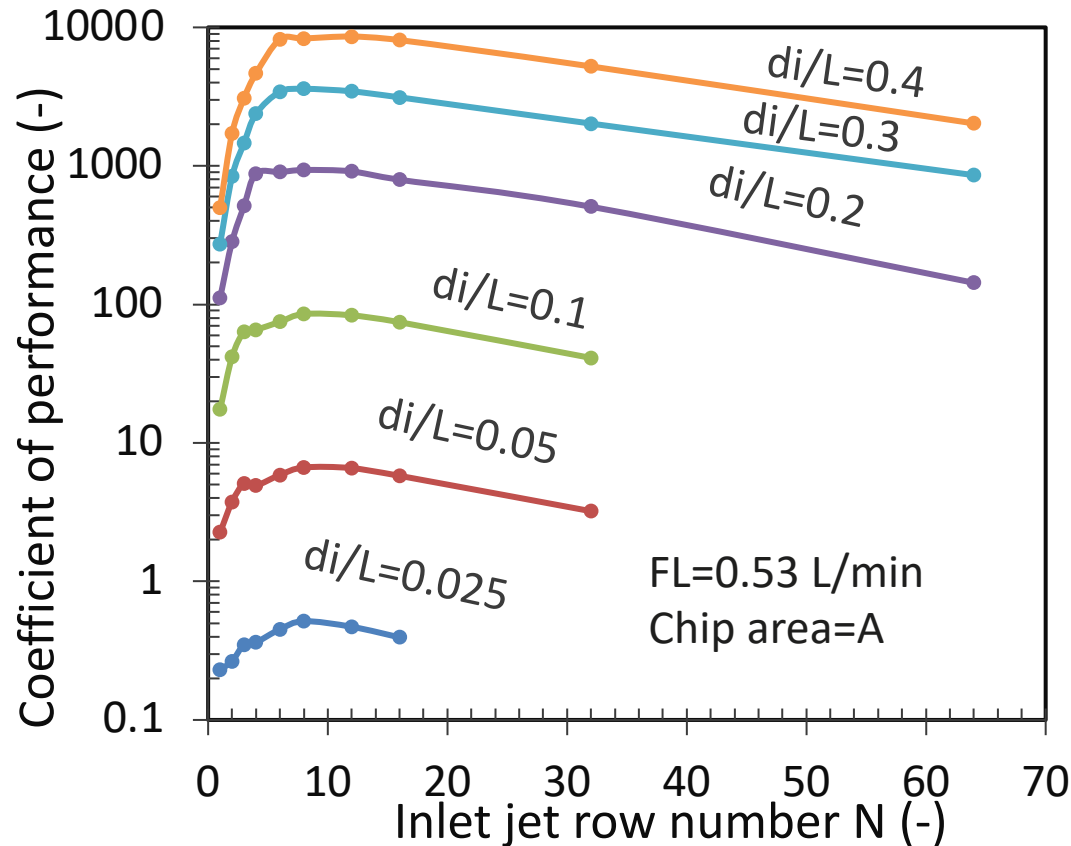


Unit Cell model modeling → Larger diameter

Wei et al., Appl. Therm. Eng., 2020: 115767.

Coefficient of performance:

$$COP = \frac{\text{Cooling Power}}{\text{Required pump power}} = \frac{\text{Max allowed temp increase}/R_{th}}{\text{Required pump power}}$$



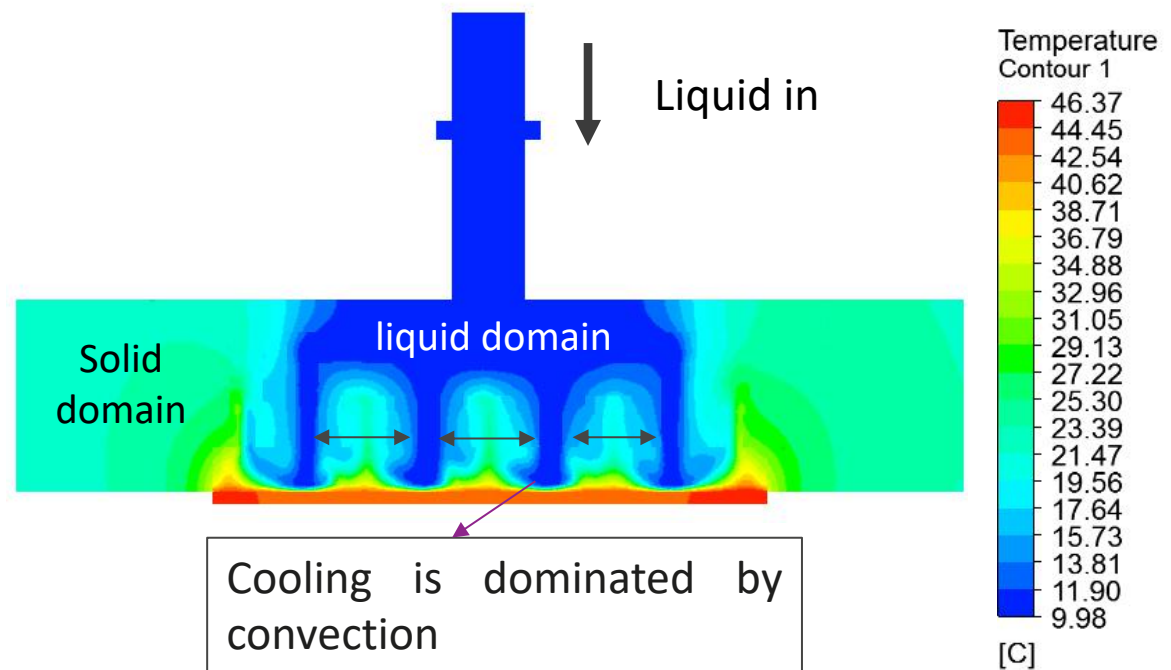
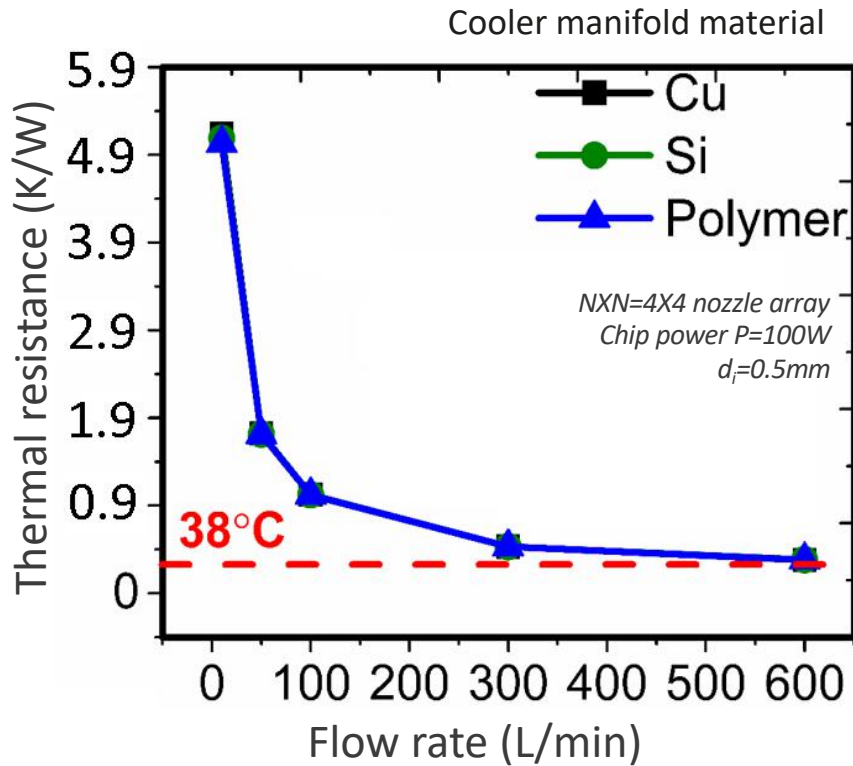
d_i/L : inlet diameter ratio

$N \times N$: total inlet jet number = $A/(L \cdot L)$

For a constant flow rate:

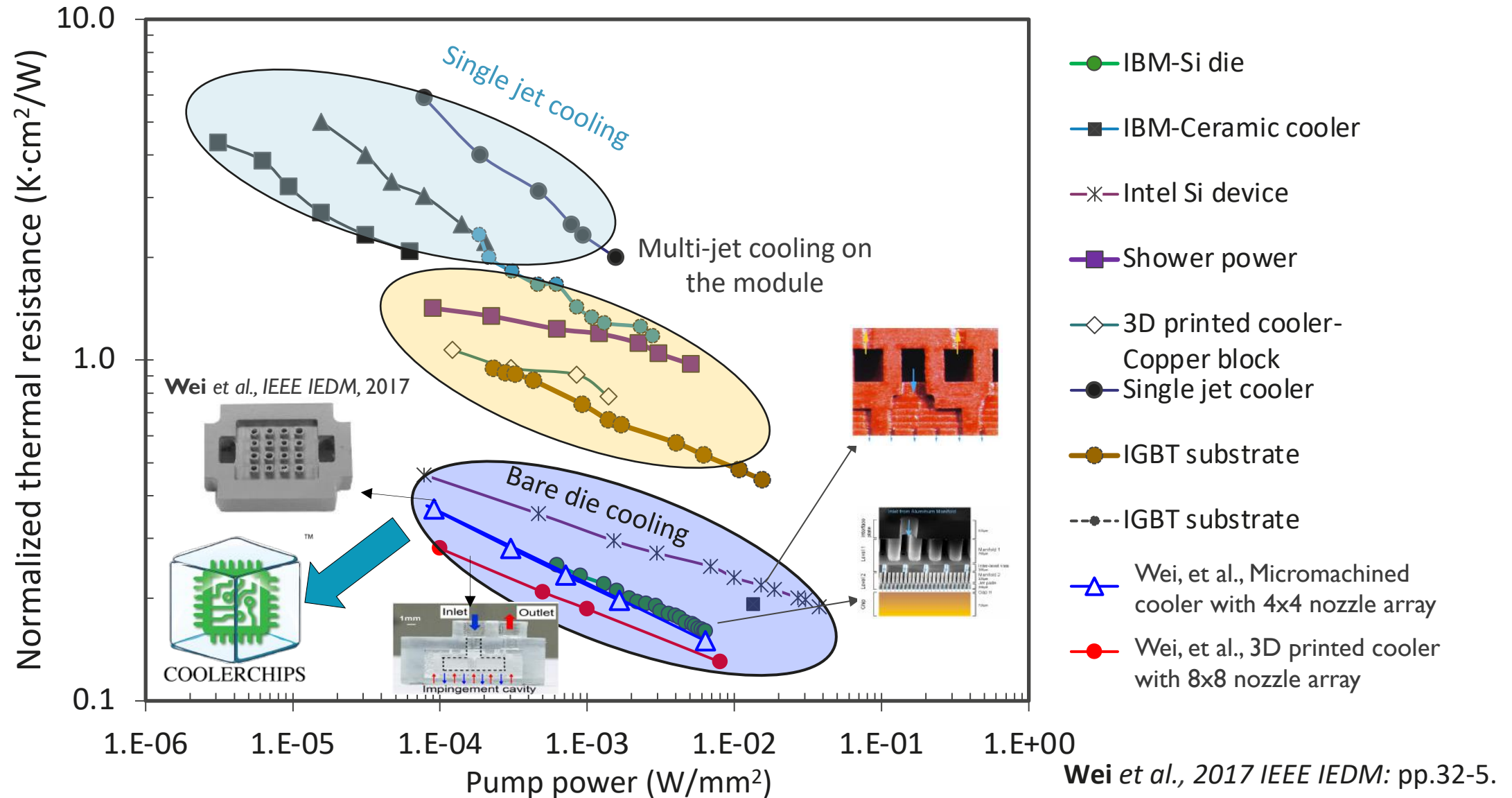
- Higher inlet diameter ratio d_i/L has larger COP
- Inlet nozzle number N between $N=6$ and $N=8$ shows optimal COP
- Making the required diameters compatible with **additive manufacturing** fabrication methods

Full cooler level modeling → cooler material



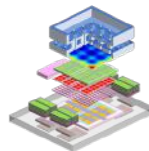
- Negligible impact of cooler material thermal properties
- Enables low-cost fabrication technologies → polymer-based jet cooler

Bare die microjet cooling in packaging benchmarking



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Cooler reliability considerations

During cooler assembly

- Cooler assembly options:
 1. First assemble package to board, then mount cooler on package (glue, clamping, ...) → No harsh temperature requirement for cooler material
 2. First mount and seal cooler on package, then assemble package with cooler on PCB → Cooler assembly needs to survive reflow temperature (250°C)
- Property: Heat deflection temperature *HDT*
*the temperature at which a plastic deforms under a specified load (e.g. 0.45 MPa)

Ideal material: $HDT > 250^{\circ}\text{C}$

During cooler operation

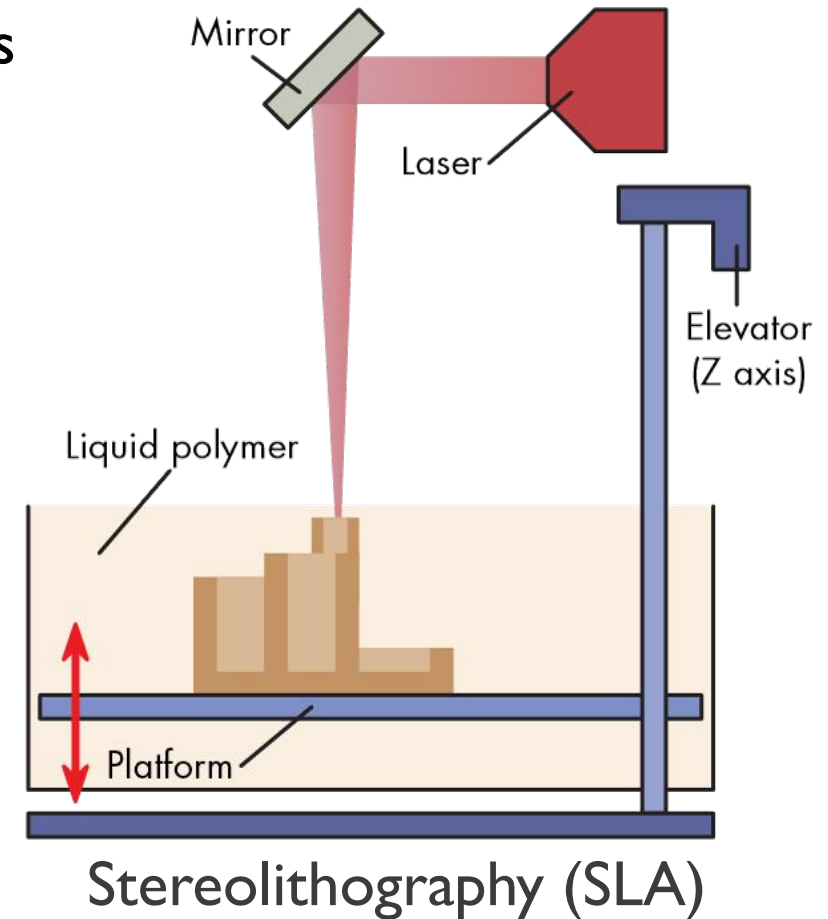
- High reliability required for thermal cycling
- Property: Coefficient of thermal expansion *CTE*

Ideal material: CTE matched with package substrate

Polymer based 3D printing (1)

Stereolithography (SLA) used for fabrication of demonstrators

- UV exposure of **liquid resin** (acrylic based thermosetting polymer)
- Material: Somos Watershed UX III 22 (DSM) ([link](#))
- Typical properties do not meet requirements
 - CTE: 100 – 150 ppm/°C
 - HDT: 45 – 60°C
- Recent material developed:
Formlabs FLHTAM01 High Temp Resin ([link](#))
 - Interesting properties:
 - HDT: **289°C**
 - Other properties similar to Watershed material

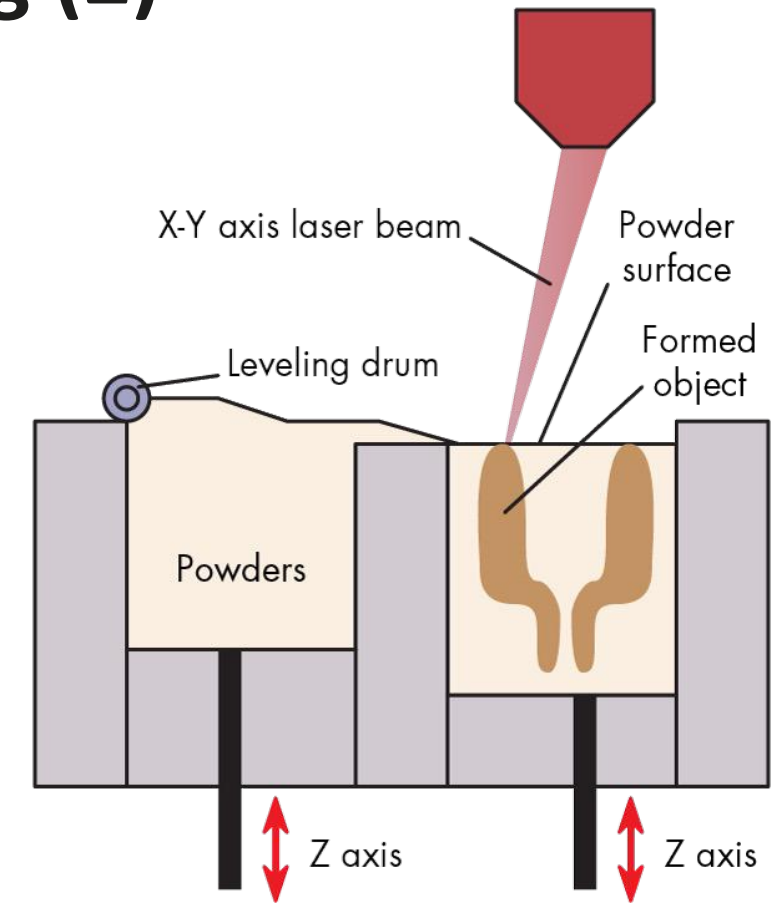


Source: What's the Difference Between Stereolithography and Selective Laser Sintering?

