

# Unified Lattice Boltzmann Computation for Patient-specific Hemodynamics in Healthy and Diseased Aorta

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## Contributors

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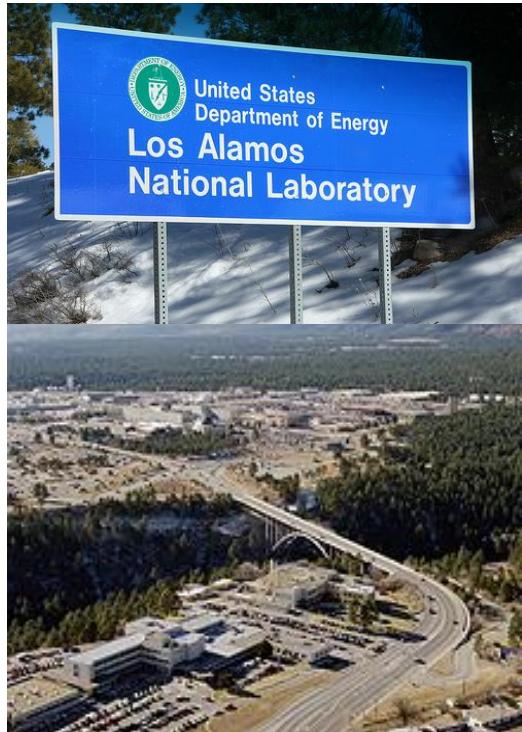




**B.S., Physics**



**Postdoc**



**Ph D, Aerospace Engineering**

**Postdoc**



**Ph D, Physics**



**Assistant Professor**

# Previous Research Experience

## ● **Turbulence computation (modeling and simulation)**

### Kinetic CFD, lattice Boltzmann method

- ▶ Decaying isotropic turbulence w/wo rotation — Texas A&M
- ▶ Turbulent rectangular jets — Texas A&M
- ▶ Flaming in reacting flow — Texas A&M
- ▶ Heat/mass transfer in natural convection — Los Alamos
- ▶ Binary scalar mixing with equal and unequal masses — Texas A&M
- ▶ Peristaltic transport in gastrointestinal tract — Penn State

### Hydrodynamic CFD, Navier-Stokes equations

- ▶ Compressible Rayleigh-Taylor instability w/wo combustion, massive parallel — Los Alamos

## ● **Applied fluid mechanics**

- ▶ Linear stability analysis of compressible RT instability in cylindrical geometry — Los Alamos
- ▶ Rapid distortion theory in compressible turbulence — Texas A&M
- ▶ Public turbulence database enabled analysis for Lagrangian turbulence — Johns Hopkins

## ● **Cyber CFD and database technology (computational and experimental data)**

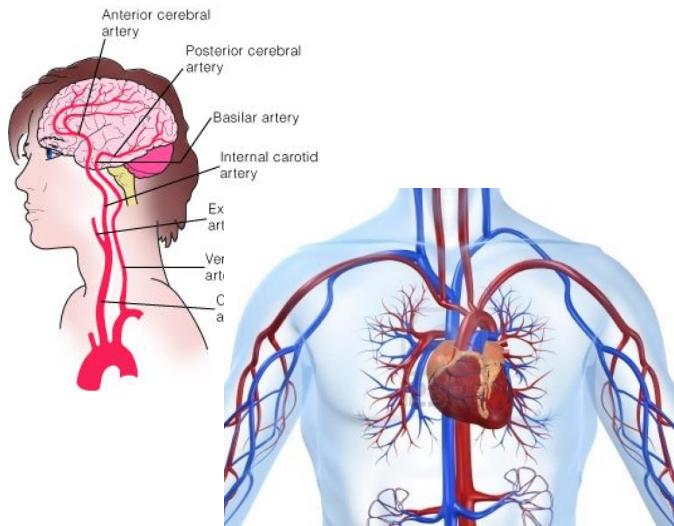
- ▶ Web-accessed turbulence database, “cyber fluid dynamics” — Johns Hopkins
- ▶ Cohesive experimental database for predicting long-term corrosion/erosion of steel exposed to flowing liquid lead/lead bismuth eutectic — Los Alamos

# Outline

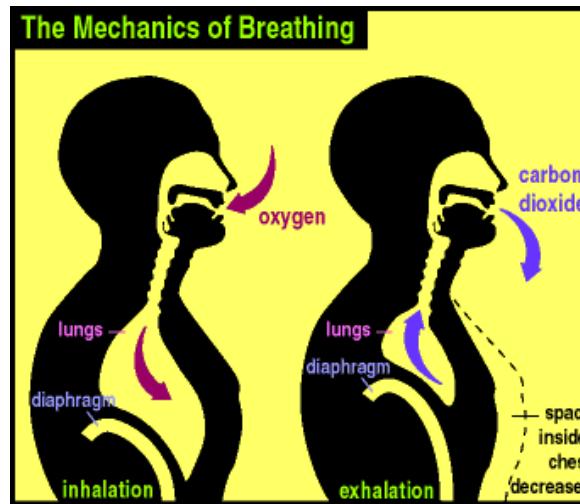
- Background and research motivation
- Unified computation platform for patient-specific computational hemodynamics using lattice Boltzmann method
- Preliminary results on patient-specific hemodynamics in healthy and diseased aorta
- Summary

# Flows in Human Body

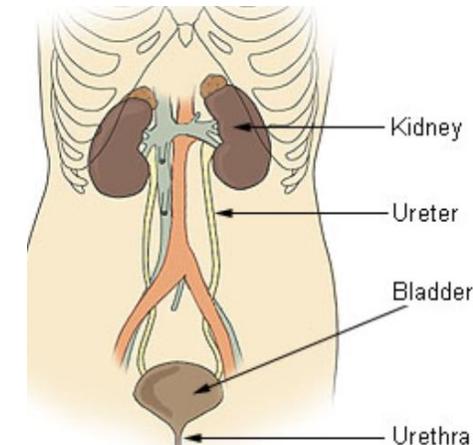
## Circulatory System



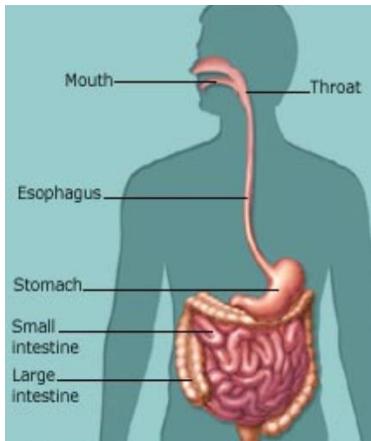
## Respiratory System



## Urinary System



## Digestive System



## Fluid-structure interaction

### Structure:

- Arbitrary geometry
- Bifurcations
- Deformable
- Willfully/compliantly moving

### Fluid/flow:

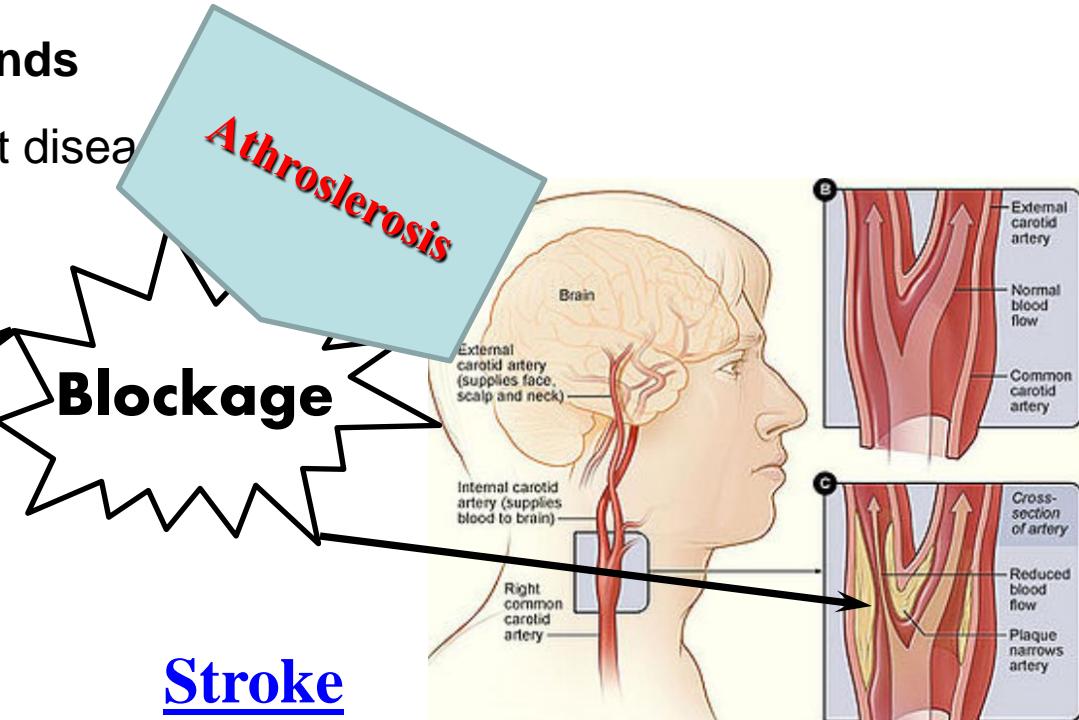
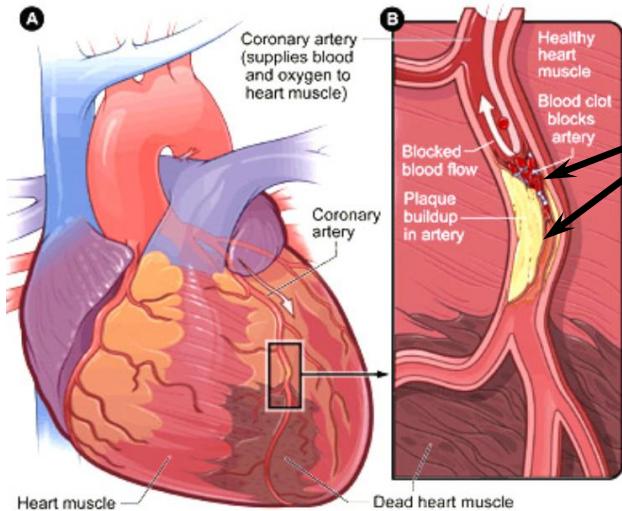
- Pulsatile
- Laminar/turbulence
- Non-Newtonian
- Multiphase