Polymer based 3D printing (2)

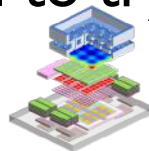
Selective laser sintering (SLS) can be alternative:

- Laser sintering of **polymer powder** (thermoplastic polyamide)
- Based on Nylon / polyamide polymers
 - Typical HDT ~ 150°C
 - Improvements: Aluminum filled PA (Alumide): HDT 169°C, Glass filled PA: HDT 176°C
- Previously not considered due to water absorption
- Recent new material development: Solvay AV-755 ([link](#))
 - PAEK (polyaryletherketone)
 - HDT **278°C**
 - Very low water absorption of 0.01%
- Typical challenge for SLS: surface finish
- Interesting material to try out for demonstrator



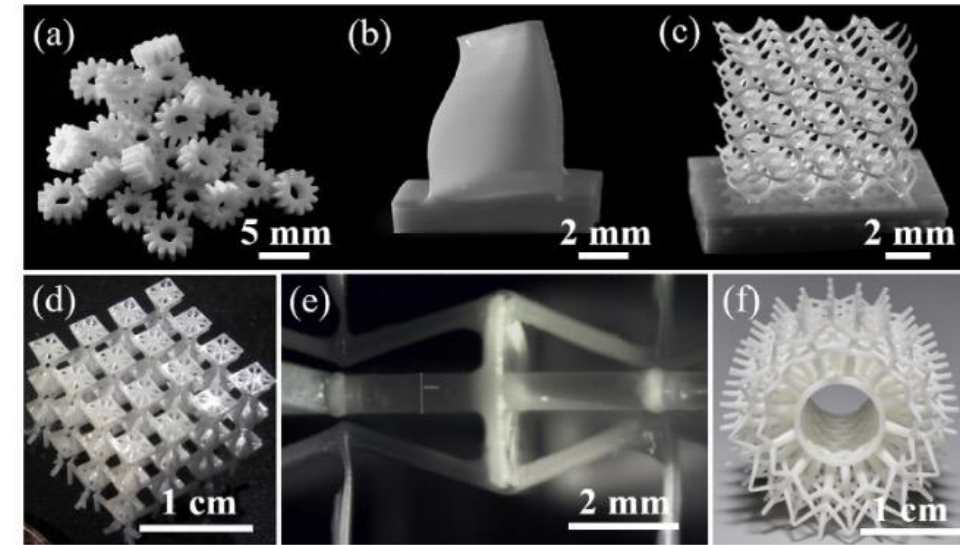
Selective laser sintering (SLS)

Source: What's the Difference Between Stereolithography and Selective Laser Sintering?



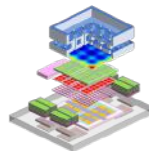
Other materials considered for 3D printing

- **Ceramics** can be used for high precision fabrication with good surface finish:
 - Slurry based photo-polymerization (*SLA*, *DLP*, *TPP*) with SiO_2 , Al_2O_3 , ZrO_2 or SiC show great potential for small scale fabrication with controllable feature size and surface finish
 - Demonstration of 3D microstructures with sub- μm resolution
 - Power based fusion (*SLS*, *SLM*) still under development
 - Very high temperature resistance: $+1400^\circ\text{C}$
 - Interesting option to explore with printing partner
 - More expensive than polymer fabrication
- Additive manufacturing with **metals** also allows very high temperature resistance:
 - Ti: 1660°C
 - Al: 1250°C
 - Stainless steel: 1400°C



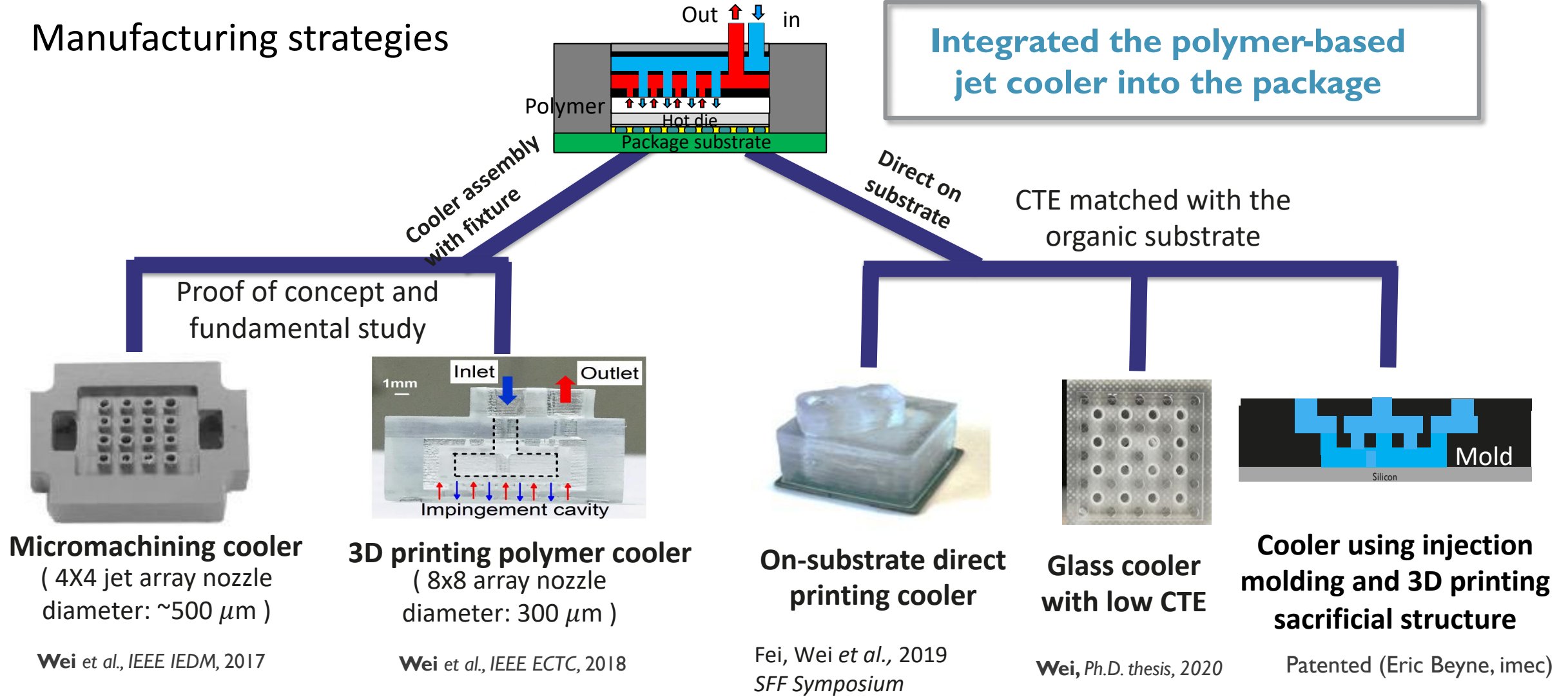
Source: ZhangweiChen, et al., 3D printing of ceramics: A review, Volume 39, Issue 4, April 2019, Pages 661-687

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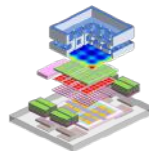
Previous work: bare die impingement in package

Manufacturing strategies



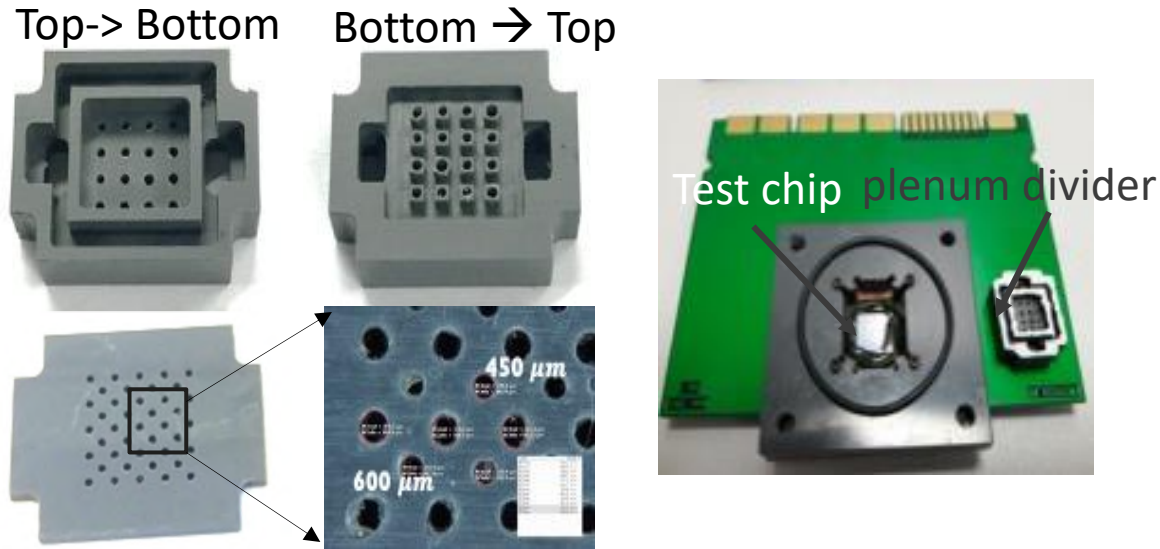
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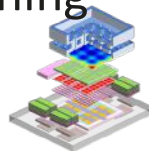
Novel 3D-shaped polymer multi-jet impingement cooler

Wei et al., 2017 IEEE IEDM: pp.32-5.

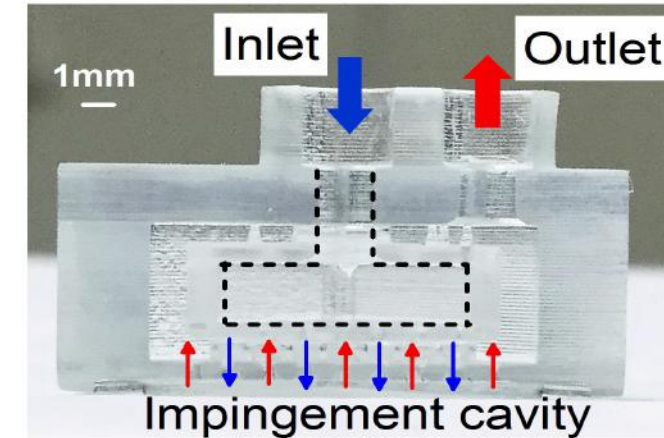
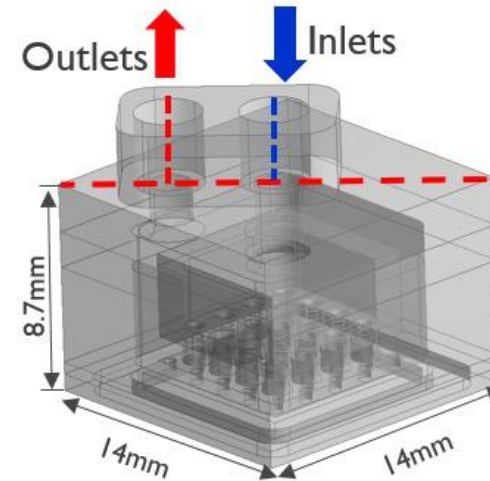


First demonstration of a low-cost polymer-based impingement jet cooler, reported in IEDM 2017

- 4×4 inlet jet array
- 5×5 outlet jet array
- 450 μm inlet nozzles diameter
- Mechanical machining



Wei et al., IEEE Trans. Compon. Packag. Manuf. Technol., 2019 9(9): 1815-1824.



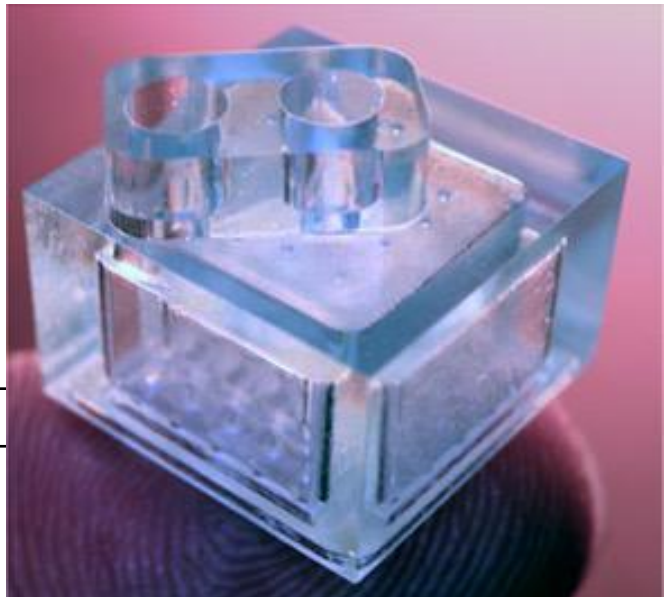
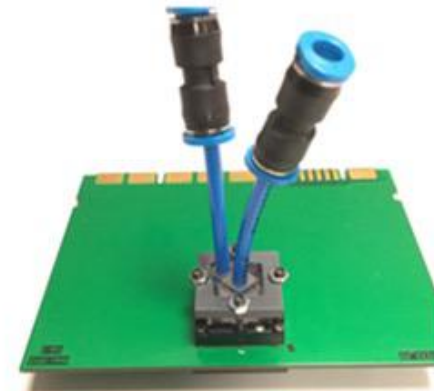
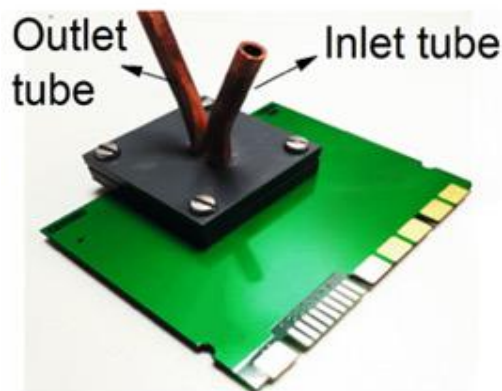
Advantages:

- Small form factor
- More **flexible** and **customizable** design
- **Finer resolution** of the internal structures

Challenges:

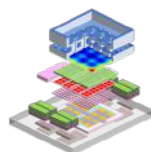
- Excess liquid resin removal
- Material compatibility with coolant
- Structural integrity → bridging of cavities

3D printed impingement jet cooling: package level size

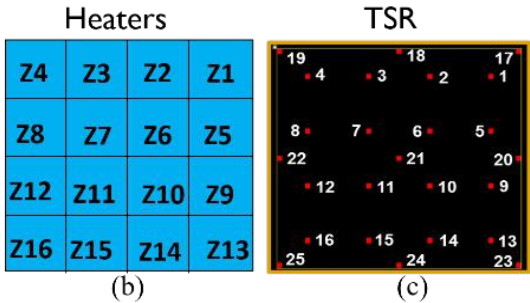
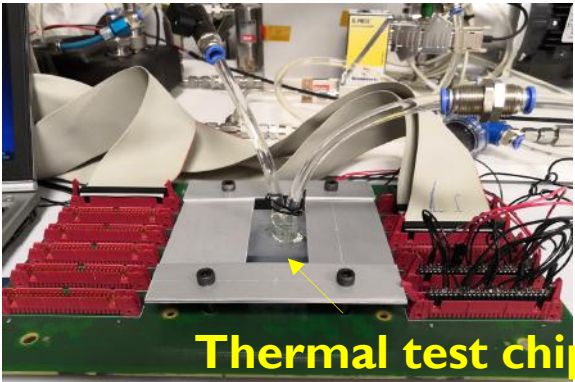


Geometry		Micromachined cooler	3D printed Cooler
Nozzle array	N	4×4	4×4
Inlet chamber height		3 mm	2.5 mm
Inlet diameter	d_i	0.45 mm/0.65mm	0.57 mm
Outlet diameter	d_o	0.6 mm	0.57 mm
Cavity height	H	0.6 mm	0.6 mm
Nozzle plate thickness	t	1 mm	0.55 mm
Cooler size	x,y,z	$46 \times 46 \times 13 \text{ (mm}^3\text{)}$	$18 \times 18 \times 8.7 \text{ (mm}^3\text{)}$

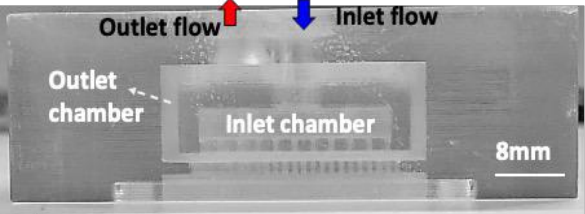
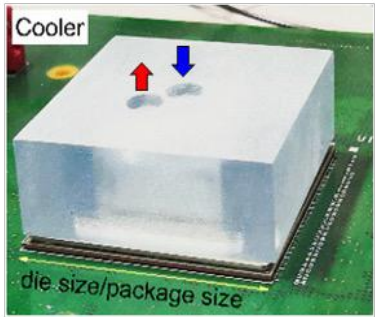
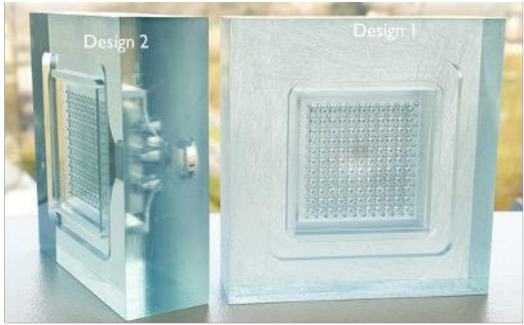
6.5X area reduction