# Cardiovascular Disease Facts

from [www.CDC.gov](http://www.CDC.gov)

## Heart Attack

- Killing **600K** people, **1 in every 4** deaths
- One heart attack every **34 seconds**
- \$108.9 billion for coronary heart disease



Hypothesis: hemodynamics likely reveals the mechanism of plaque disruption or embolization

- Killing **130K** people, **1 in every 19** deaths
- One heart attack every **34 seconds**
- \$38.6 billion for health care, medication, lost productivity

# Hemodynamics: In Vivo Imaging

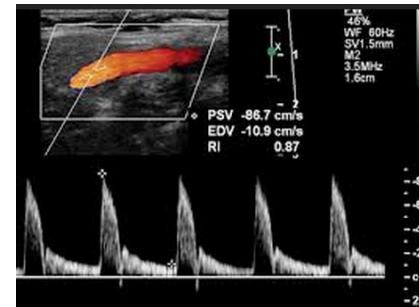
## Phase-Contrast Magnetic Resonance Imaging

*J Thorac Imaging* • Volume 28, Number 4, July 2013

REVIEW ARTICLE

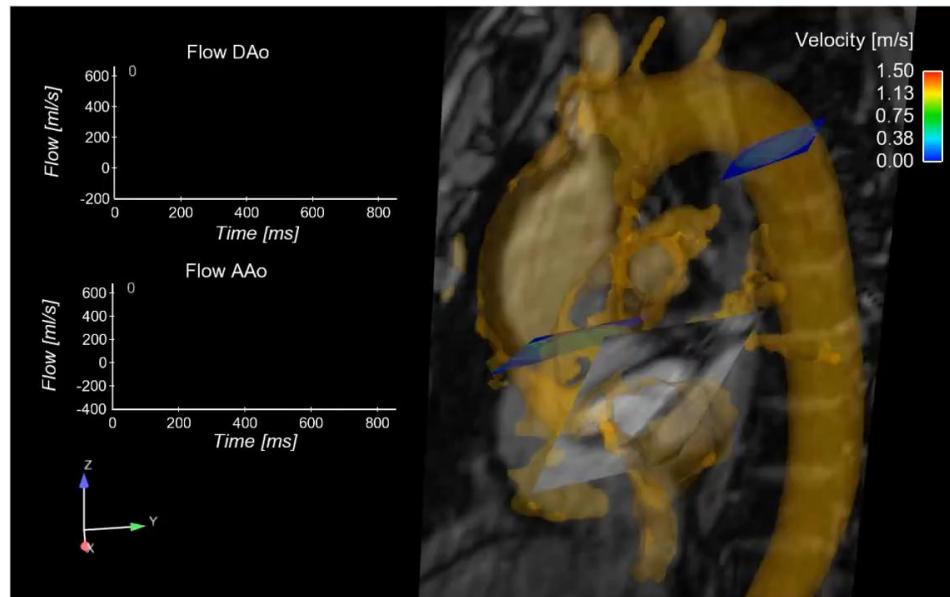
### Cardiothoracic Magnetic Resonance Flow Imaging

Michael D. Hope, MD,\* Tony Sedlic, MD,\* and Petter Dyverfeldt, PhD\*†‡

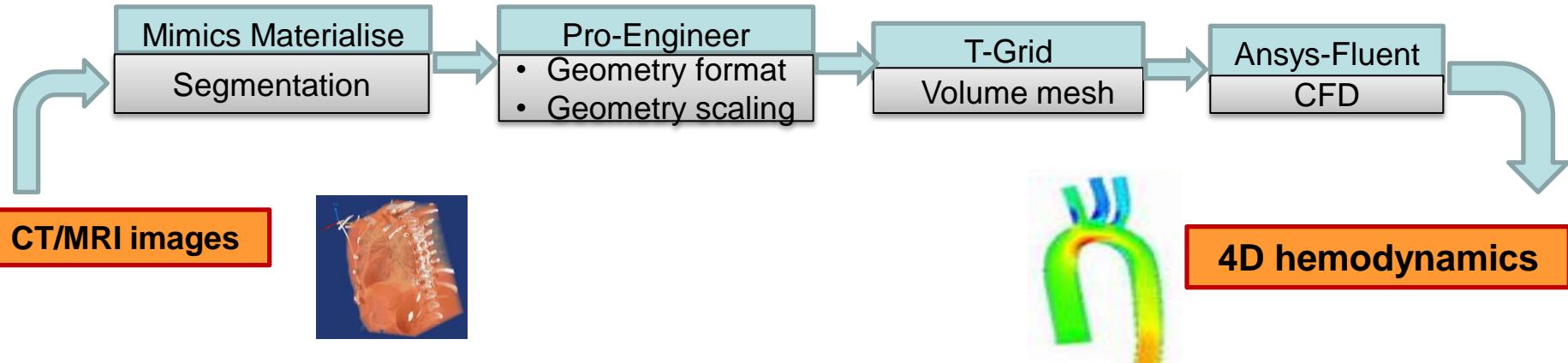


### Challenges for clinical application

- Long scan time (hours)
- Data processing  
(time consuming,  
specific operator skills)
- Lack of proven clinical applications
- Limited to heart and great vessels

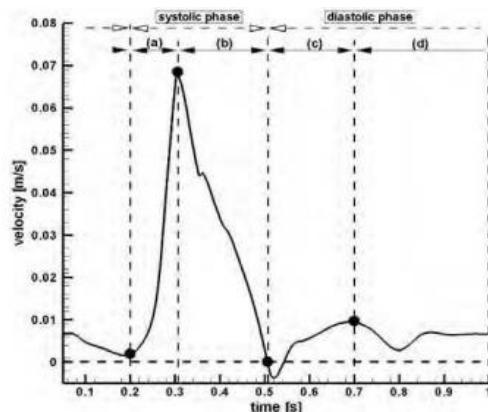


# Patient-specific Computational Fluid Dynamics

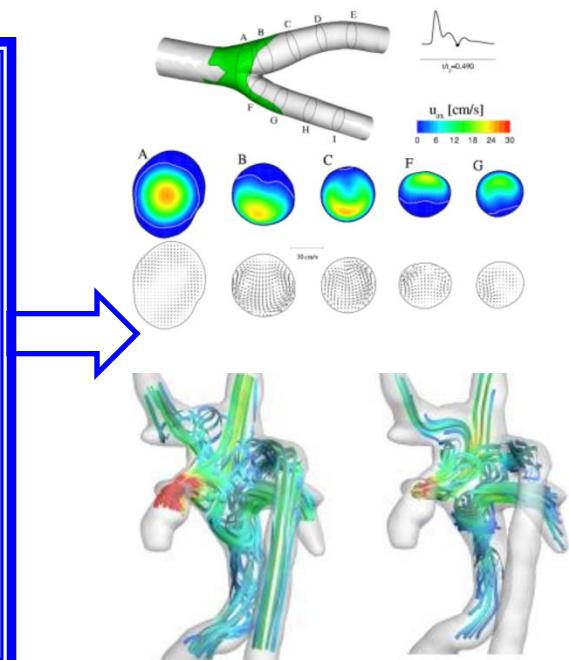
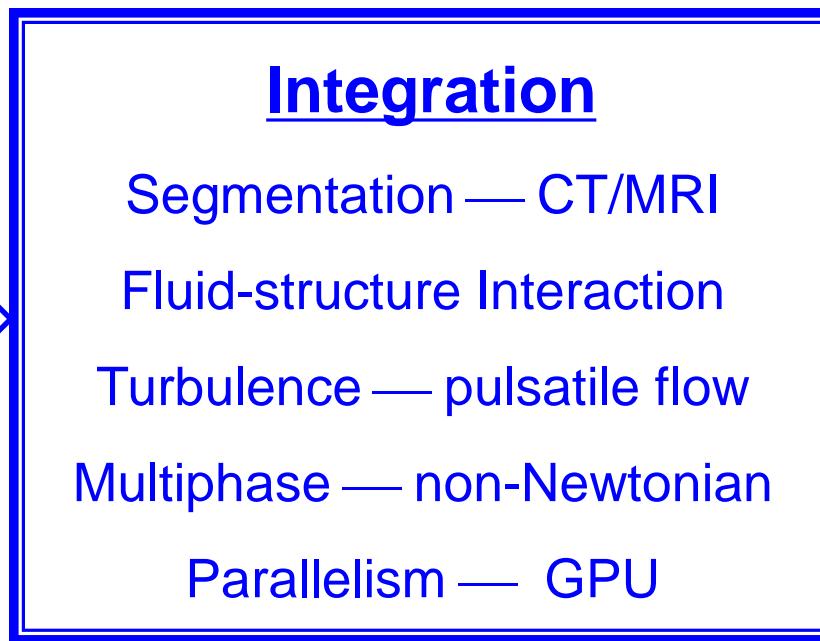
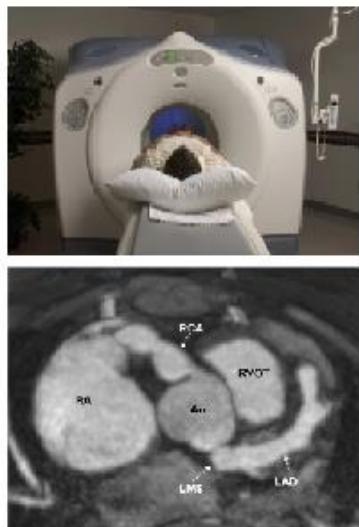


## Limitations:

1. Inadequate for pulsatile flow
2. Modeling — FSI, Multiphase, etc.
3. GPU parallel computing



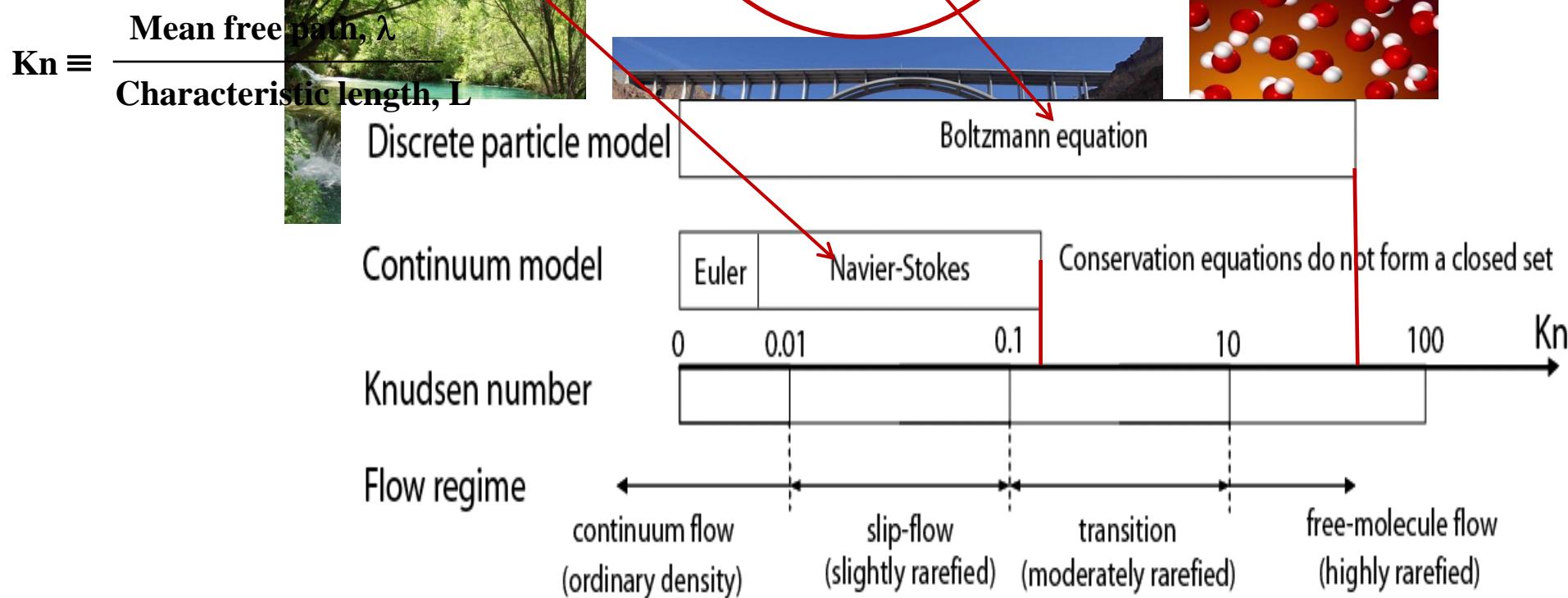
# Unified Computation Platform



# **Lattice Boltzmann Method**

# Descriptions of Fluid Dynamics

	Macroscopic	Mesoscopic	Microscopic
Theory	Hydrodynamics	Kinetic Theory	Molecular Dynamics
Equations	Navier-Stokes	Boltzmann	Newton-Hamilton
subject	Continuum variables	Particle distribution function	Particle trajectories



The diagram is adapted from Anderson J., *Hypersonic and high temperature gas dynamics*, McGraw-Hill, 1989.

# Boltzmann Equation

Key variable: particle distribution function

$$\frac{\partial f}{\partial t} + \vec{\xi} \cdot \nabla f + \frac{\partial f}{\partial \vec{\xi}} \cdot \vec{F} = J(f)$$

collision operator

$$\int \begin{bmatrix} 1 \\ \vec{\xi} \\ (\vec{\xi} - \vec{u})^2 \end{bmatrix} J(f) d\vec{\xi} = \begin{bmatrix} 0 \\ 0 \\ 0 \end{bmatrix}$$

Collision satisfies conservation laws

$$\frac{\partial \rho}{\partial t} + \frac{\partial(\rho u_i)}{\partial x_i} = 0$$

$$\rho \left( \frac{\partial u_i}{\partial t} + u_j \frac{\partial u_i}{\partial x_j} \right) + \frac{\partial P_{ij}}{\partial x_i} = \rho f_i$$

$$\rho \left( \frac{\partial e}{\partial t} + u_j \frac{\partial e}{\partial x_j} \right) + \frac{P_{ij} \partial u_i}{\partial x_j} + \frac{\partial q_i}{\partial x_i} = 0$$

$P_{ij}$ , and  $q_i$  closures

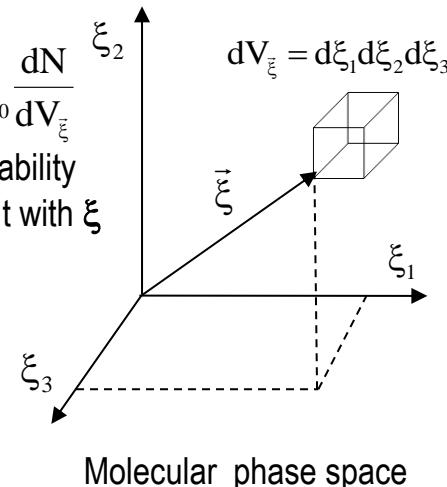
Higher order moments

Beyond NS

N-S  
Equations

$$f(\vec{x}, \vec{\xi}, t) = \frac{\rho}{N} \lim_{dV_{\vec{\xi}} \rightarrow 0} \frac{dN}{dV_{\vec{\xi}}}$$

density weighted probability  
to find a particle at  $\vec{x}$ ,  $t$  with  $\vec{\xi}$



## Hydrodynamic variables

Density  $\rho(\vec{x}, t) = \int f(\vec{x}, \vec{\xi}, t) d\vec{\xi}$

Momentum  $\rho \vec{u}(\vec{x}, t) = \int \vec{\xi} f(\vec{x}, \vec{\xi}, t) d\vec{\xi}$

Internal Energy  $\rho e(\vec{x}, t) = (1/2) \int \vec{c}^2 f(\vec{x}, \vec{\xi}, t) d\vec{\xi}$

Stress tensor  $P_{ij}(\vec{x}, t) = - \int c_i c_j f(\vec{x}, \vec{\xi}, t) d\vec{\xi}$

Heat flux density  $\vec{q}(\vec{x}, t) = (1/2) \int \vec{c} (\vec{c} \cdot \vec{c}) f(\vec{x}, \vec{\xi}, t) d\vec{\xi}$

$$\vec{c} \equiv \vec{\xi} - \vec{u}$$

## Non-hydrodynamic moments

### Remarks:

Bhatnagar-Gross-Krook (BGK) approximation

1. BE covers NS, and more than NS

2. Once  $f$  known, hydrodynamics known

$Z$ : Average collision frequency

$f_M$ : Maxwell-Boltzmann equilibrium distribution function

# A Passage from BGKBE to BGKLBE

**BGK or SRT model**

$$\partial f / \partial t + \vec{\xi} \cdot \nabla f = -Z(f - f_M), \quad f = f(\vec{x}, \vec{\xi}, t)$$