Bare die impingement in high-power, large size chip package



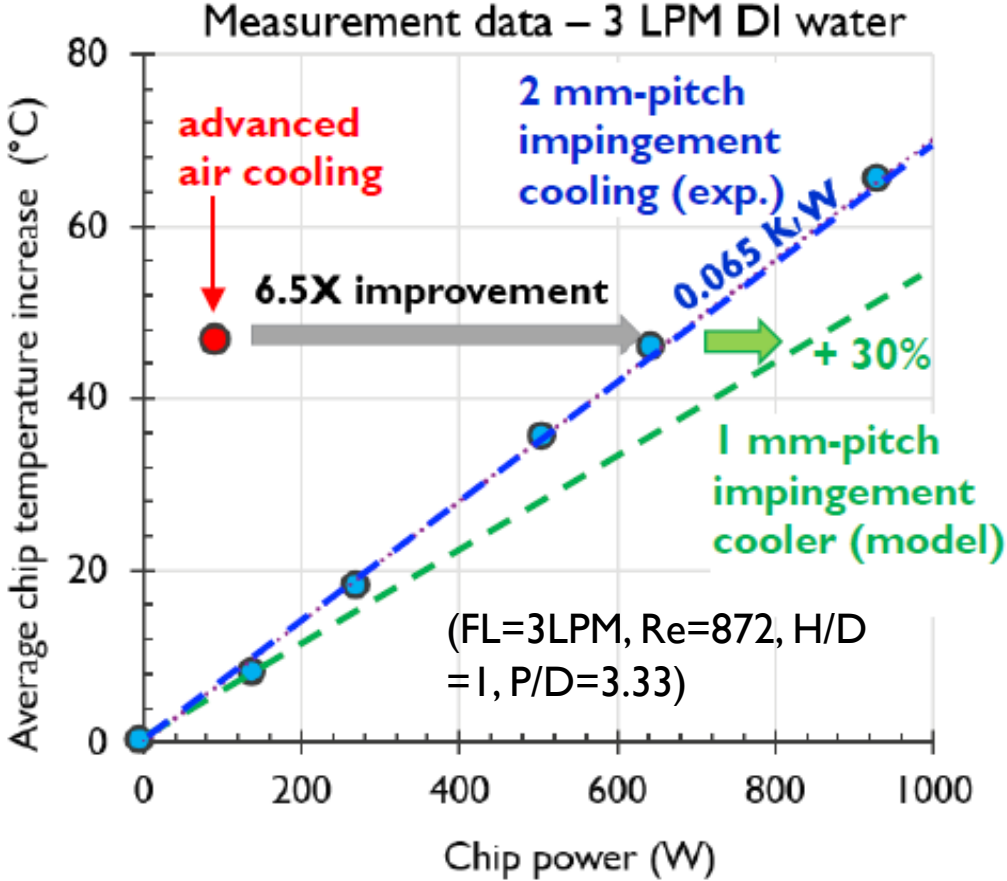
(b) 23×23 mm² test vehicle



Design 1 with nozzle array below coolant entrance connection



Design 2 with additional distribution layer to improve flow uniformity over chip surface



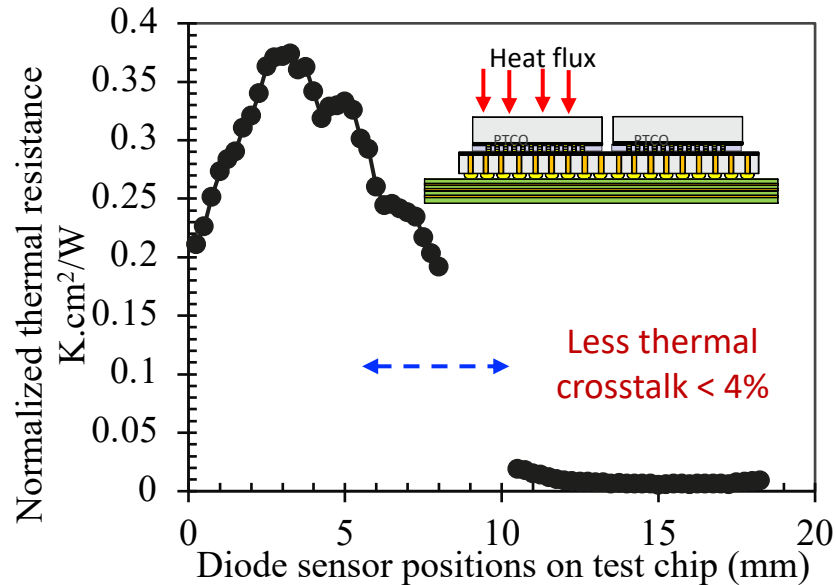
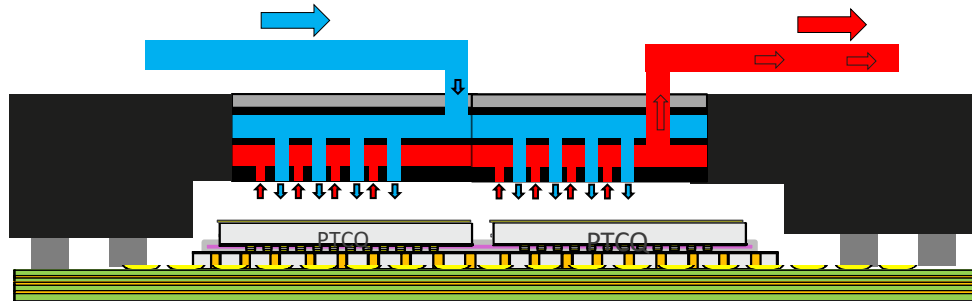
High power measurement with 1kW for 2mm inlet nozzle pitch, corresponding to a chip power density of 175 W/cm² → The average thermal resistance of the cooling with 3 LPM is 0.065 K/W.

Wei et al., IEEE Trans. Compon. Packag. Manuf. Technol, 2021: 415-425.



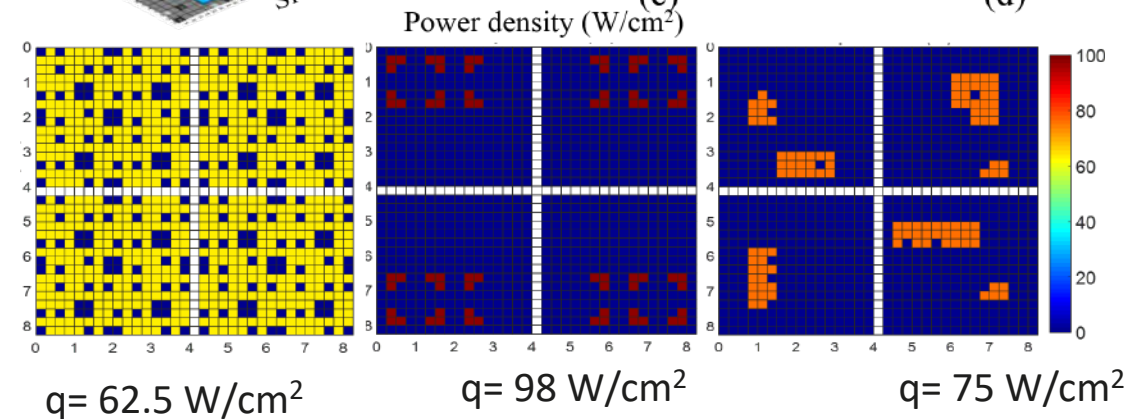
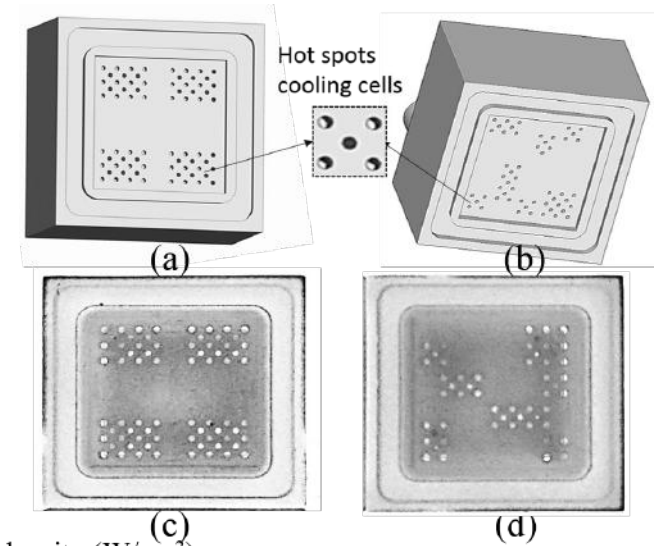
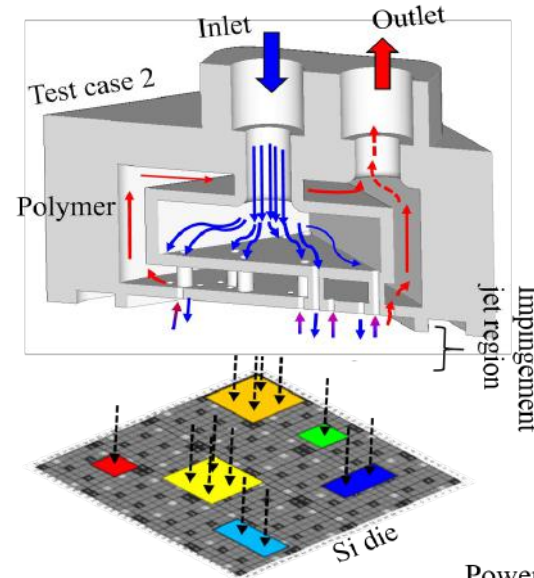
3D printing cooling for different packaging designs

2.5D interposer packaging

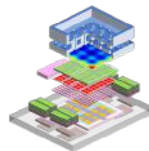


Wei et al., Appl. Therm. Eng., 2020, 164, 114535.

Hotspots targeted cooling

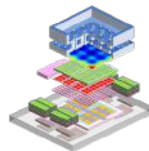


Wei et al., IEEE Trans. Compon. Packag. Manuf. Technol, 2020: 577-589.

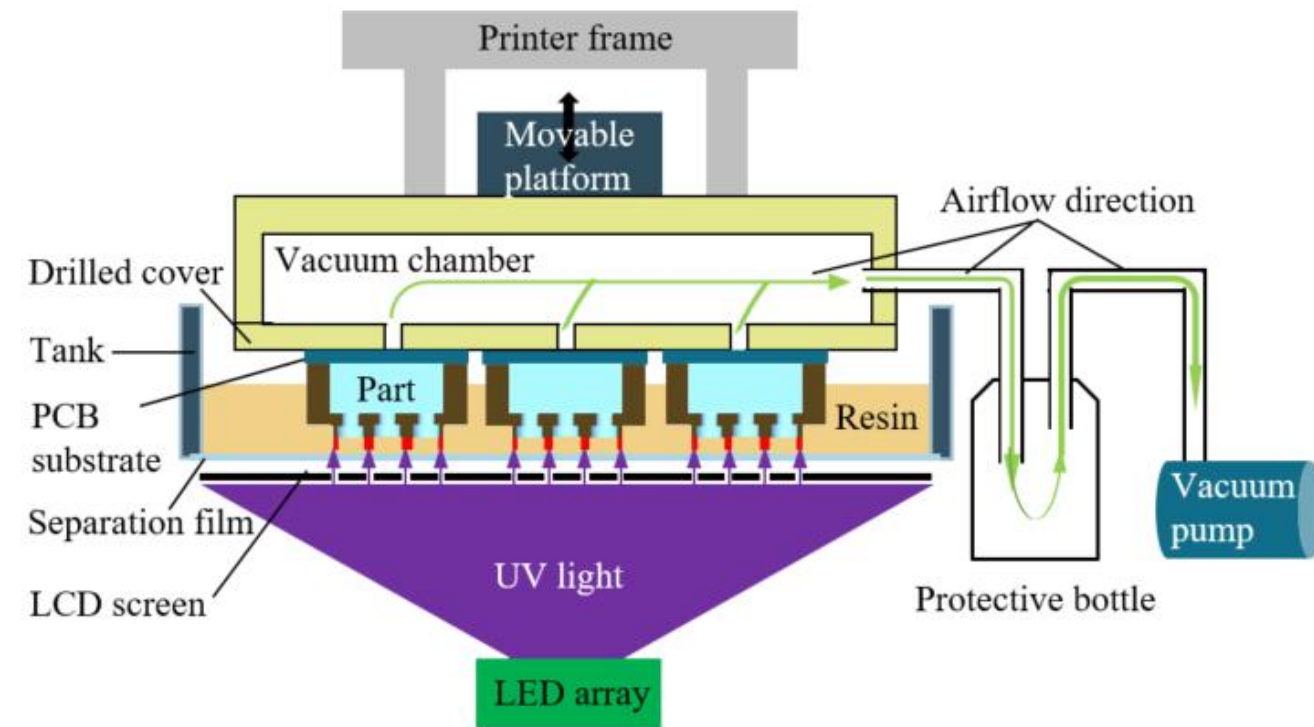


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Additive manufacturing on printed circuit board (PCB)

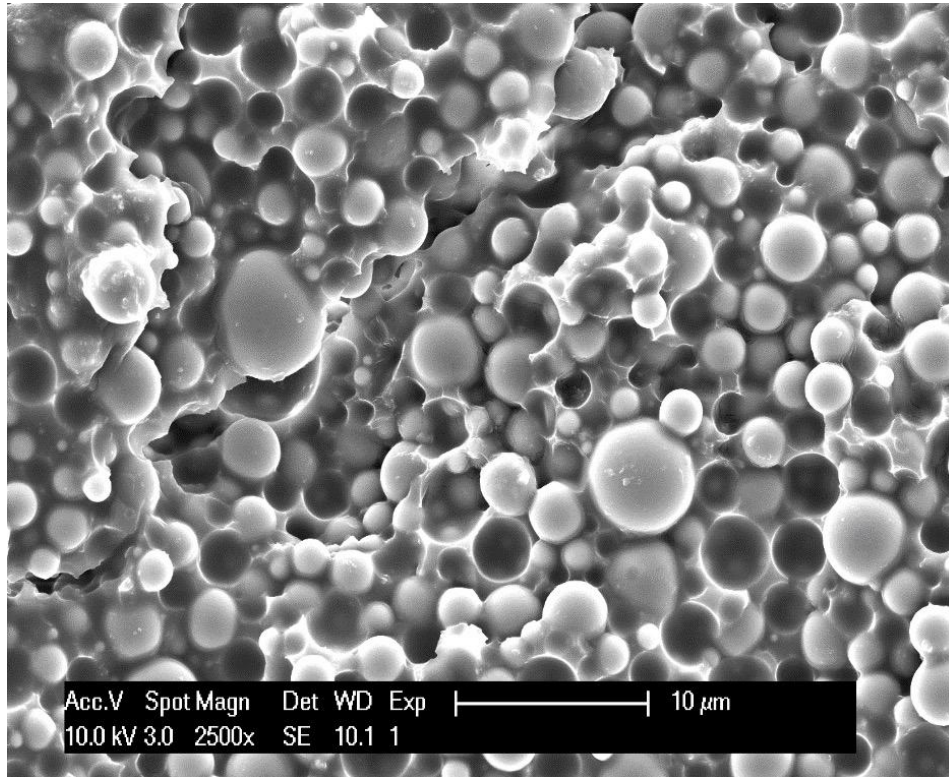


The bottom-up LCD-based stereolithography machine with a vacuum suction system (includes the vacuum chamber, the protective bottle and the pump)

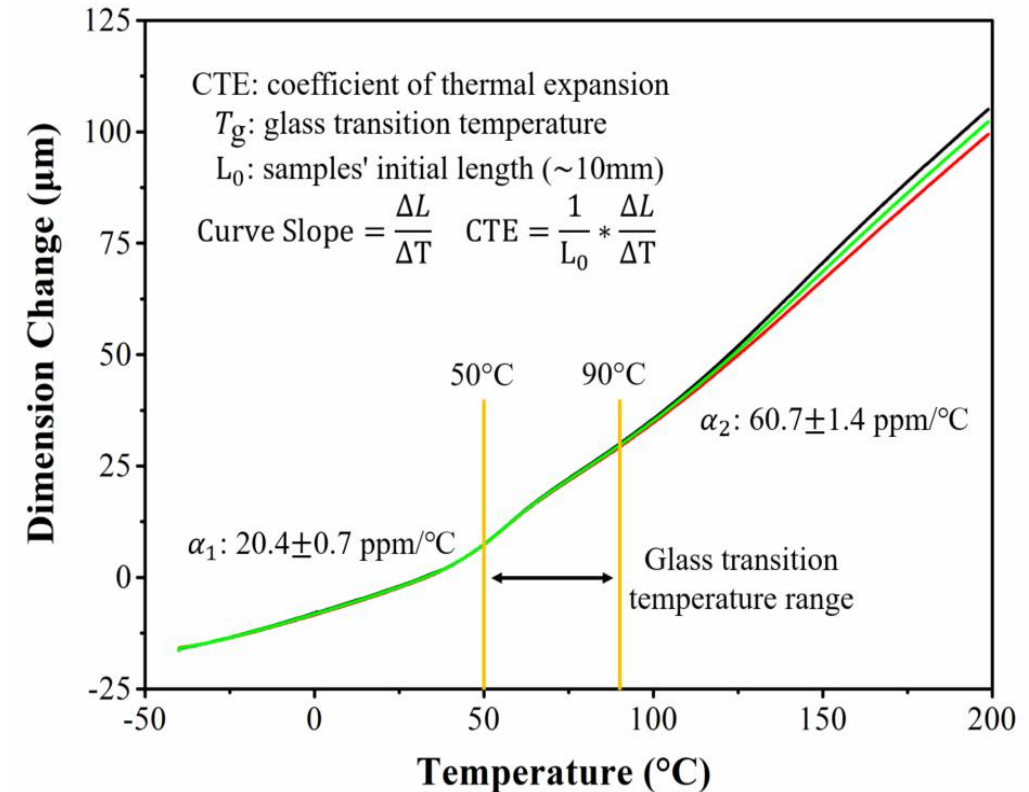
Fei, Wei *et al.*, 2019 SFF Symposium

- Need for **lower CTE polymers** due to current large mismatch with laminate CTE
- Collaboration with KU Leuven to develop the low CTE materials
- Trials with materials with lower CTE
 - **Silica and ceramic fillers** added to lower CTE
 - Limited filler concentration to keep material printable
- **Stereo-DIC technique** was used to measure the CTE of four composite materials for 3D printing of impingement cooler.