X. He and L-S Luo, PRE 56, 6811(1997)

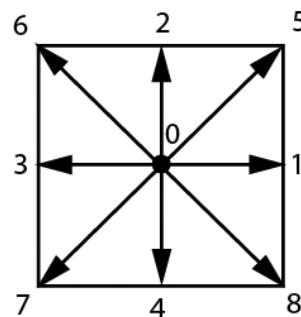
## 1. Discretization of time

$$f(\vec{x} + \vec{\xi}\delta t, \vec{\xi}, t + \delta t) = f(\vec{x}, \vec{\xi}, t) - [f(\vec{x}, \vec{\xi}, t) - f_M(\vec{x}, \vec{\xi}, t)]/\tau$$

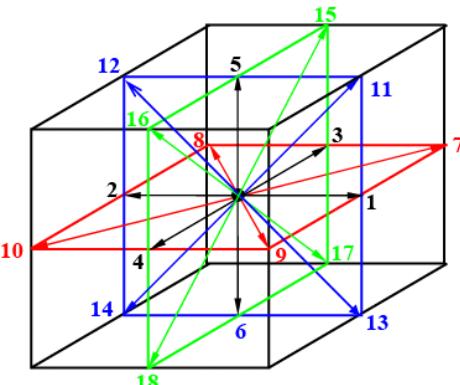
$$\tau = 1/(Z\delta t)$$

## 2. Discretization of physical space and molecular velocity space coherently in finite directions satisfying conservation laws and symmetry needs

## 3. Taylor expand $f_M$ at low Mach number limit and determine coefficients based on conservation laws and symmetry needs



$$\vec{e}_\alpha = \begin{cases} (0,0) & \alpha = 0 \\ (\pm 1, 0), (0, \pm 1) & \alpha = 1-4 \\ (\pm 1, \pm 1) & \alpha = 5-8 \end{cases}$$



$$\vec{e}_\alpha = \begin{cases} (0,0,0) & \alpha = 0 \\ (\pm 1, 0, 0), (0, \pm 1, 0), (0, 0, \pm 1) & \alpha = 1-6 \\ (\pm 1, \pm 1, 0), (\pm 1, 0, \pm 1), (0, \pm 1, \pm 1) & \alpha = 7-18 \end{cases}$$

$$f_\alpha(\vec{x} + \vec{e}_\alpha \delta t, t + \delta t) = f_\alpha(\vec{x}, t) - [f_\alpha(\vec{x}, t) - f_\alpha^{(eq)}(\vec{x}, t)]/\tau$$

$$\tau = 3v/(c\delta x) + 0.5$$

Chapmann-Enskog technique

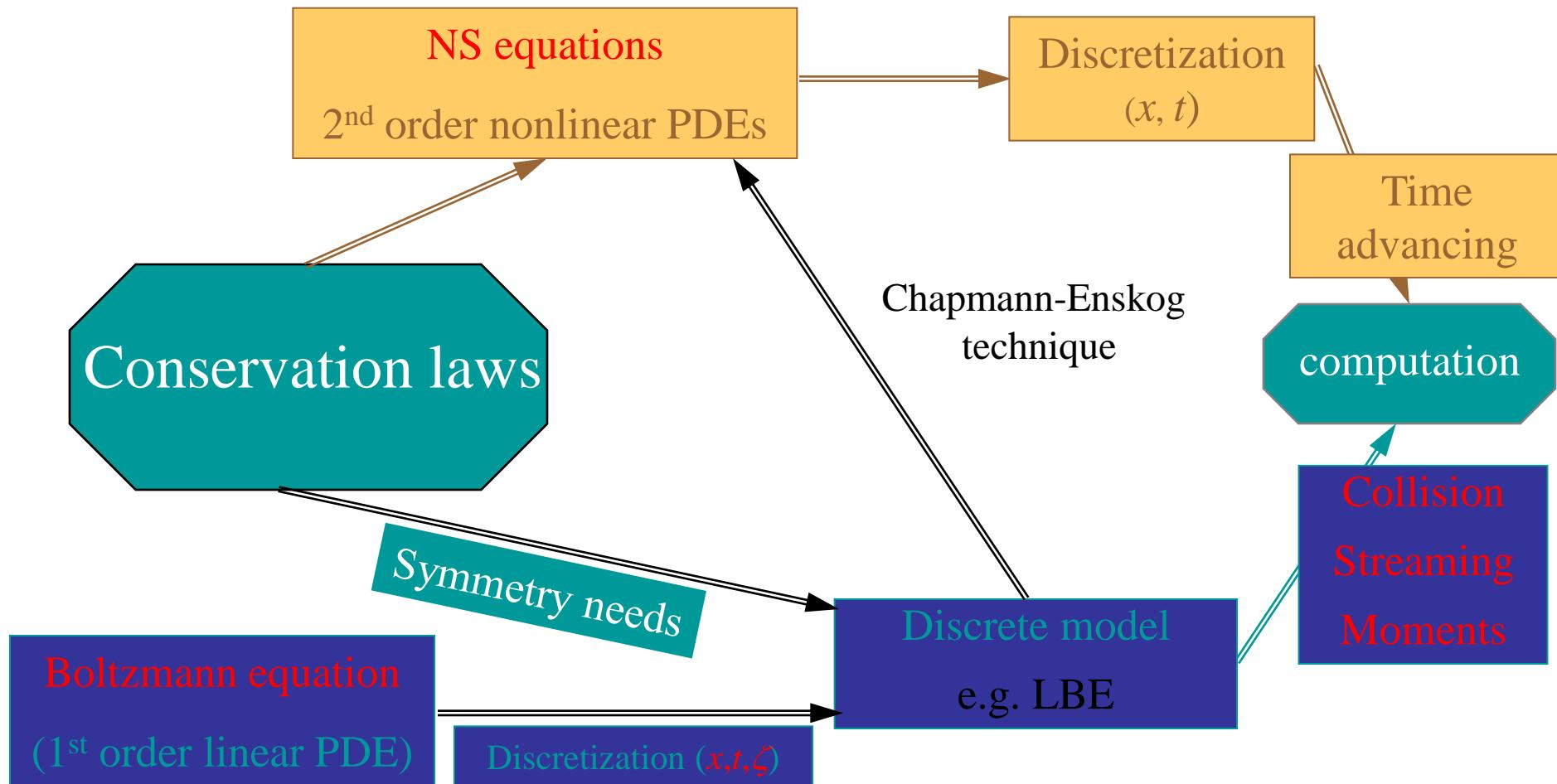
$$\nabla \cdot \vec{u} = 0, \quad \partial \vec{u} / \partial t + \vec{u} \cdot \nabla \vec{u} = -\nabla p / \rho + v \nabla^2 \vec{u}$$

$$\rho = \sum f_\alpha$$

$$\rho \vec{u} = \sum c \vec{e}_\alpha f_\alpha$$

# Computation Methodologies

## Computational Fluid Dynamics (CFD)



## Digital Fluid Dynamics (DFD)

# Potential Advantages of LBM

$$f_\alpha(\vec{x} + \vec{e}_\alpha \delta t, t + \delta t) = f_\alpha(\vec{x}, t) - [f_\alpha(\vec{x}, t) - f_\alpha^{(eq)}(\vec{x}, t)] / \tau$$

$$\rho = \sum f_\alpha, \rho \vec{u} = \sum \vec{e}_\alpha f_\alpha$$

- Simpler implementation

Linear equation  
Discrete equation  
Single variable  
Arithmetic calculation  
(no derivative involved)

- More physical concepts: collision and streaming

e.g. Single phase: self collision  
Multiphase: self and mutual collisions  
Miscible: attracting  
Immiscible: repelling  
No-slip boundary: bounce-back

- Easy handling of **complicated geometry or boundary**

e.g. porous media, bio-transport, etc.