CTE modified polymer cooler with resin-silica composite



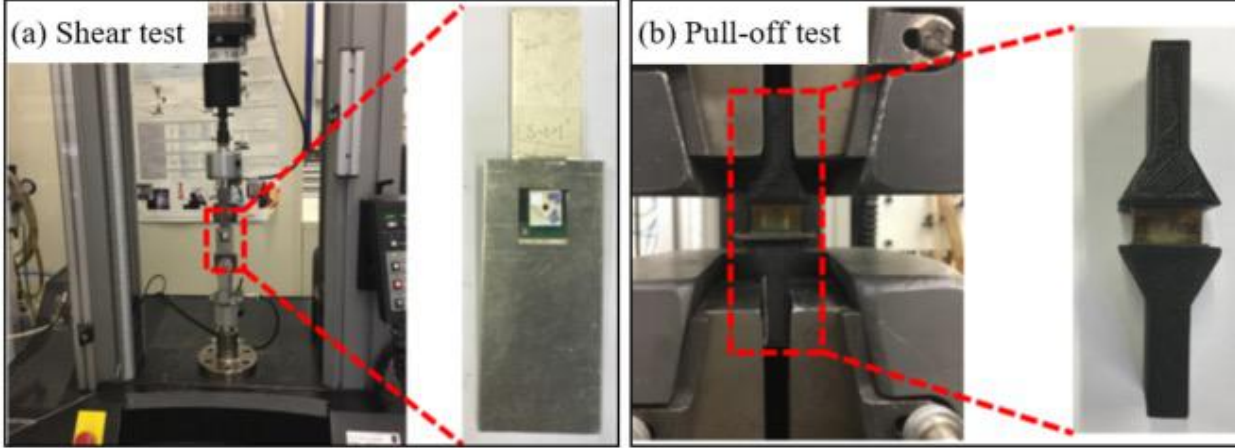
The microstructure of resin-silica composite printed at 25°C



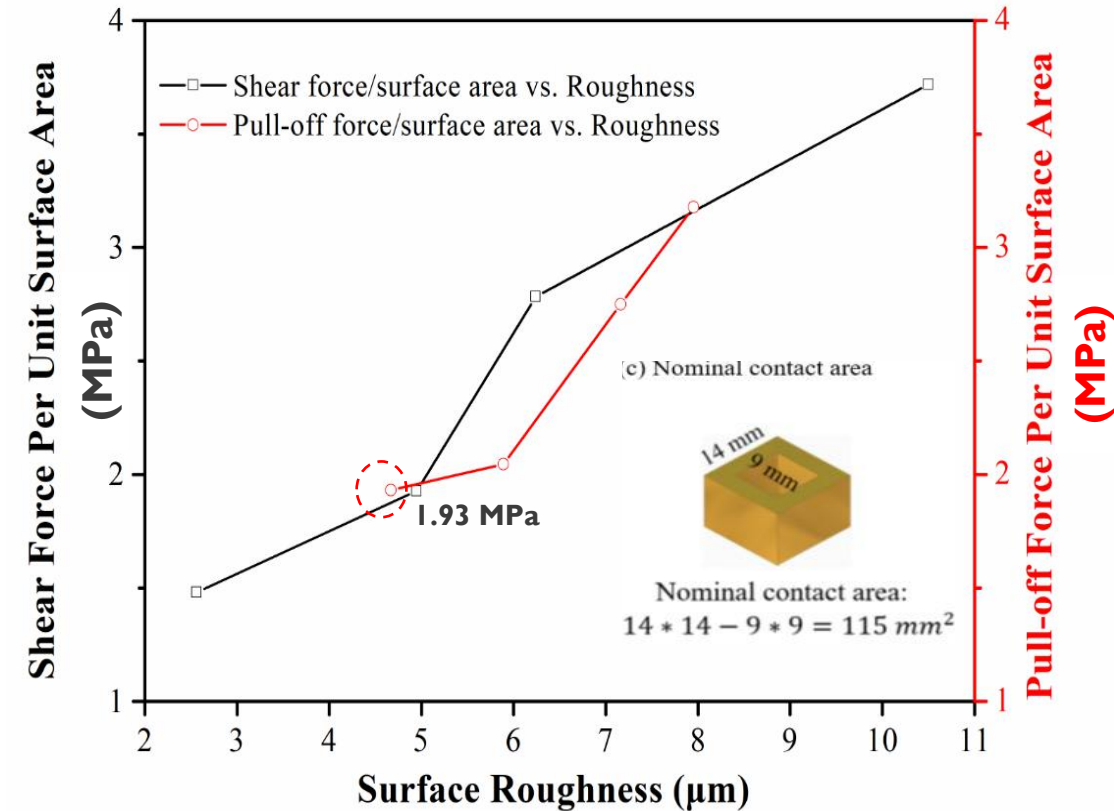
Dimensional change with temperature of 3 composite samples (Manufactured under the same conditions with the SEM samples)

The results show that α_1 is close to the CTE of commercial PCB, indicating the part can bond well on the PCB when the IC runs at a temperature below 90°C.

Adhesion properties measurements of resin-silica composite



Fei, Wei et al., 2019 SFF Symposium

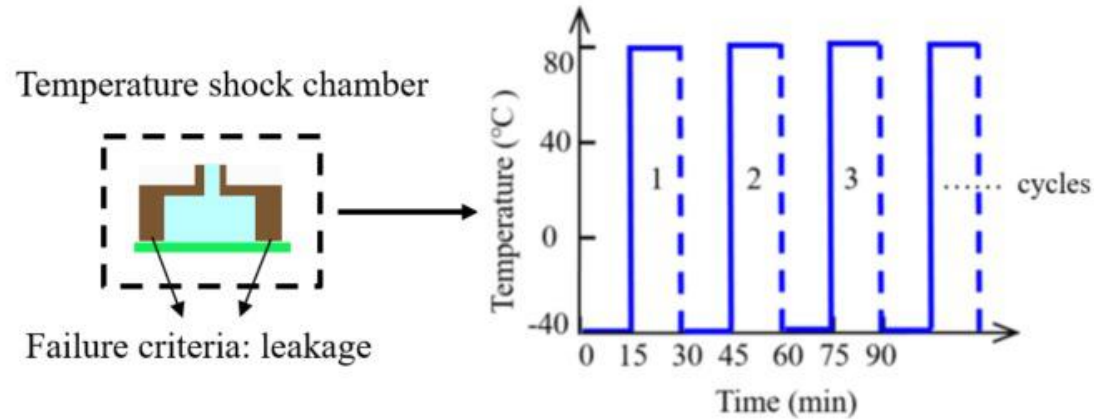


The influence of surface roughness on adhesion forces.

- Adhesion properties between different part/PCB substrate showed the adhesion on the part-PCB interface depends on their surface interactions.
- The larger the interface roughness, the greater the interaction forces on the contact surface.
- All the pull-off test and pressure test prove the bonding force between part-PCB is strong enough to keep them as an integrity system.

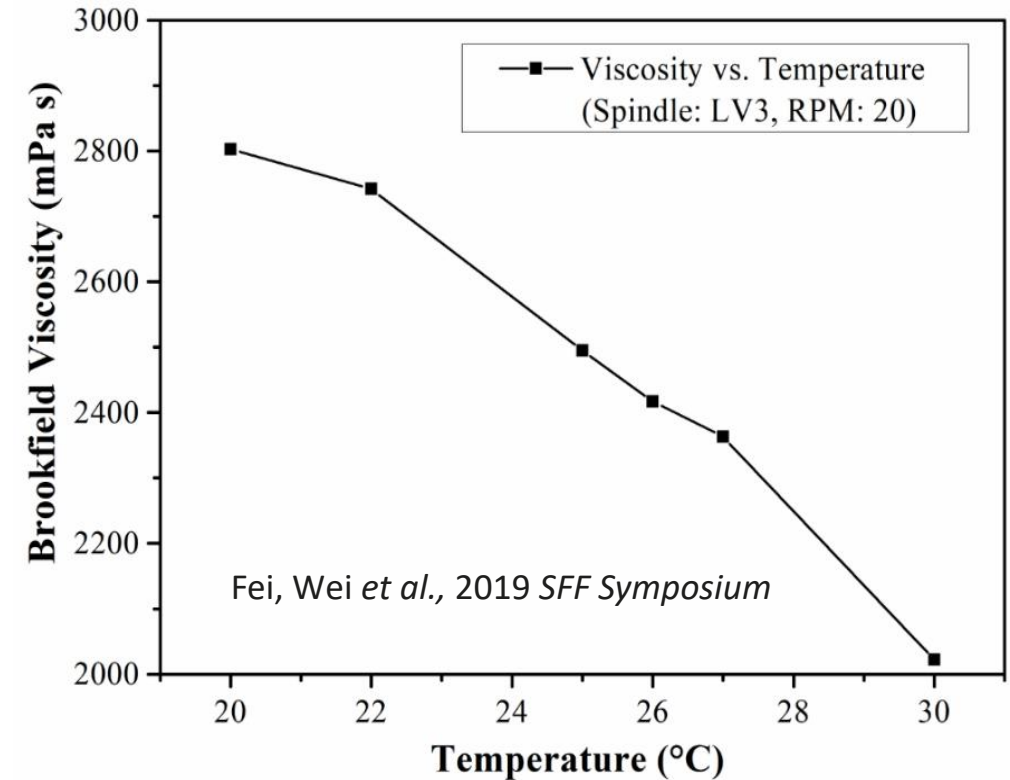
Suspension viscosity and particle dispersion of resin-silica composite

Fei, Wei *et al.*, 2019 SFF Symposium



The thermal shock test

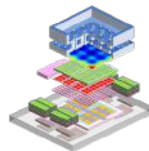
- Regarding the printing material, the silica-resin suspension containing 60 vol.% silica is uniformly enough to ensure the flowability during printing, at the same time, it has a low CTE which is close to that of the PCB material.
- The thermal cycling test indicated the tailored part owned good CTE compatibility with the PCB substrate.



Variation of the viscosity of silica-resin suspensions with temperature

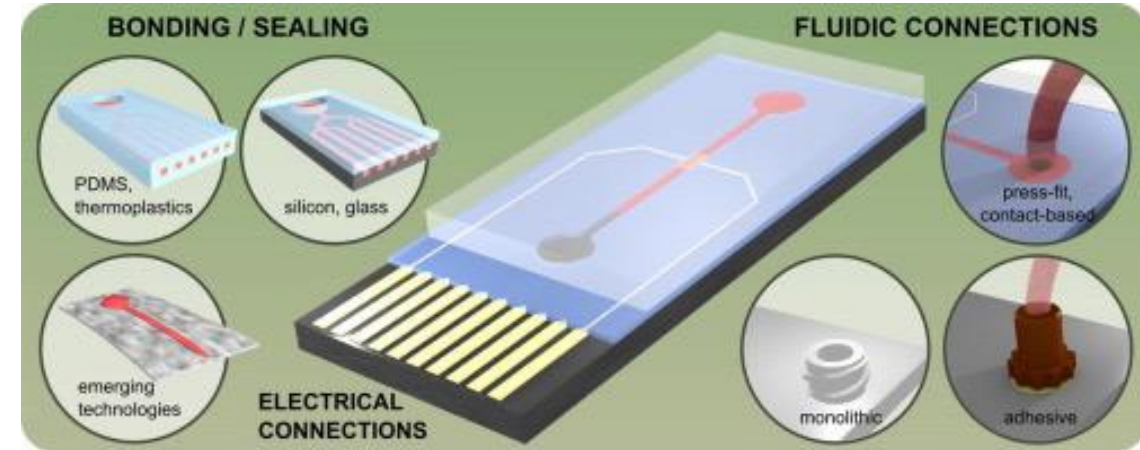
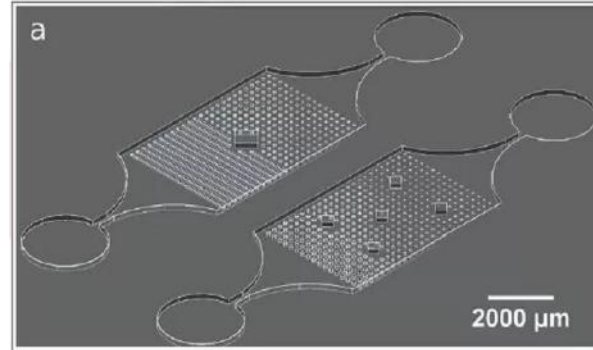
OUTLINE

- Background and introductions
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 - CTE modified polymer-based cooler
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 - Metal 3D-Printed Direct Liquid Jet-Impingement Cooling
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- Other cooling reliabilities: clogging, corrosion...



Alternative fabrication: Glass cooler

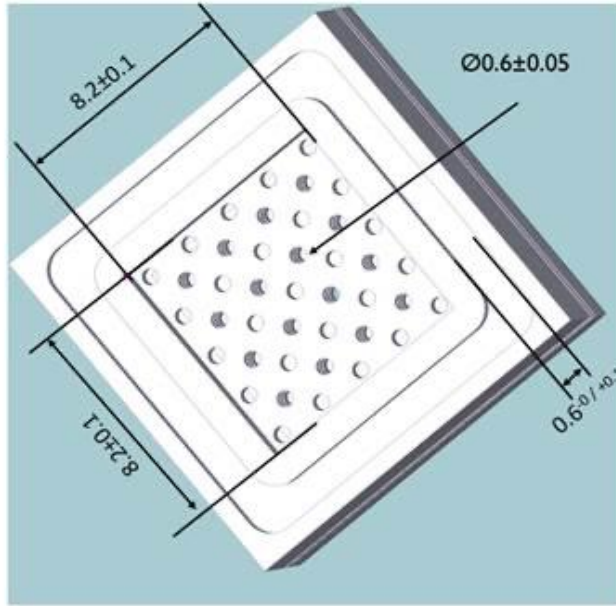
Fabrication of microstructures in glass



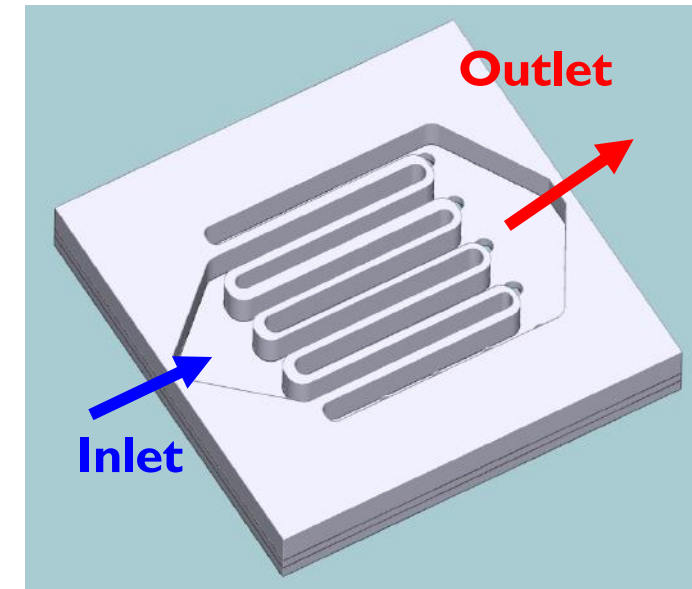
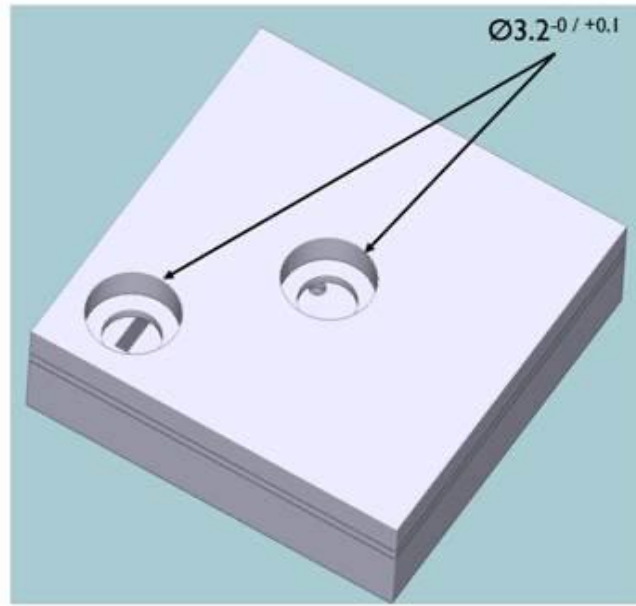
Yuksel Temiz, Robert D. Lovchik, Govind V. Kaigala, Emmanuel Delamarche, Lab-on-a-chip devices: How to close and plug the lab?, Microelectronic Engineering, Volume 132, 2015, Pages 156-175,

- Recent developments in glass fabrication enable internal microstructures
- Interesting material properties for our cooler (material: fused silica) :
 - CTE 0.5 ppm/°C → more compatible with Si and substrate than polymer
 - High temperature resistance
- Explore feasibility for glass cooler → adapt cooler design for glass microfabrication design rules

Design considerations: Glass cooler



Design 1



Design 2

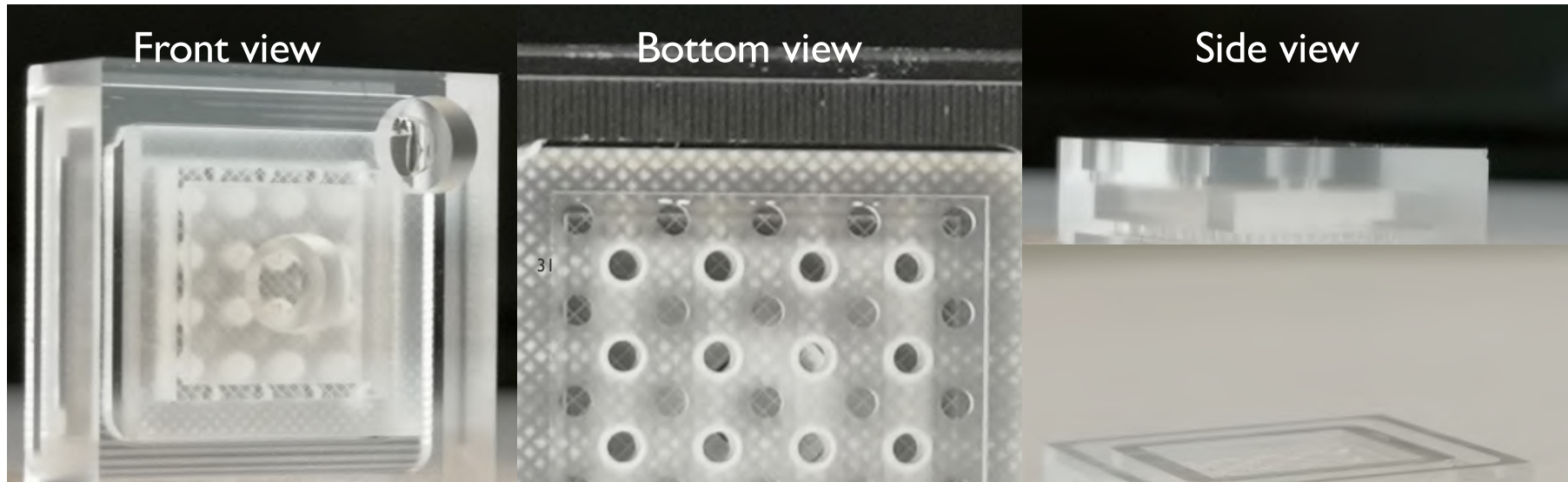
- 2 fabrication options:
 1. Monolithic structure
 2. Welding bonding
- Designs for both options finished
- Fabrication ongoing

Manufacturability

Resolution	$< 1 \mu\text{m}$
Surface roughness	$R_a < 100\text{na}$
Aspect ratio	$> 1:500$
Glass-to-glass seal withstands	100 bar

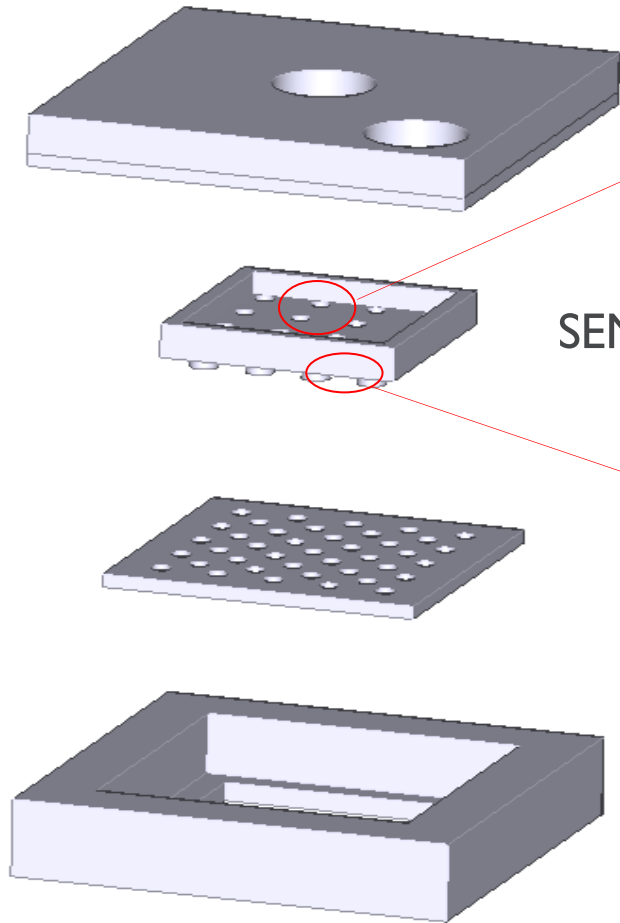
Demonstration of the Glass cooler

- Glass has interesting material properties:
 - Lower CTE than printed polymers → more compatible with Si and package
 - High temperature resistance
- Subtractive manufacturing technique used to create complex internal structures:
 - Focused laser beam locally modifies the density inside the glass
 - Cavities created by additional chemical etching
- Demonstrated for cooler geometry: 4x4 nozzle array design

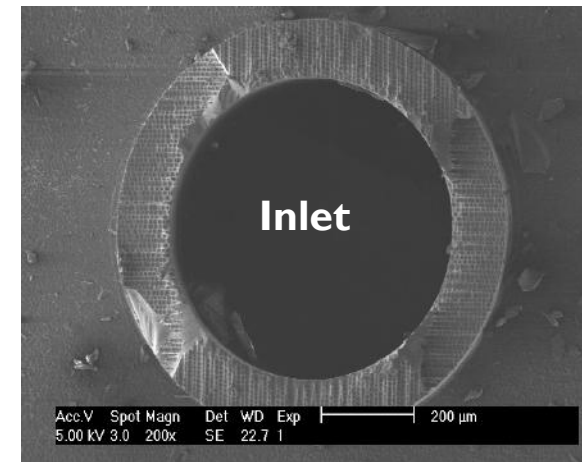
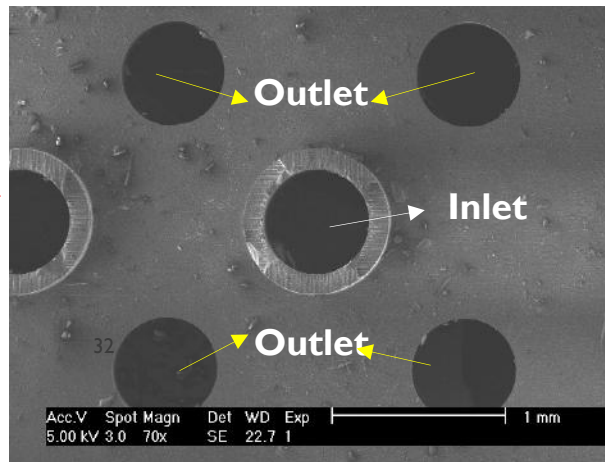
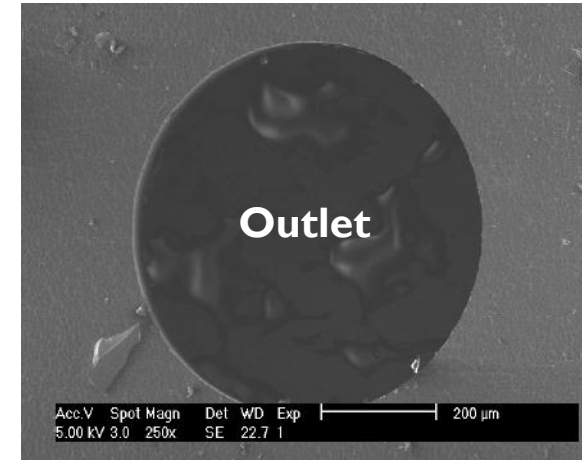
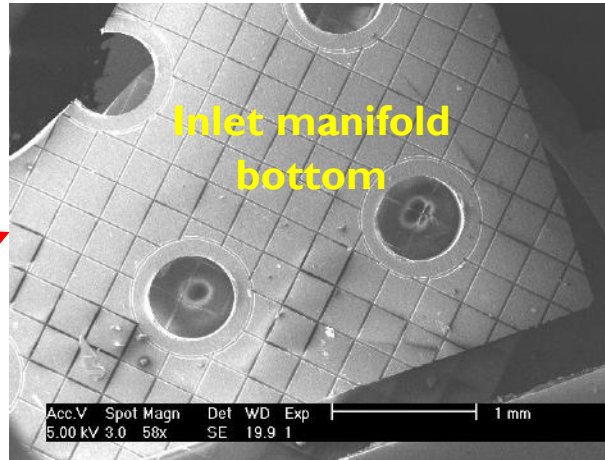


Demonstration of the Glass cooler

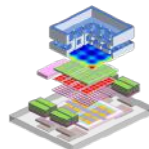
Wei, Ph.D. thesis, 2020



SEM images



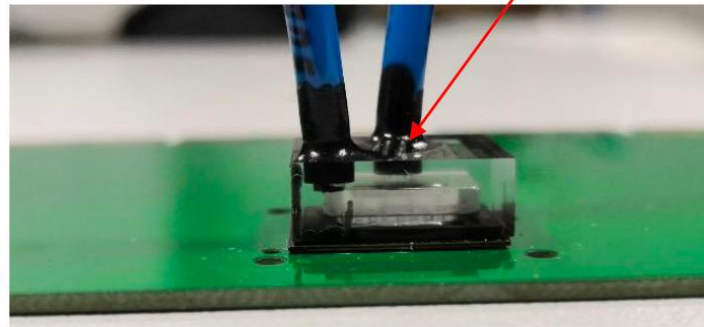
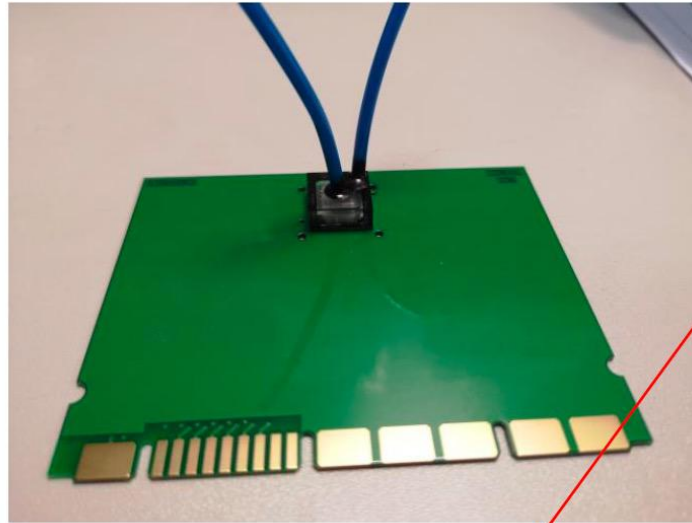
Accurate fabrication of internal geometry and circular nozzles
Measured nozzle diameter $605 \pm 5 \mu\text{m}$ (nominal design $600 \mu\text{m}$)



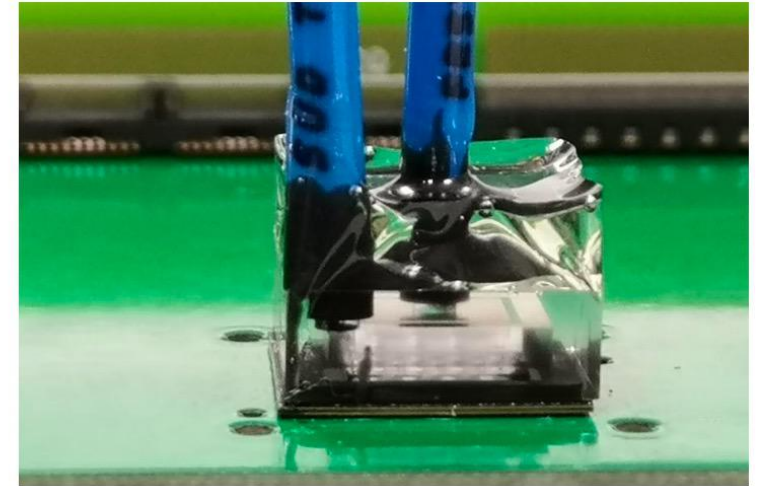
Assembly of the Glass cooler on to the packaging



Wei, Ph.D. thesis, 2020



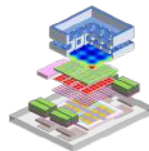
PTCQPLUS soldered to PCB
Glass cooler glued to the package
In-/Out-let tubes glued to the glass cooler
Water leakage at the in-let tube connection point



Additional epoxy applied to strengthen tube connections

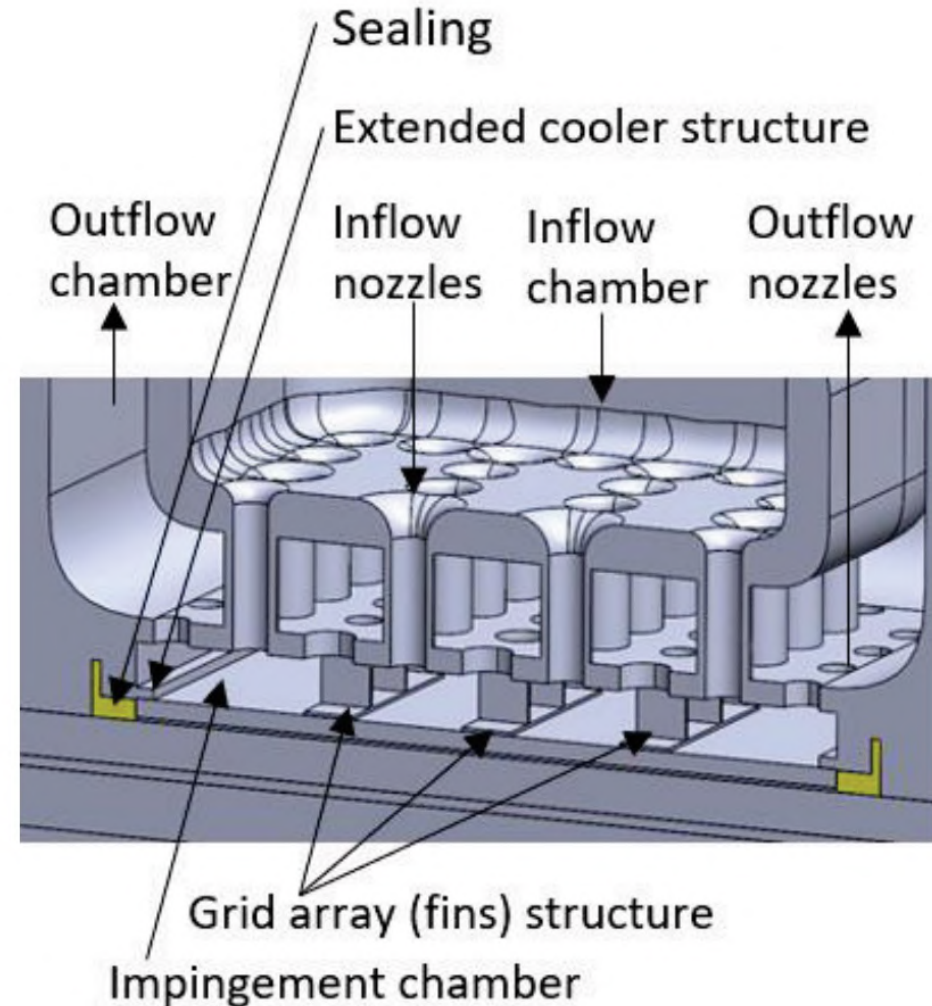
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 - Ceramic-based on cooler
- Other cooling reliabilities: clogging, corrosion...