- Ideally suited for **multi-phase** flows

e.g. interfacial dynamics, fluid structure interaction, etc

- Good candidate for problems **beyond Navier-Stokes**,

e.g. rarified gas, plasma, micro/nano fluidics

- Well suited for large-scale, **parallel** (GPU) computing

# A Historic View of LBM

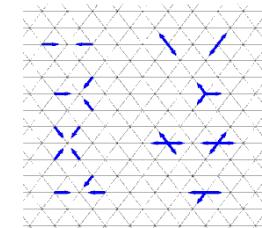
## Lattice gas automata (LGA)

Frisch, Hasslacher, and Pomeau, PRE, 1986

$$n_\alpha(x + \delta_t e_\alpha, t + \delta_t) = n_\alpha(x, t) + C_\alpha(\{n_\beta\}), C_\alpha(\{n_\beta\}): \text{collision operator}$$

Main drawbacks:  $n_\alpha \in [0,1]$ : Boolean particle number

Intrinsically noisy; lack of Galilean invariance,  
unphysical pressure; unphysical conserved quantities



Discrete molecular phase space

Ensemble Average of LGA:  $f_\alpha = \langle n_\alpha \rangle \in [0,1]$ , G. McNamara and G. Zanetti, PRE, 1988

## Lattice Boltzmann method (LBM)

Qian, d'Humières, Lallemand, Europhys. Lett. (1992), H Chen, S Chen, and Matthaeus, Phys. Rev. E, 1992,

$$f_\alpha(x + \delta_t e_\alpha, t + \delta_t) = f_\alpha(x, t) + \Omega_\alpha(x, t)^*$$

$f_\alpha$ : particle number with  $e_\alpha$  at  $x$

$\Omega_\alpha$ : collision operator

\* Empirical evolution of LGA historically. Mathematical proof by Abe, JCP(1997), He&Luo, PRE (1997)

Restrictions: — incompressible flow

Small Mach number assumption; Small knudsen number assumption;

thermal model numerically unstable; not clear how to extend beyond NS

Bhatnagar-Gross-Krook approximation

$$\Omega_\alpha(x, t) = -[f_\alpha(x, t) - f_\alpha^{(eq)}(x, t)]/\tau$$

Moment expansion, Shan & He, PRL, 1998

## Kinetic theory representation of hydrodynamic Navier-Stokes and beyond

Shan, Yuan, and Chen, JFM, 2006

Breakthroughs:

Compressible, shocks, rarified, thermodynamic effect

# LBM for Imagine Processing

**Image segmentation**

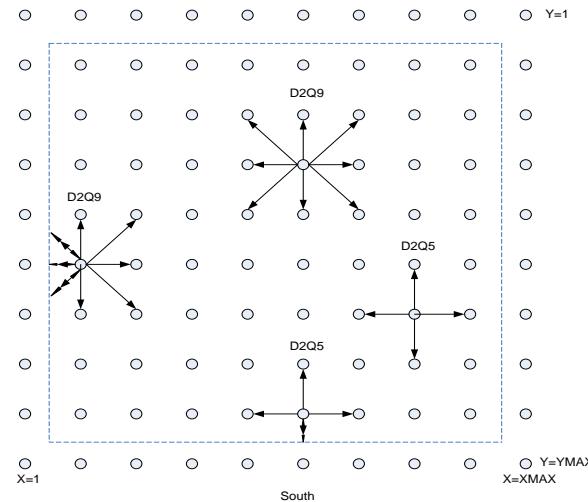
**Image denoising**

**Image Filtering**

**Image lighting**

- Zhao, Y., *Lattice Boltzmann based PDE solver on the GPU*. Visual Computer, 2008.
- Zhao, Y. *GPU-Accelerated Surface Denoising and Morphing with Lattice Boltzmann Scheme*, in *IEEE International Conference on Shape Modeling and Applications*, 2008.
- Hagan, A. and Zhao, Y., *Parallel 3D Image Segmentation of Large Data Sets on a GPU Cluster*, in *the 5th International Symposium on Visual Computing*, 2009.
- Cahang, Q. and Yang, T., *A lattice Boltzmann method for image denoising*. IEEE Transactions on Image Processing, 2009.
- Zhang, W. and Shi, B., *Application of Lattice Boltzmann Method to Image Filtering*. Journal of Mathematical Imaging and Vision, 2012.
- Balla-Arabé, O. and Gao, X., *A fast and robust level set method for image segmentation using fuzzy clustering and lattice Boltzmann method*. IEEE Trans Syst Man Cybern B., 2012.

# Modern Graphics and Visualization



- Modern images are digitized.
- PDEs are widely used in graphics and visualization applications
  - Image processing
  - Surface processing
  - Volume graphics and visualization

# Image Segmentation

Caselles, Kimmel, and Sapiro, Int. J. Comp. Vision, 1997.

## Geometric Active Contour (GAC) model:

$$\frac{\partial \vec{C}}{\partial t} = [g(\kappa + \alpha) - (\nabla g \cdot \vec{N})]\vec{N}$$

$I_0$ : original image  
 $C$ : evolving curve  
 $\kappa$ : curvature  
 $g$ : edge-stopping function  
 $\sigma$ : smooth parameter

Image      smoothing

$$g = \frac{1}{1 + |\nabla(G_\sigma * I_0)|^2}$$

gradient of a Gaussian smoothed data

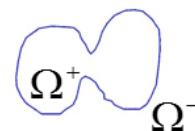


## Level set formulation — diffusion equation with an external force

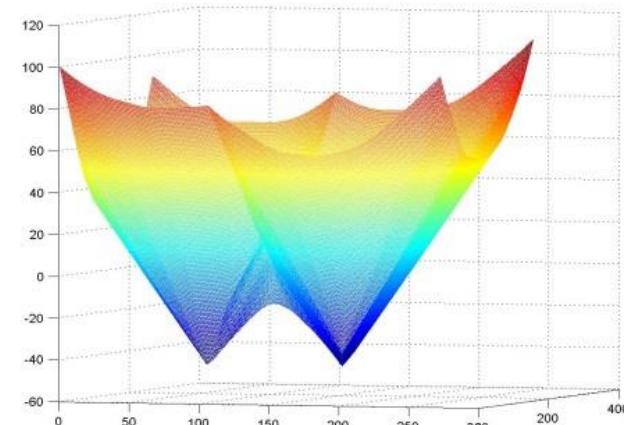
$$\frac{\partial u}{\partial t} = \nabla \cdot (g \nabla u) + F$$

$u$ : level set function — distance field of the active contour

$F$ :  $ga$



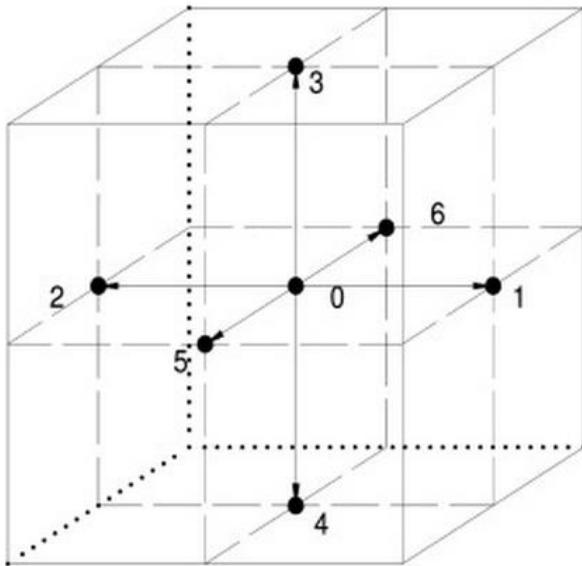
Contour (zero level set)



# LB-GAC Model

$$f_i(\vec{x} + \Delta t \cdot \vec{e}_i, t + \Delta t) - f_i(\vec{x}, t) = \omega \cdot [f_i^{\text{eq}}(\vec{x}, t) - f_i(\vec{x}, t)] + \Delta t F_i \quad (i = 1, \dots, 7)$$

D3Q7 lattice



$$\omega = 2/(1 + 6\Delta t g)$$

$$F_i(\vec{x}, t) = \frac{1}{7} F(\vec{x}, t)$$

$$f_i^{\text{eq}}(\vec{x}, t) = \frac{1}{7} u(\vec{x}, t)$$

$$u(\vec{x}, t) = \sum_{i=1}^7 f_i(\vec{x}, t)$$

I. Ginzburg, Equilibrium-type and Link-type Lattice Boltzmann models for generic advection and anisotropic-dispersion equation, Adv Water Resour, 2005

# Segmentation Flow Chart

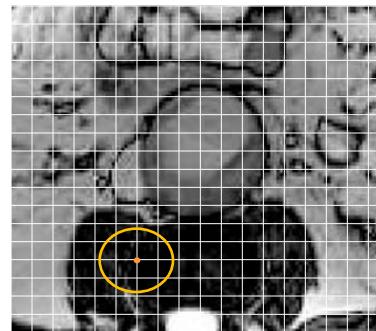
Given image data  $I_0(\vec{x}) \Rightarrow g(\vec{x})$

$$F_i(\vec{x}, 0) = \alpha g(\vec{x}, 0) / 7$$

Initialization

$$u(\vec{x}, t) \begin{cases} < 0, \text{inside} \\ > 0, \text{outside} \\ = 0, \text{interface} \end{cases}$$

$$f_i(\vec{x}, 0) = f_i^{\text{eq}}(\vec{x}, 0) = u(\vec{x}, 0) / 7$$



LBM collision

$$f'_i(\vec{x}, t) = f_i(\vec{x}, t) + \omega \cdot [f_i^{\text{eq}}(\vec{x}, t) - f_i(\vec{x}, t)] + \Delta t F_i$$