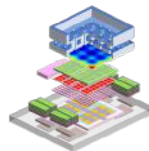


Metal 3D-Printed Direct Liquid Jet-Impingement Cooling

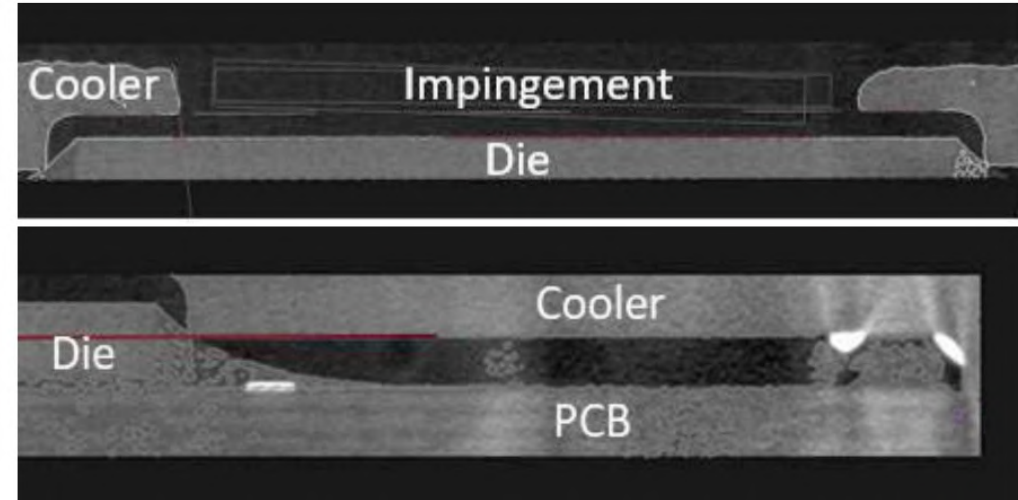
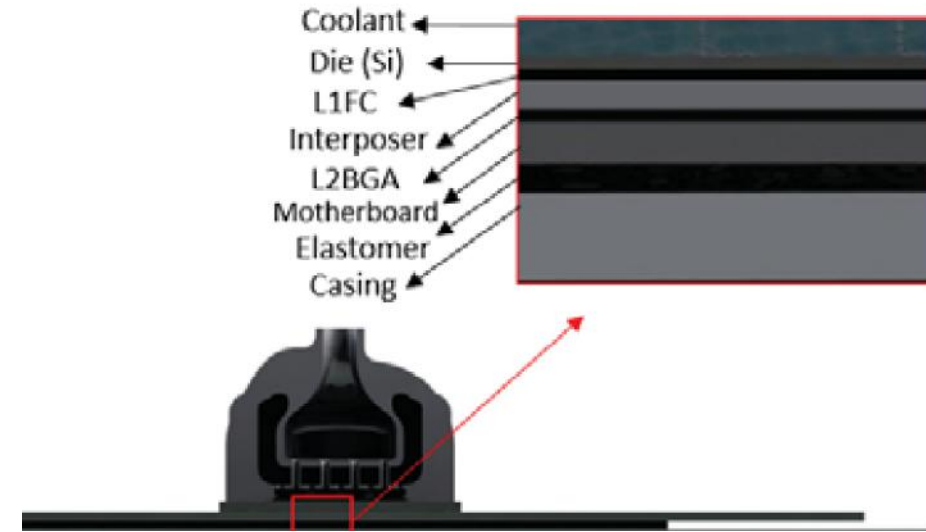
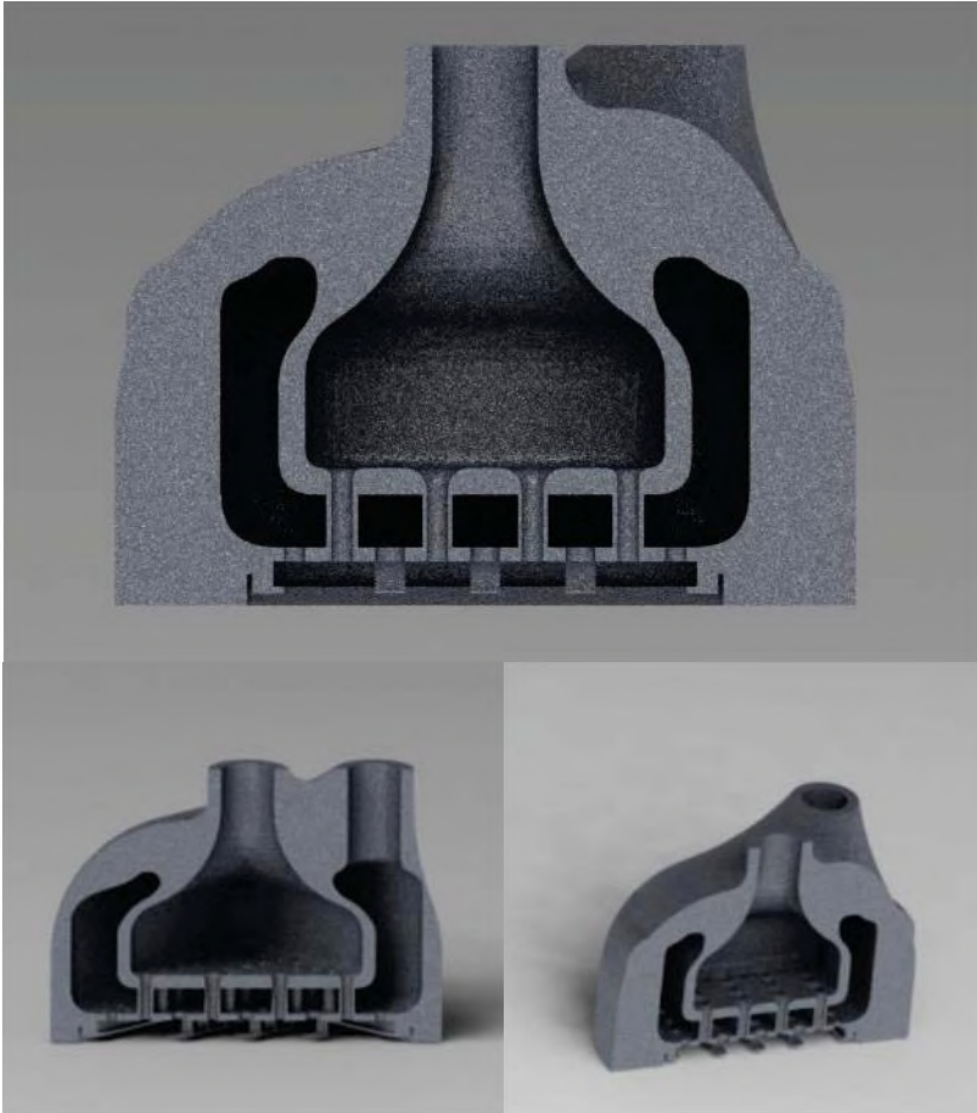
- The advantages of metal 3D printing are numerous, such as the improved dimensional stability and the minimum warpage and shrinkage of parts.
- For the specific application it can be mentioned also the reduction of the CTE mismatch between metal cooler and PCB, on the integration and reliability point of view and the not absorption of liquid by the device.
- More in general, 3D printing makes possible to manufacture parts with shapes and geometries that no other techniques can.



Pappaterra, Antonio, et al. "Advanced (Metal 3D-Printed) Direct Liquid Jet-Impingement Cooling Solution for Autonomous Driving High-Performance Vehicle Computer (HPVC)." EuroSimE. IEEE, 2021

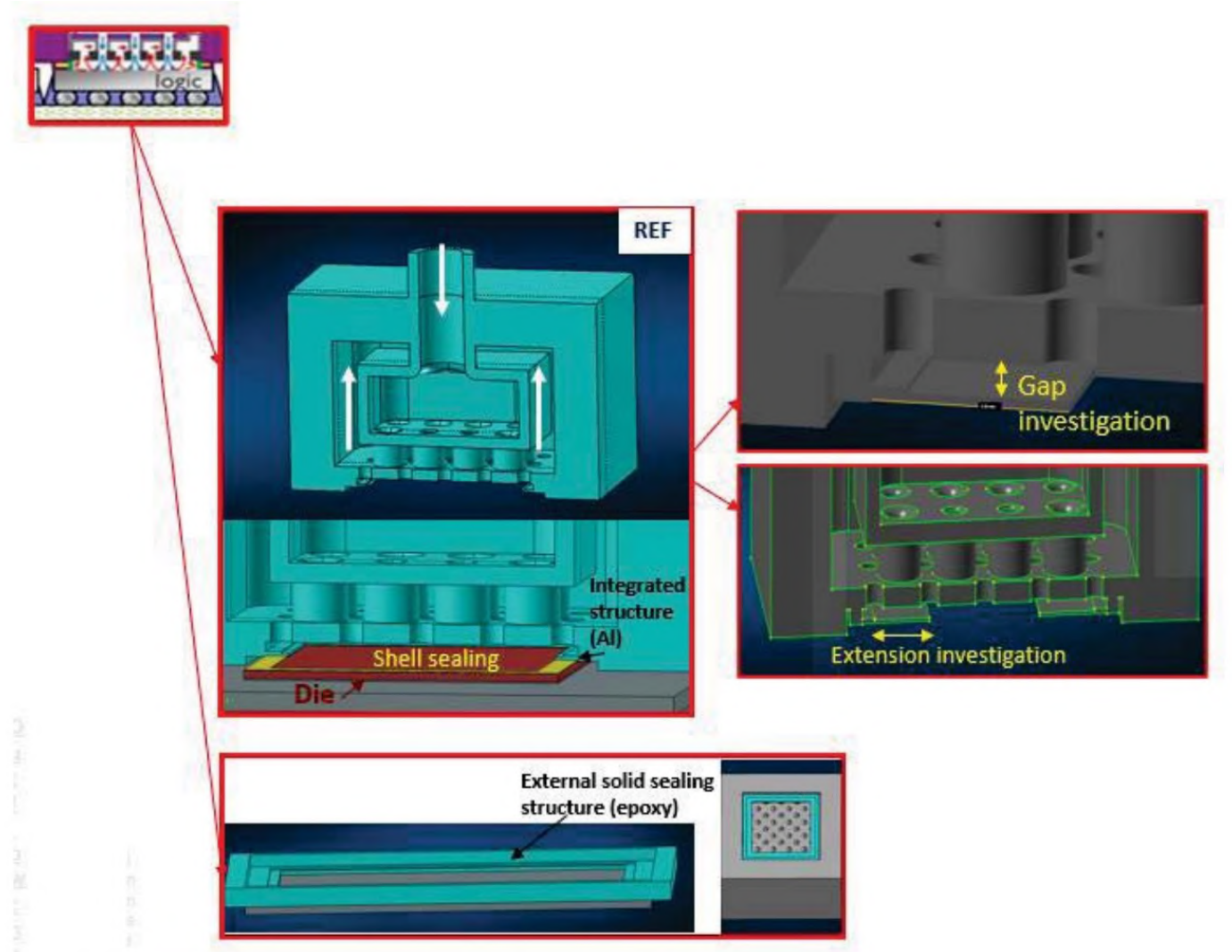


Metal 3D-Printed Direct Liquid Jet-Impingement Cooling



CTS from the side of the cooler

Metal 3D-Printed Direct Liquid Jet-Impingement Cooling



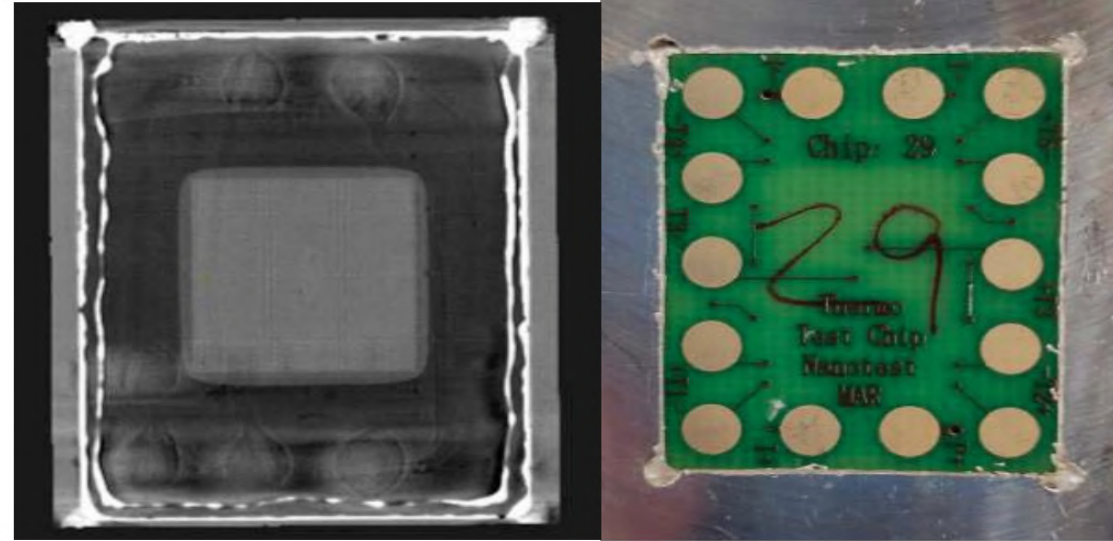
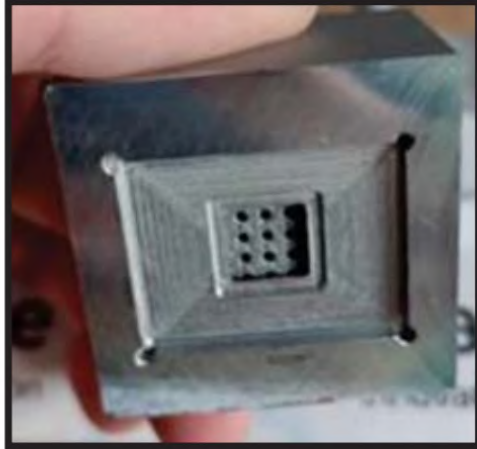
ctor Packaging Laboratory

(All-in-one for Semiconductor Packaging, Heat transfer, and Assembly Lab)

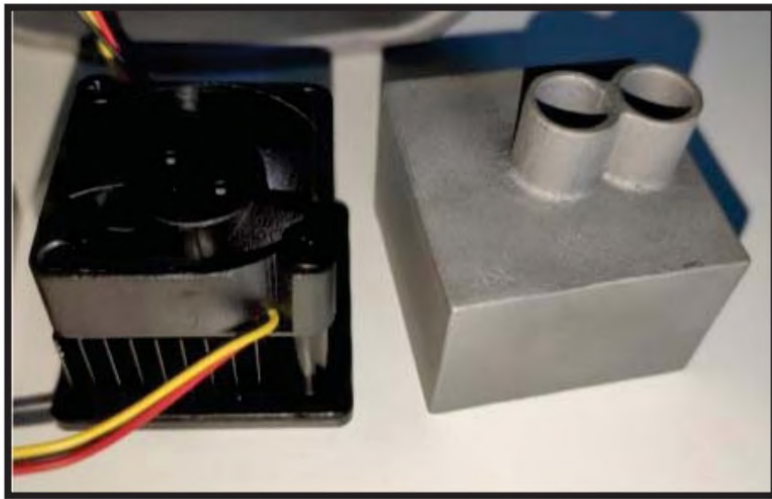
S-PACK Lab

(Advanced Packaging)

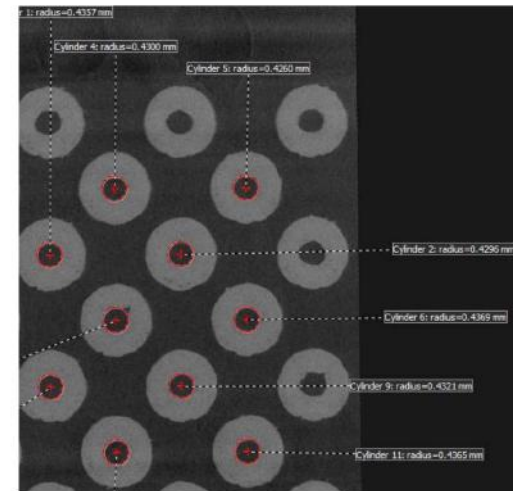
Metal 3D-Printed Direct Liquid Jet-Impingement Cooling



Computed tomography scan (CTS) from the top and picture from the bottom of the chip bonded to the cooler



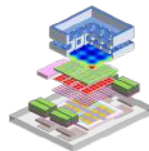
Computed tomography scan (CTS) from the top and picture from the bottom of the chip bonded to the cooler



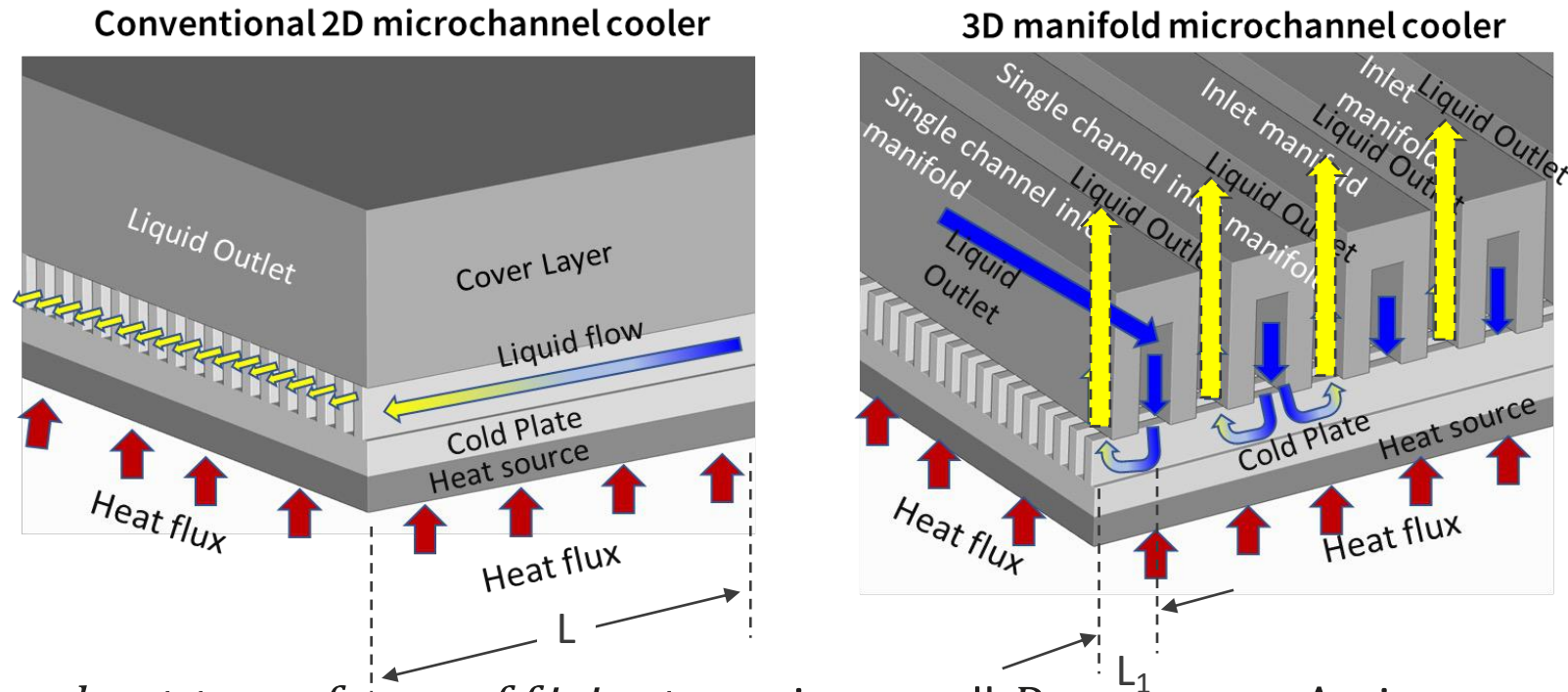
CTS nozzles diameters

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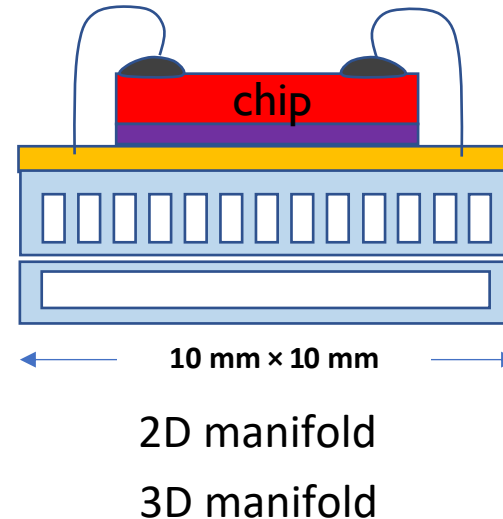
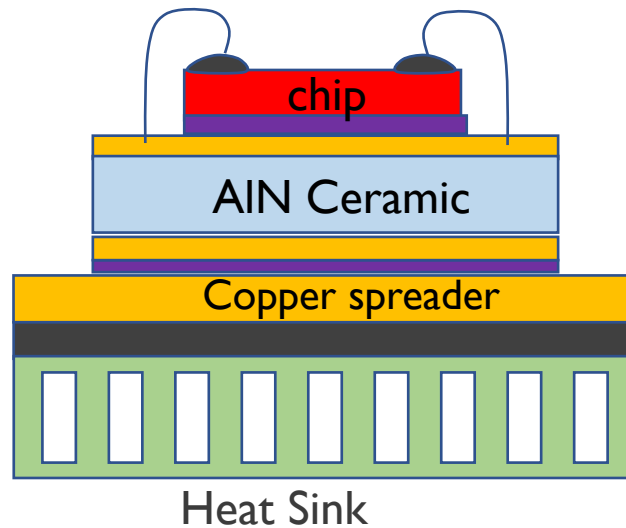
Embedded microchannel with 3D manifold



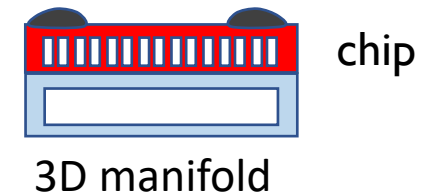
- Higher *heat transfer coefficient* requires small D_h , however, Δp increases \rightarrow system pump power \uparrow
- To reduce Δp , decreasing L using **3D manifold** to deliver cold liquid from the top and collect the hot fluid using U-shape “short” micro-channel
- This results in smaller pressure drop, temperature uniformity, higher heat transfer coefficient, and higher heat flux $> 1\text{kW}/\text{cm}^2$

Embedded microchannel cooling for power electronics

Fluidic Cooling	Cold-plate	Ceramic substrate	Chip
	Conventional package with cold plate cooling	Compact package with DBC embedded u-channel cooling	Ultra-compact package with chip embedded u-channel cooling



Ceramic

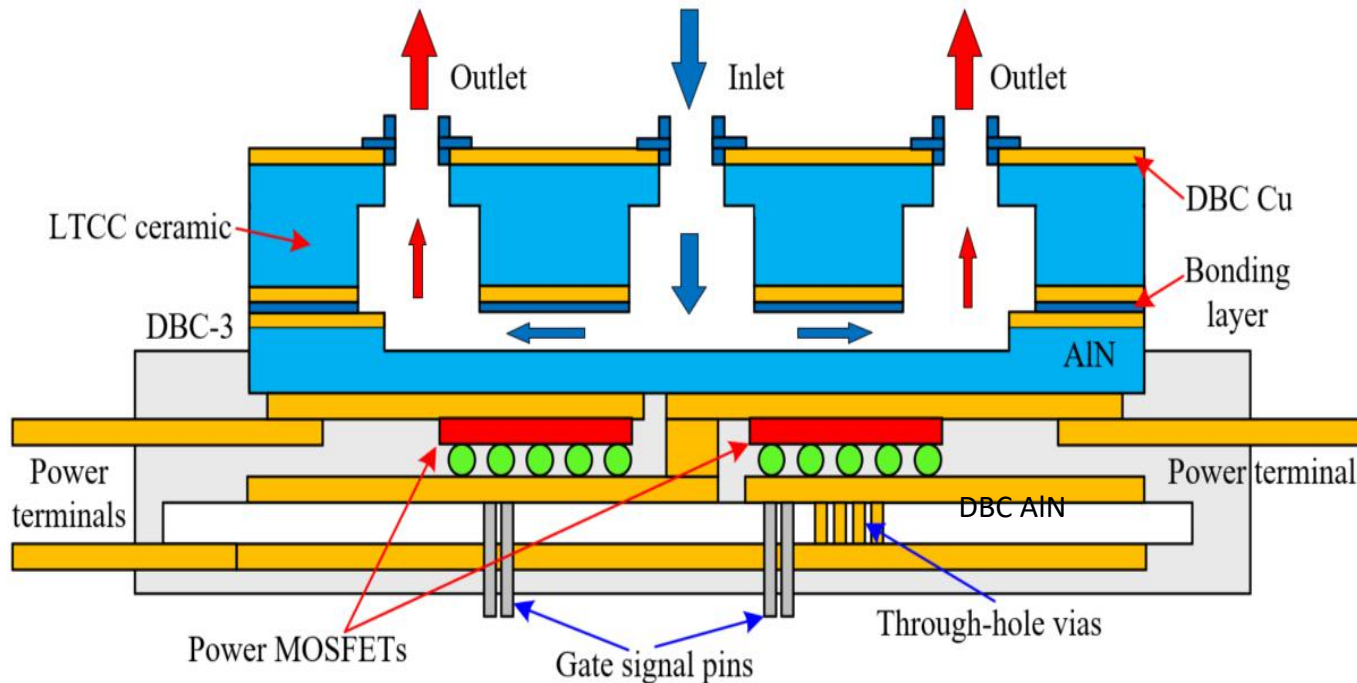


- Power electronics packaging is different → high electrical voltage
- Embedded u-channel inside device needs dielectric liquid
- Ceramic-based channel cooling is promising!



Package-level ceramic-based microchannel cooling integration for power electronics

POETS project: Heterogeneous SiC Power Modules with DBC Active (laser cut) Microchannel Cooling



- Embedded micro-channels into aluminum nitride substrate
- Heterogenous integration: micro-bump bonding and through hole vias
- Electrical-thermal co-design
- Single side cooling → future double side cooling

STANFORD
nanoHeat



PURDUE
UNIVERSITY



Semiconductor Packaging Laboratory

(All-in-one for Semiconductor Packaging, Heat transfer, and Assembly Lab)

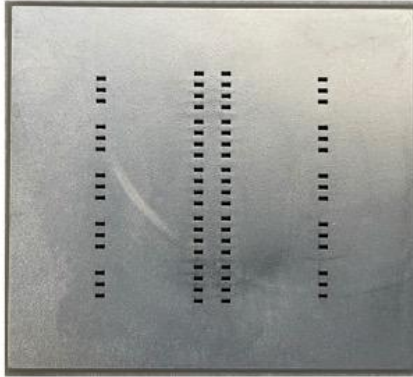
S-PACK Lab

(Advanced Packaging)

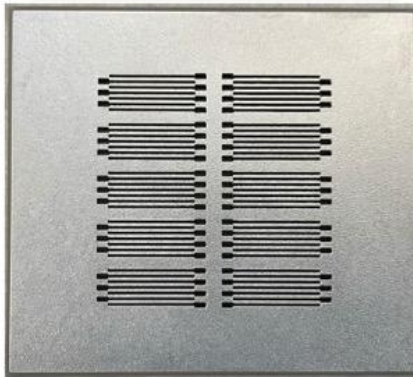
Package-level ceramic-based microchannel cooling integration for power electronics

(a)

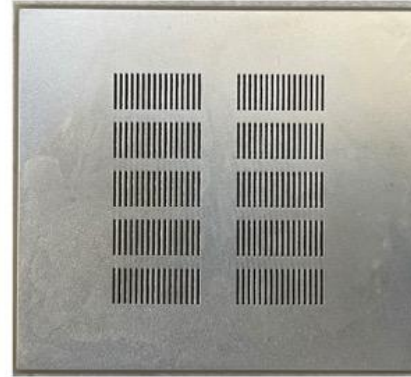
Manifold (Top)



Manifold (Bottom)



u-channel (Top)

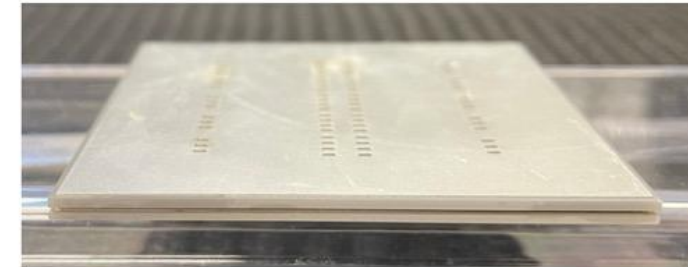


u-channel (Bottom)



(b)

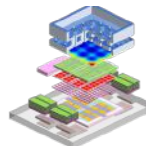
STANFORD
nanoHeat



View from the manifold DBC side

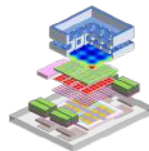


View from the u-channel DBC side



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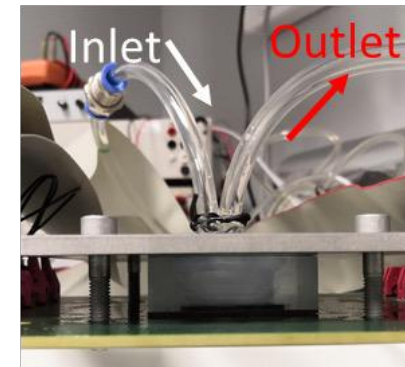
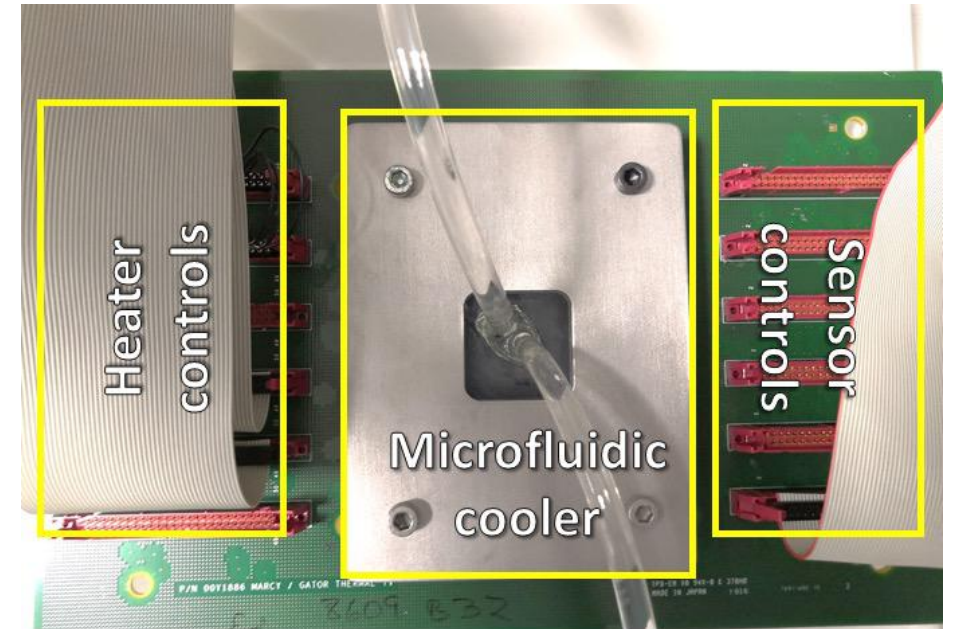
Long term thermal measurement

INTRODUCTION

- Objective: long term measurement of the μ cooler
 - Most challenging case: bar die package
 - Identify reliability issues

PROCEDURE

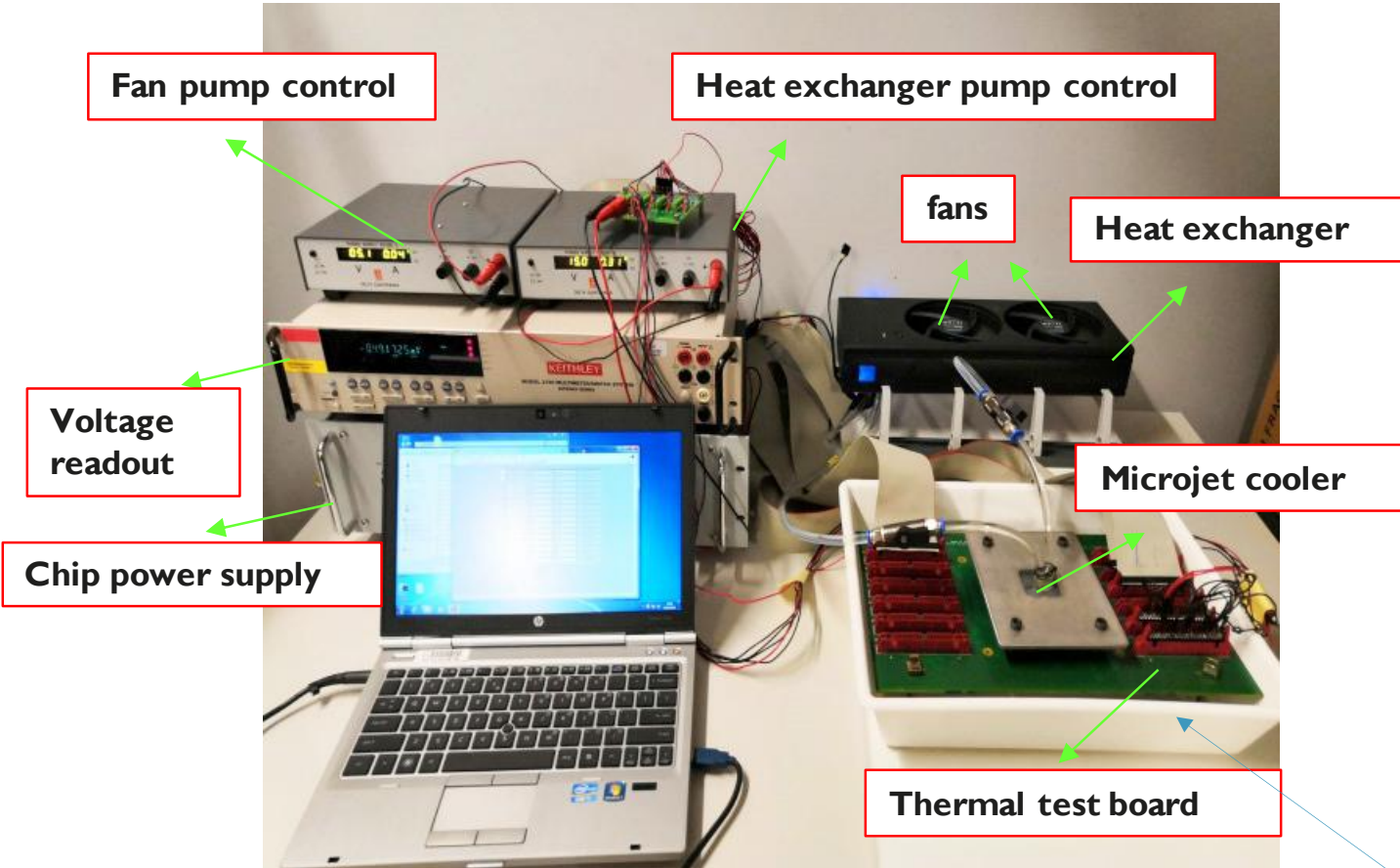
- Duration: 1000h
- Monitor chip temperature
 - Measure every day (24 hours)
- Evaluate cooler geometry:⁴⁵
 - Optical inspection with microscope
 - Measurement at beginning and end of test



Test chip and test board
Courtesy of Global Foundries

Long term thermal measurement

MEASUREMENT SET-UP

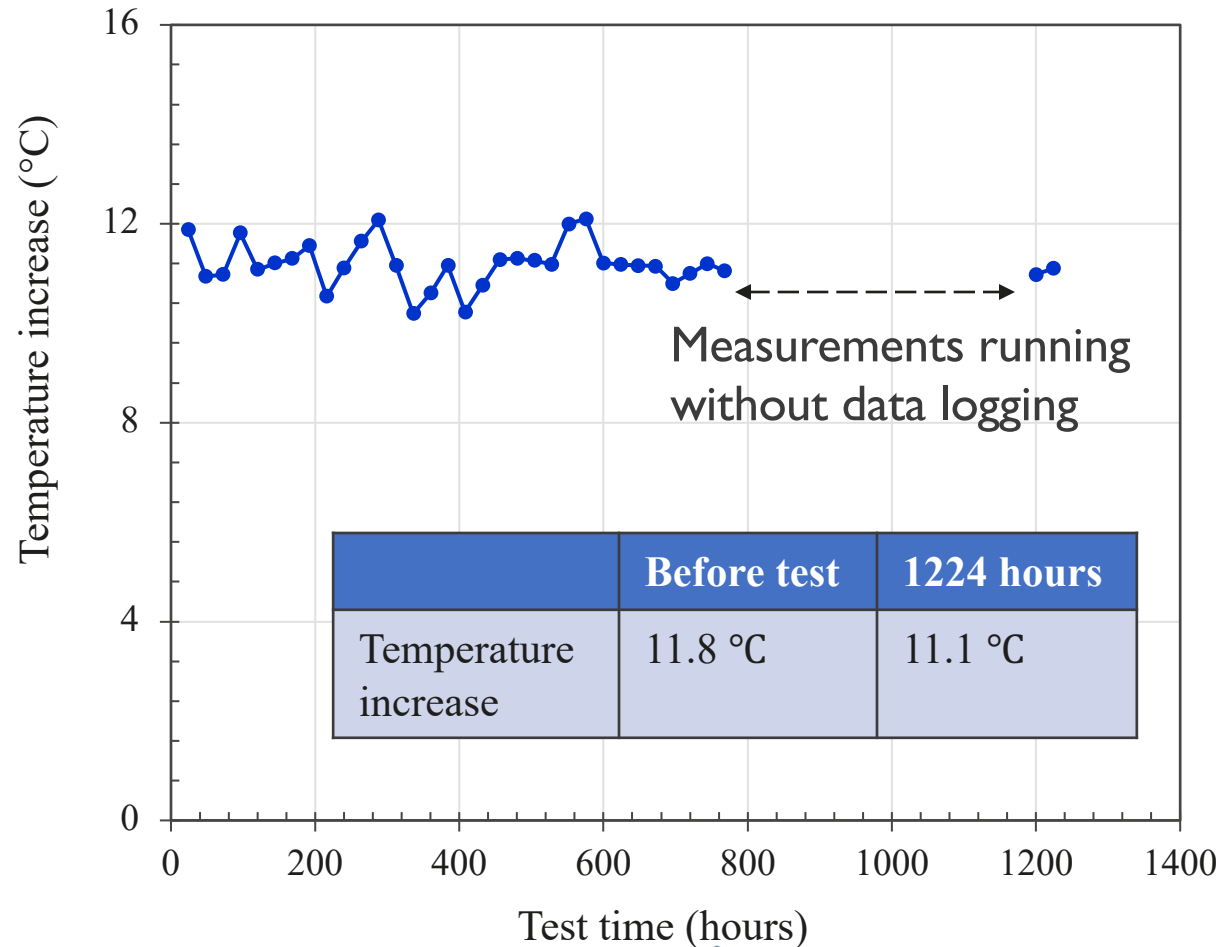


- Simplified set-up developed for thermal and flow measurement
- Integrated pump and heat exchanger for coolant flow loop
 - Fan control
 - Pump control
 - No flow rate control and measurement, can be estimated
- DI water used as liquid coolant
- No filters used in simplified test
- Temperature measurement in all 25 sensors of test chip
- Test board placed in plastic tray to check for leakage