streaming

$$f_i(\vec{x} + \Delta t \cdot \vec{e}_i, t + \Delta t) = f'_i(\vec{x}, t)$$

Updated distance function

$$u(\vec{x}, t + \Delta t) = \sum_i f_i(\vec{x}, t + \Delta t)$$



Update  $u(\vec{x}, t + \Delta t) = 0$

$$f_i^{\text{eq}}(\vec{x}, t + \Delta t) = u(\vec{x}, t + \Delta t) / 7$$

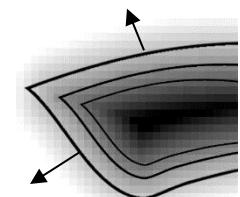
Solid volume

Voxelize a 3D triangular-polygon mesh to compute the volume of boundary cell

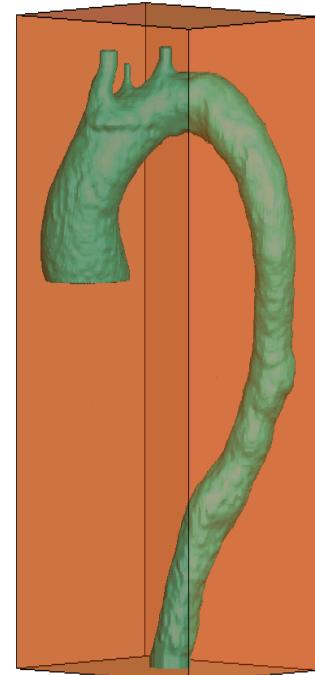
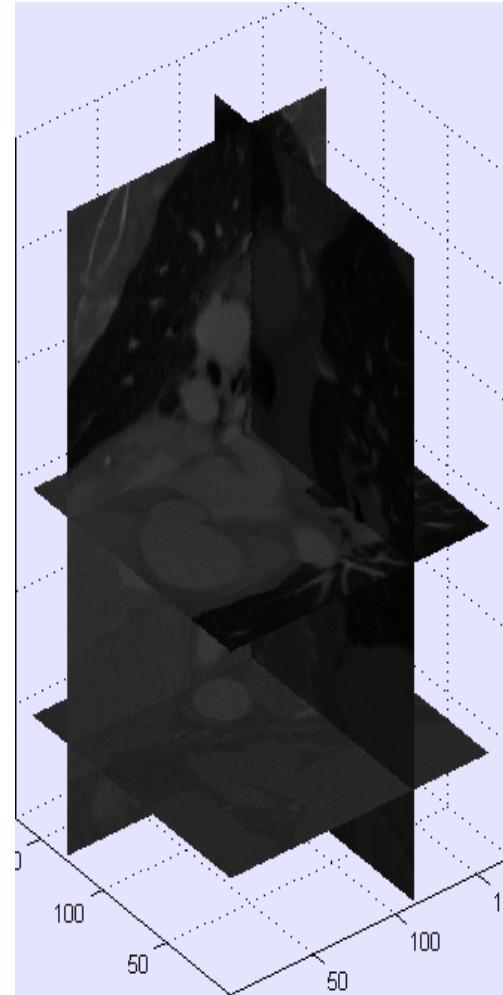
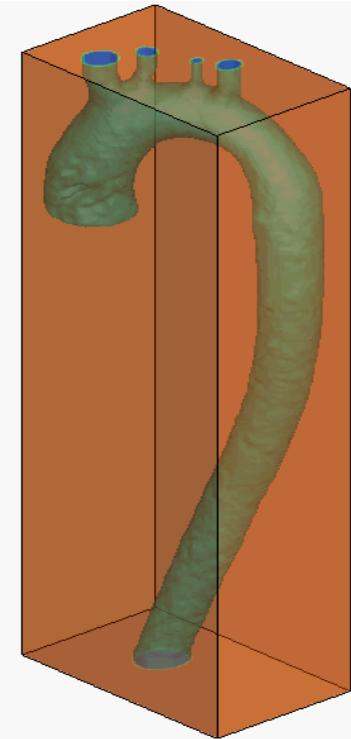
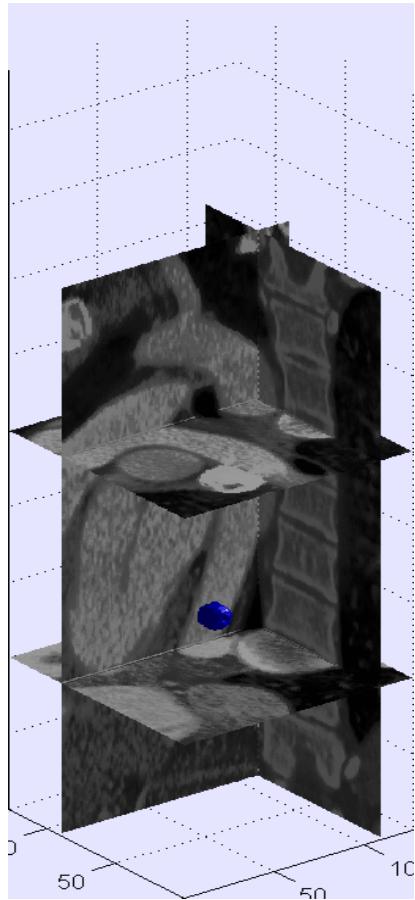
$$0 < p(\vec{x}) = V_s / V < 1$$

Wall normal direction

$$\vec{N} = \frac{\nabla u}{|\nabla u|}$$



# Healthy and Diseased Aortas from CT Images



Z  
X

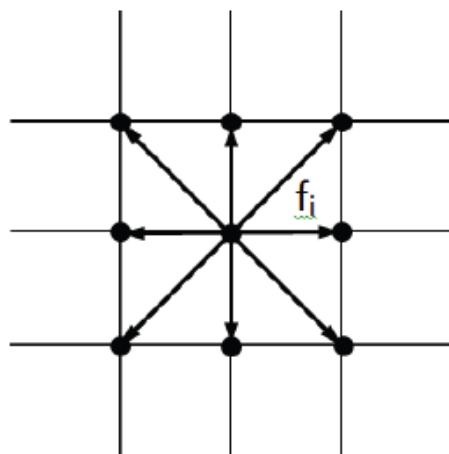
# **Mass-conserved Volumetric LBM**

# Node-based LBM

Time evolution of particle distribution functions

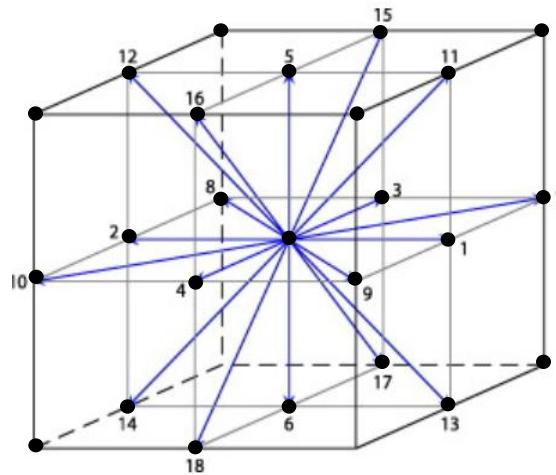
$$f_\alpha(\vec{x} + \vec{e}_\alpha \Delta t, t + \Delta t) = f_\alpha(\vec{x}, t) + \Omega_\alpha(\vec{x}, t)$$

$\alpha=0,1,\dots,8$



D2Q9

$\alpha=0,1,\dots,18$



D3Q19

# Node-based LBM for Curved Boundary

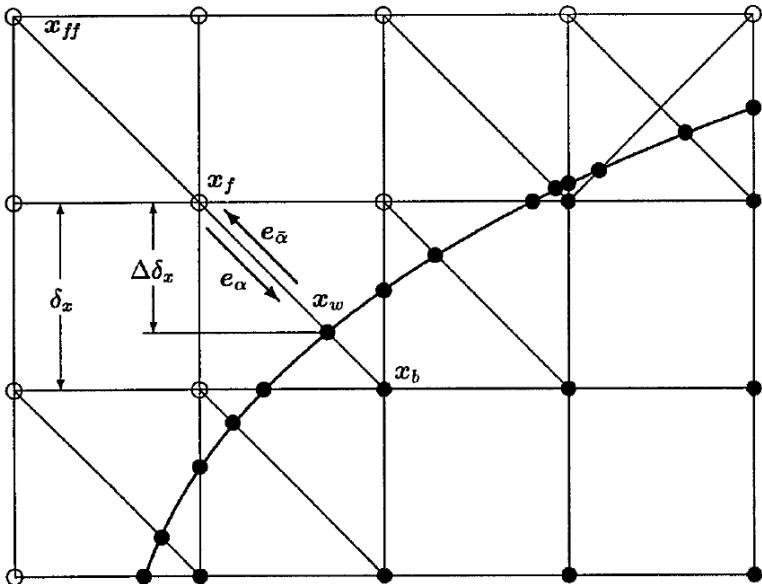


FIG. 2. Layout of the regularly spaced lattices and curved wall boundary. The thick curve marks the boundary location. The solid circles (●) mark the positions where particle-boundary collision occurs. The empty (○) and shaded (●) circles are fluid sites and solid sides, respectively.

R. Mei, L-S Luo, and W. Shyy, NASA/CR-2000-209854, ICASE Report No. 2000-6

## Bases of schemes:

1. Point-wise particle distribution interpolation
2. particle distribution transformation into local curve-linear coordinate system

Main drawback: mass conservation of fluid not insured.

— May not reliable/plasticla for arbitrary moving boundaries

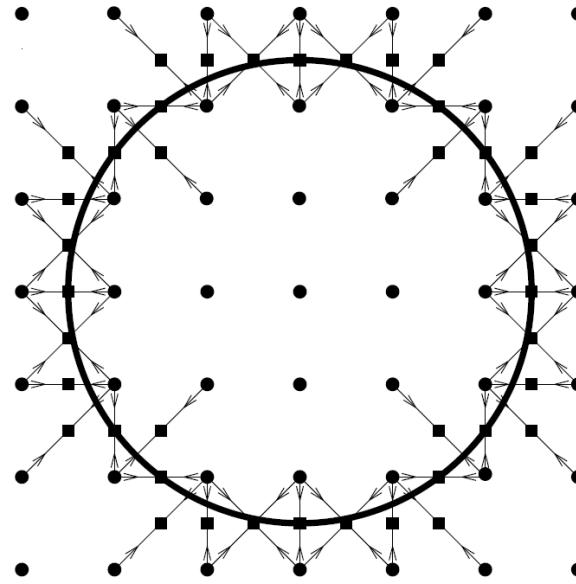


FIGURE 2. Location of the boundary nodes for a circular object of radius 2.5 lattice spacings. The velocities along links cutting the boundary surface are indicated by arrows. The location of the boundary nodes are shown by solid squares and the lattice nodes by solid circles.

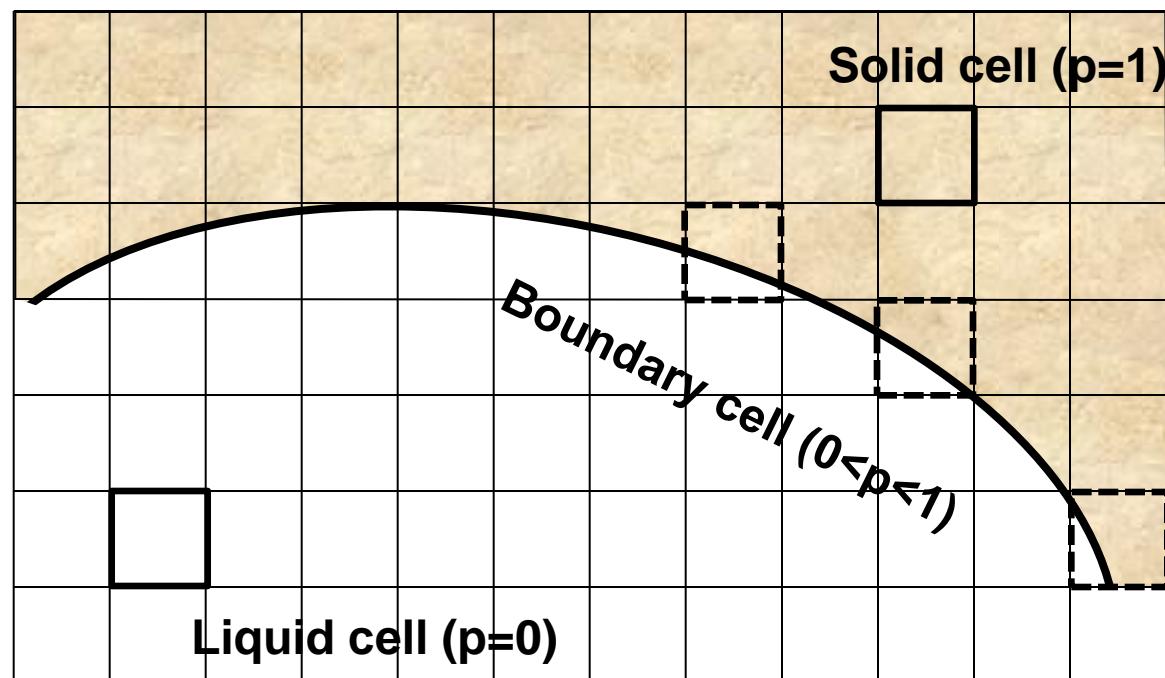
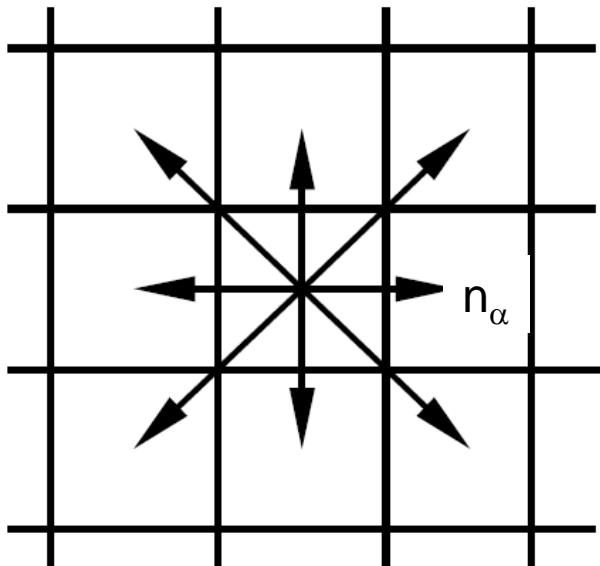
A. J. C. Ladd, JFM, 1994

# Volumetric Representation

$$p(\vec{x}, t) = \frac{\Delta v_s(\vec{x}, t)}{\Delta V}$$

$$\Delta V = \Delta V_s + \Delta V_f$$

$$n_\alpha = f_\alpha \Delta V_f$$



When  $\Delta V_s=0$ ,  $\Delta V_f=\Delta V$ , volumetric representation recovers node-based description

# Volumetric Lattice Boltzmann Equations

Time evolution of particle population

$$n_\alpha(\vec{x} + \vec{e}_\alpha \Delta t, t + \Delta t) = n_\alpha(\vec{x}, t) + \Omega_\alpha(\vec{x}, t)$$

$$\alpha = 0, 1, \dots, 8$$

$$N = \sum_{\alpha} n_{\alpha}$$

$$\bar{u}(\vec{x}, t) = \frac{\sum_{\alpha} \vec{e}_{\alpha} n_{\alpha}}{N}$$

$$\rho(\vec{x}, t) = \frac{N}{(1-p)\Delta V}$$

**Particle population evolution consists of**

- **Collision**

Momentum exchange between solid and fluid accounted

- **Streaming**

Volumetric bounce-back included

- **Boundary induced particle migration**

Mass conservation of fluid guaranteed

# Collision

$$\Omega_\alpha(\vec{x}, t) = -\frac{1}{\tau} [n_\alpha(\vec{x}, t) - n_\alpha^{\text{eq}}(\vec{x}, t)] \quad \tau = \frac{1}{2} + \frac{3v}{c^2 \delta t}$$

$$n_\alpha^{\text{eq}}(\vec{x}, t) = N w_\alpha \left[ 1 + \frac{3(\vec{e}_\alpha \cdot \vec{U})}{2c^2} + \frac{9(\vec{e}_\alpha \cdot \vec{U})^2}{2c^4} - \frac{3U^2}{2c^2} \right] \quad \vec{U} = \vec{u} + \delta \vec{u}$$

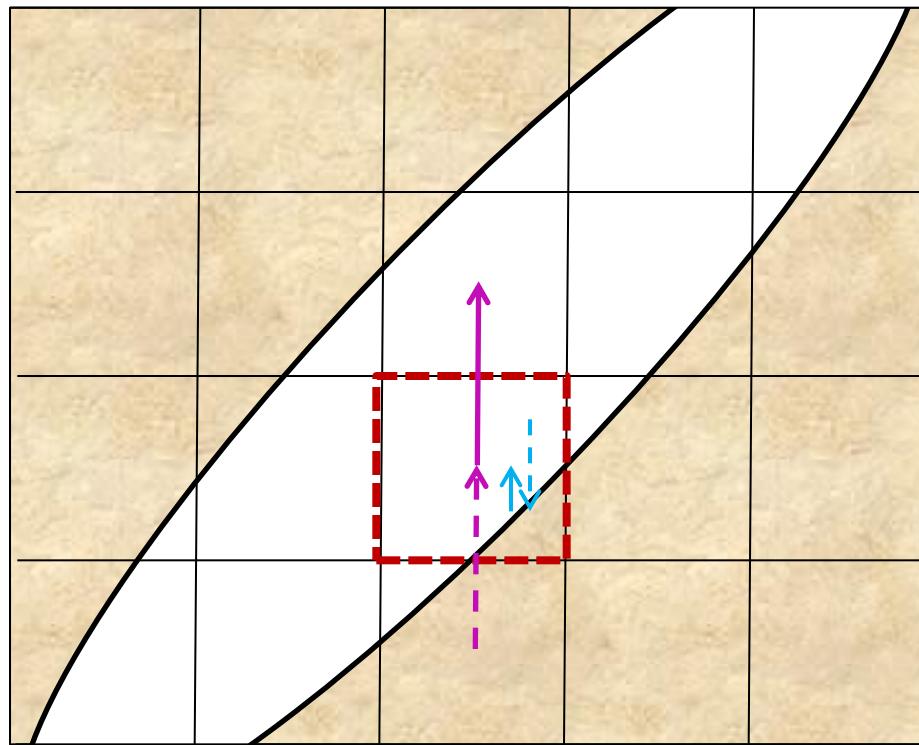
$$\delta \vec{u}(\vec{x}, t) = \tau p(\vec{x}, t) \vec{u}_b(\vec{x}, t) + \frac{\tau}{N(\vec{x}, t)} \sum_{\beta=1}^8 p(\vec{x} + \vec{e}_\beta, t) n_\beta(\vec{x}, t) \vec{u}_b(\vec{x} + \vec{e}_\beta, t)$$