Long term thermal measurement

RESULTS

Average test chip temperature increase above ambient



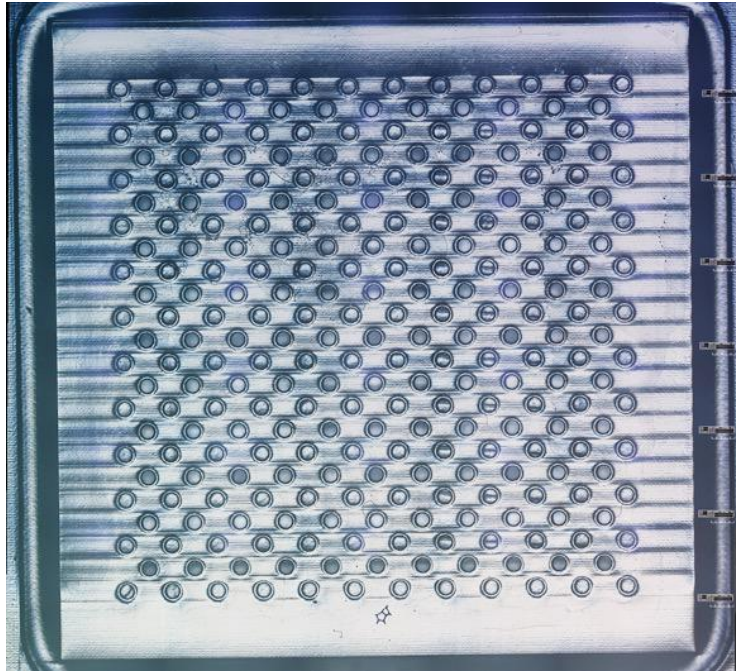
- Test conditions:
 - Chip power: 30W / 90W
 - Pump voltage: 12 V
 - Heat exchanger voltage: 10V
 - Flow rate at 12V: estimation 1.5 L/min
- Cooler performance and room temperature monitored for 50 days

Observations:

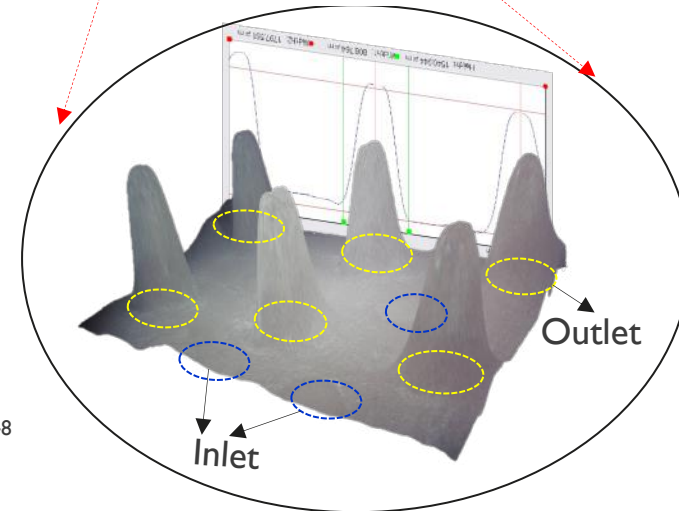
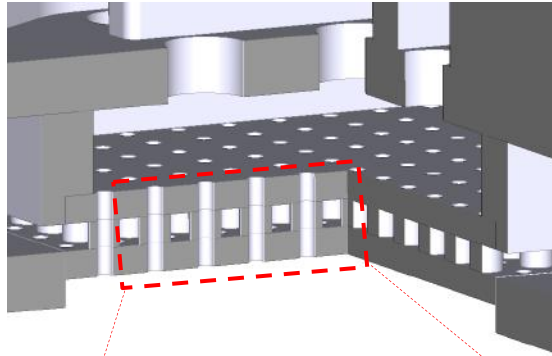
- No leakage observed during the test on the bare die package
- Consistent thermal performance during the 50 days → small variation
- Similar behaviour for all 25 sensors

Long term thermal measurement

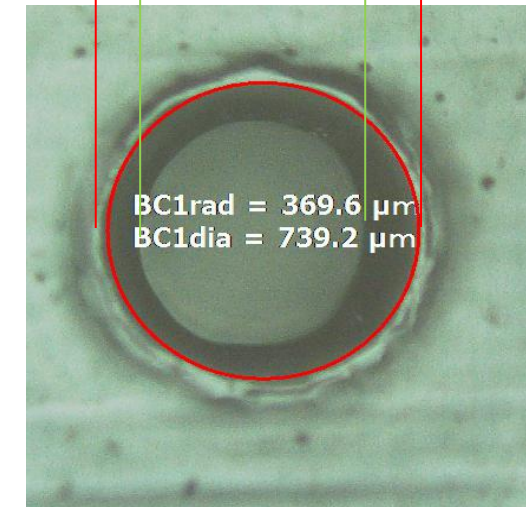
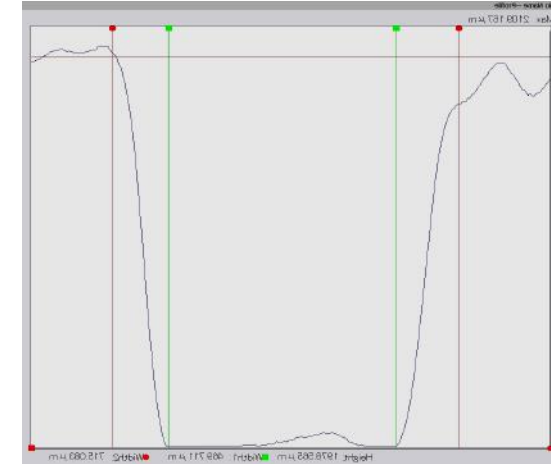
- Impact on cooler geometry: nozzle diameter



Bottom view
(11 x 11 inlet nozzle array)

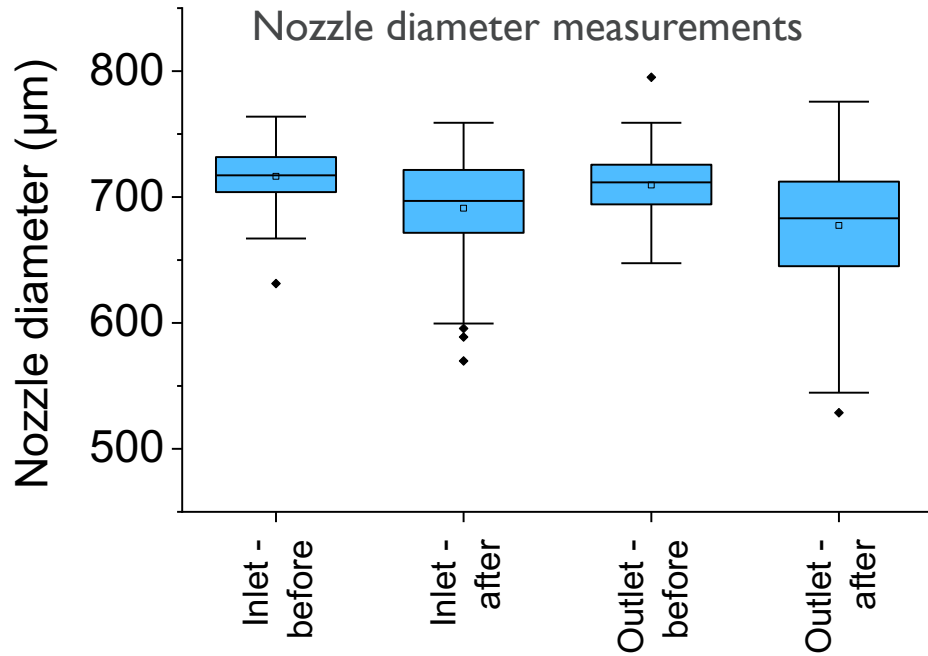


48



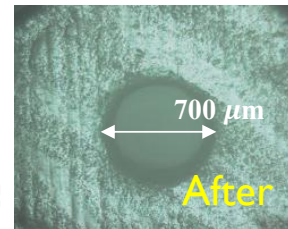
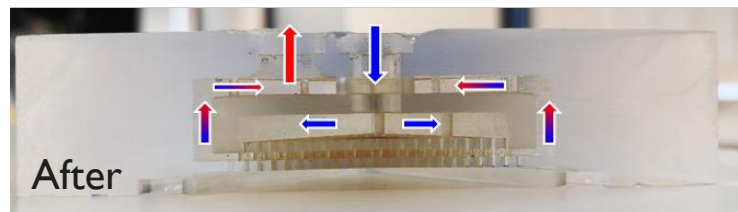
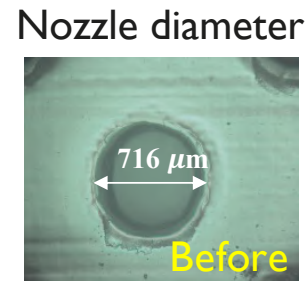
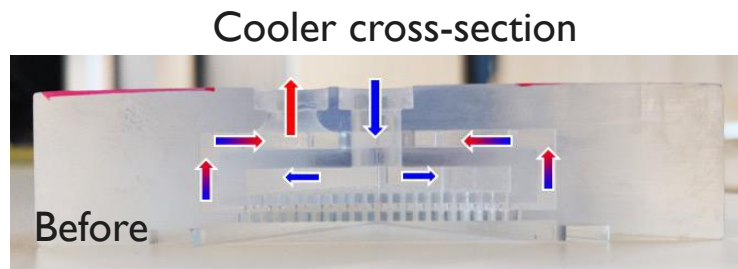
- Nozzle geometry and nozzle diameter evaluation with 2D and reconstructed 3D microscope image before the long-term measurement

Long term thermal measurement: impact of cooler nozzles



Observations after long term measurement with DI water for the 3D printed plastic cooler:

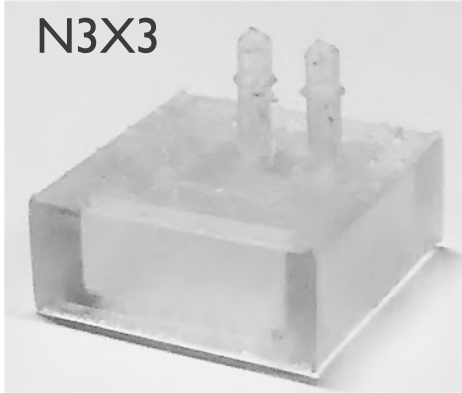
- **No clogging** of the nozzles or internal channels despite lack of filters in simple test setup
- No erosion of the nozzles.
- No significant difference for the nozzle diameters before and after the measurements
- Discoloration of the cooler material in contact with the cooler



Defect measurements of 3d printed cooler

Gen-1 printed cooler

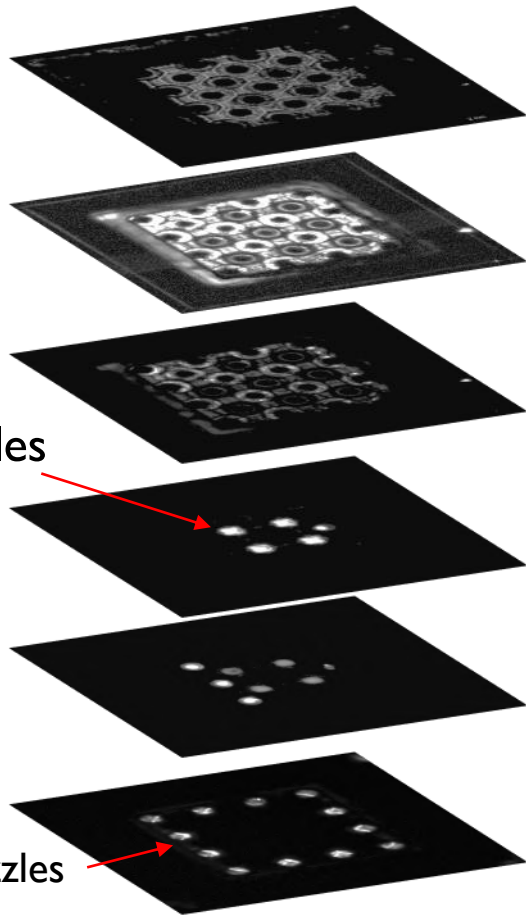
N3X3



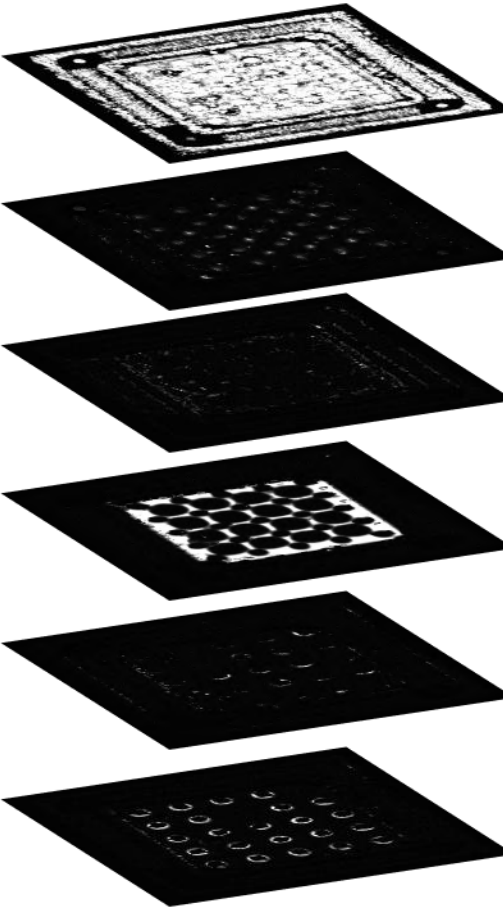
blocked nozzles

tapered nozzles

**SAM image with blocked
nozzles**



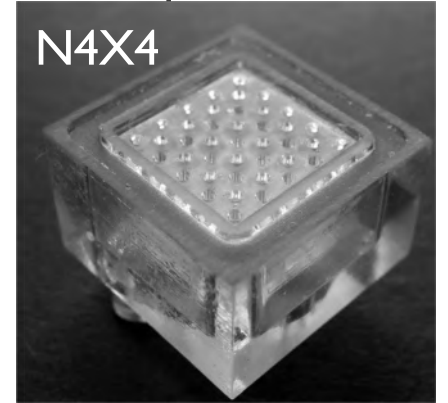
Increasing focus depth



**SAM image with good
nozzles**

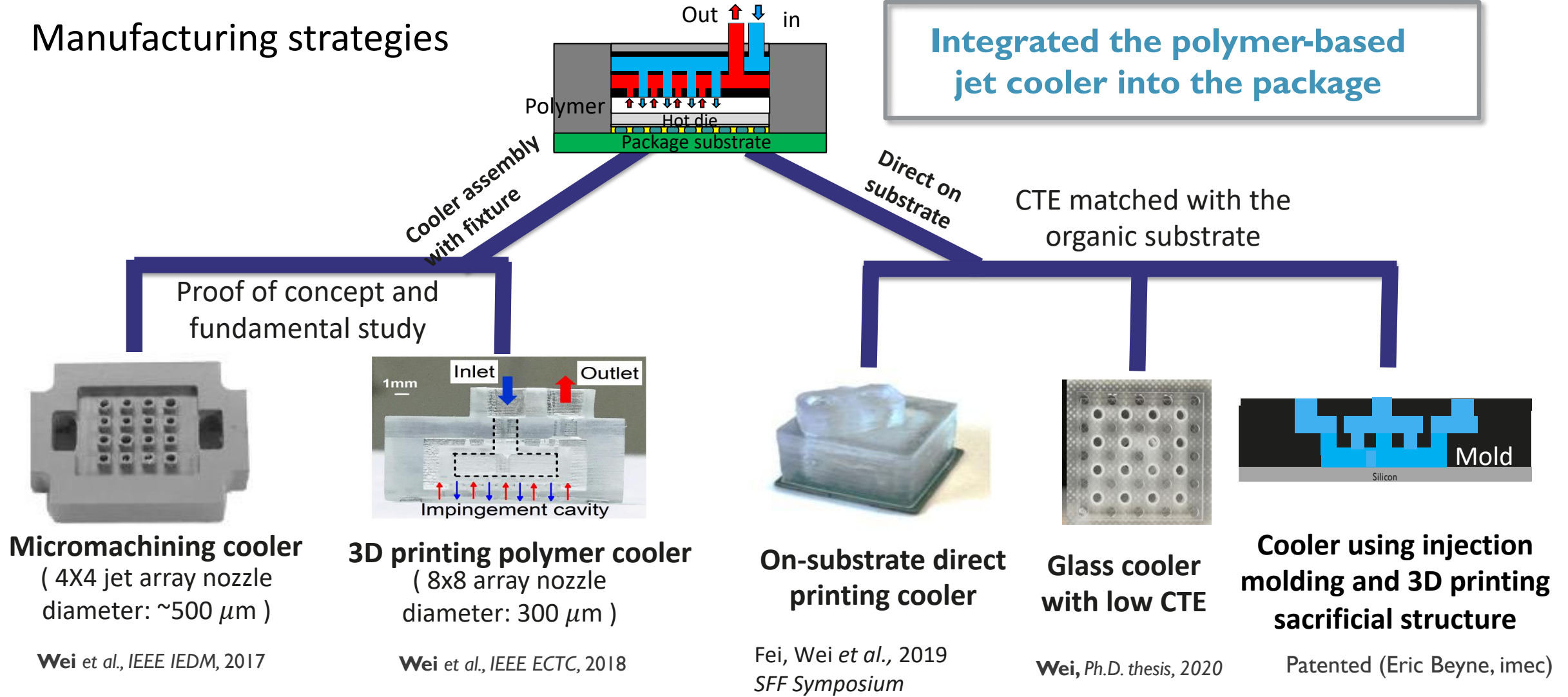
Gen-2 printed cooler

N4X4



Previous work: bare die impingement in package

Manufacturing strategies



***THANK YOU FOR YOUR
ATTENTION!***