1. Reflecting momentum change due to boundary movement ( $\vec{u}_b \neq 0$ )
2. Only for boundary cells and their neighboring fluid cells
3. Satisfying mass conservation in boundary cells

# Streaming

## (Generalized bounce-back condition)

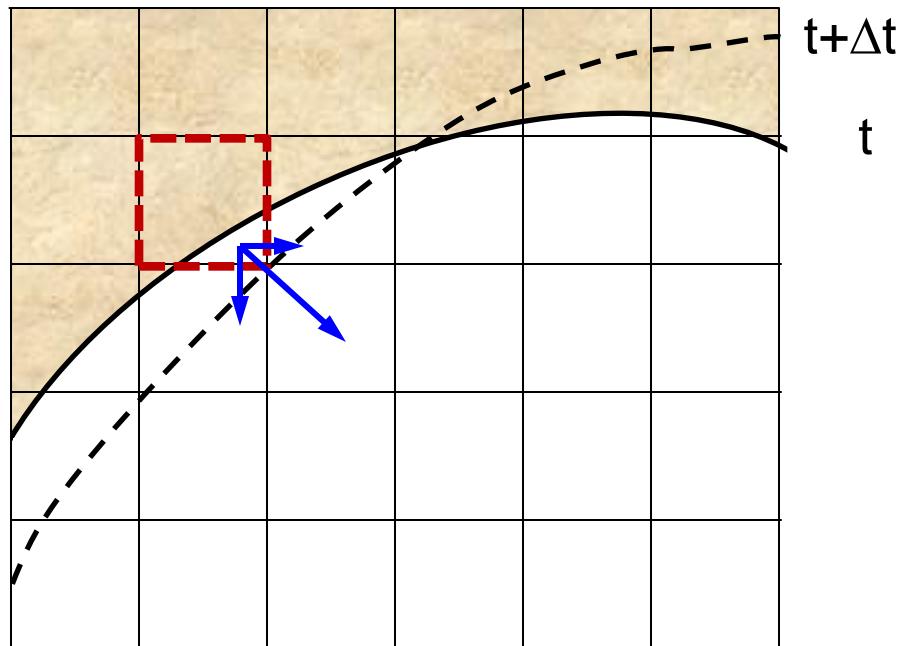
$$n''_{\alpha}(\vec{x}, t + \Delta t) = [1 - p(\vec{x}, t + \Delta t)]n'_{\alpha}(\vec{x} - \vec{e}_{\alpha}\Delta t, t) \leftarrow \text{Upwind streaming}$$
$$+ p(\vec{x} + \vec{e}_{\alpha^*}, t + \Delta t)n'_{\alpha^*}(\vec{x}, t) \leftarrow \text{Downwind bounce-back}$$



# Boundary-induced Particle Migration

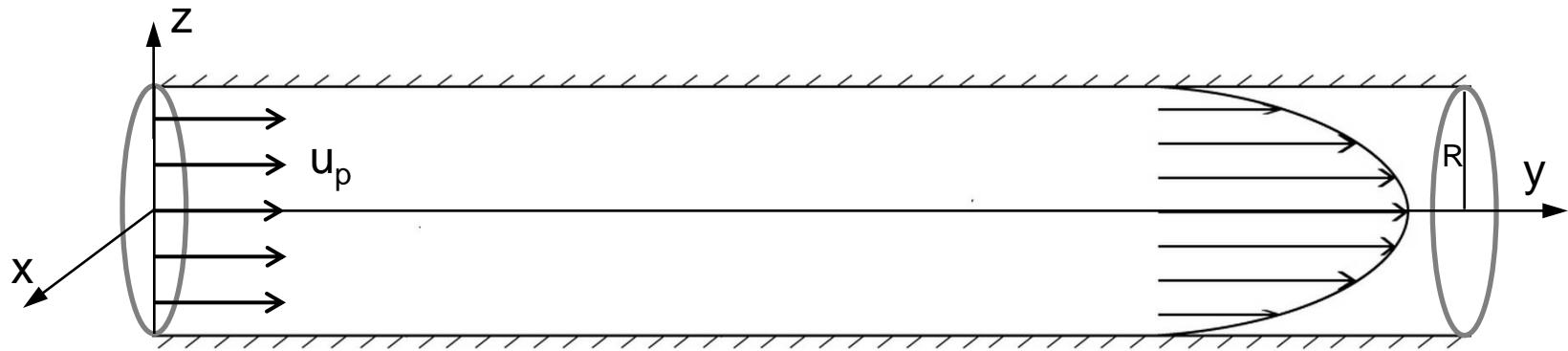
## (mass conservation)

$$n_{\alpha}(\vec{x}, t + \Delta t) = [1 - p(\vec{x}, t + \Delta t)] n''_{\alpha}(\vec{x}, t + \Delta t) + \sum_{\beta=1}^b \tilde{n}_{\alpha,\beta}(\vec{x} - \vec{e}_{\alpha} \Delta t, t + \Delta t)$$



$$\tilde{n}_{\alpha,\beta}(\vec{x}, t + \Delta t) = p(\vec{x}, t + \Delta t) n''_{\alpha}(\vec{x}, t + \Delta t) \frac{[1 - p(\vec{x} + \vec{e}_{\beta} \Delta t, t + \Delta t)] n_{\beta}(\vec{x}, t)}{\sum_{k=1}^8 [1 - p(\vec{x} + \vec{e}_k \Delta t, t + \Delta t)] n_k(\vec{x}, t)}$$

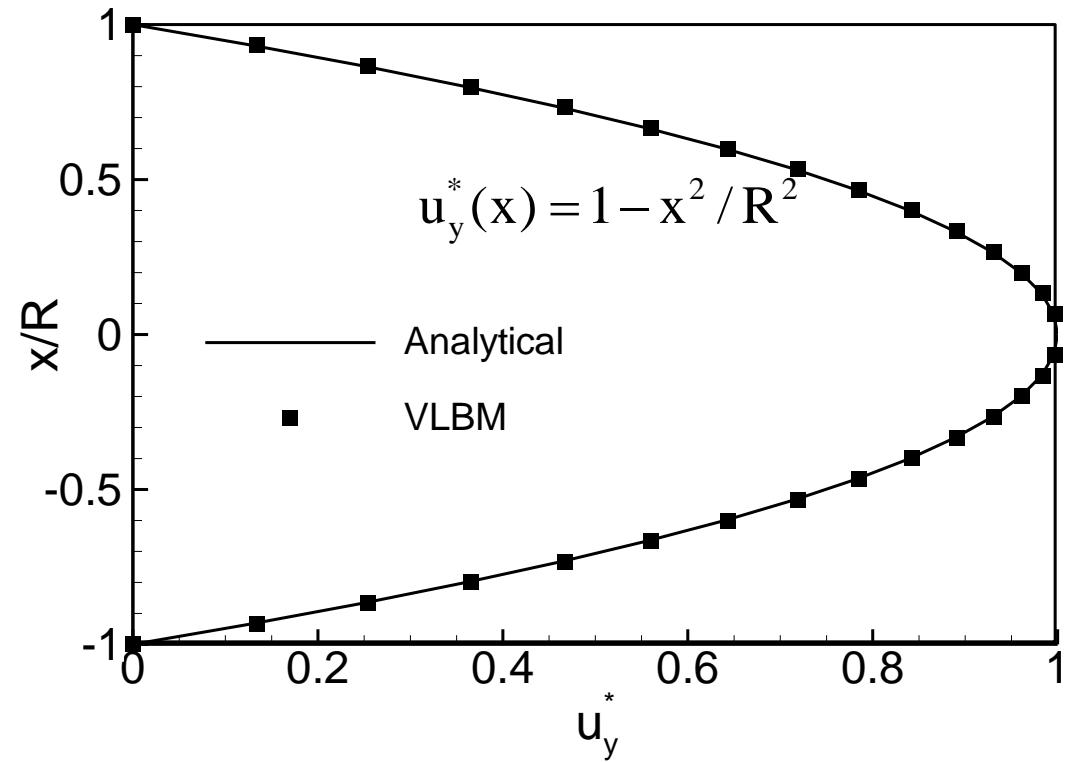
# Steady Pipe Flow



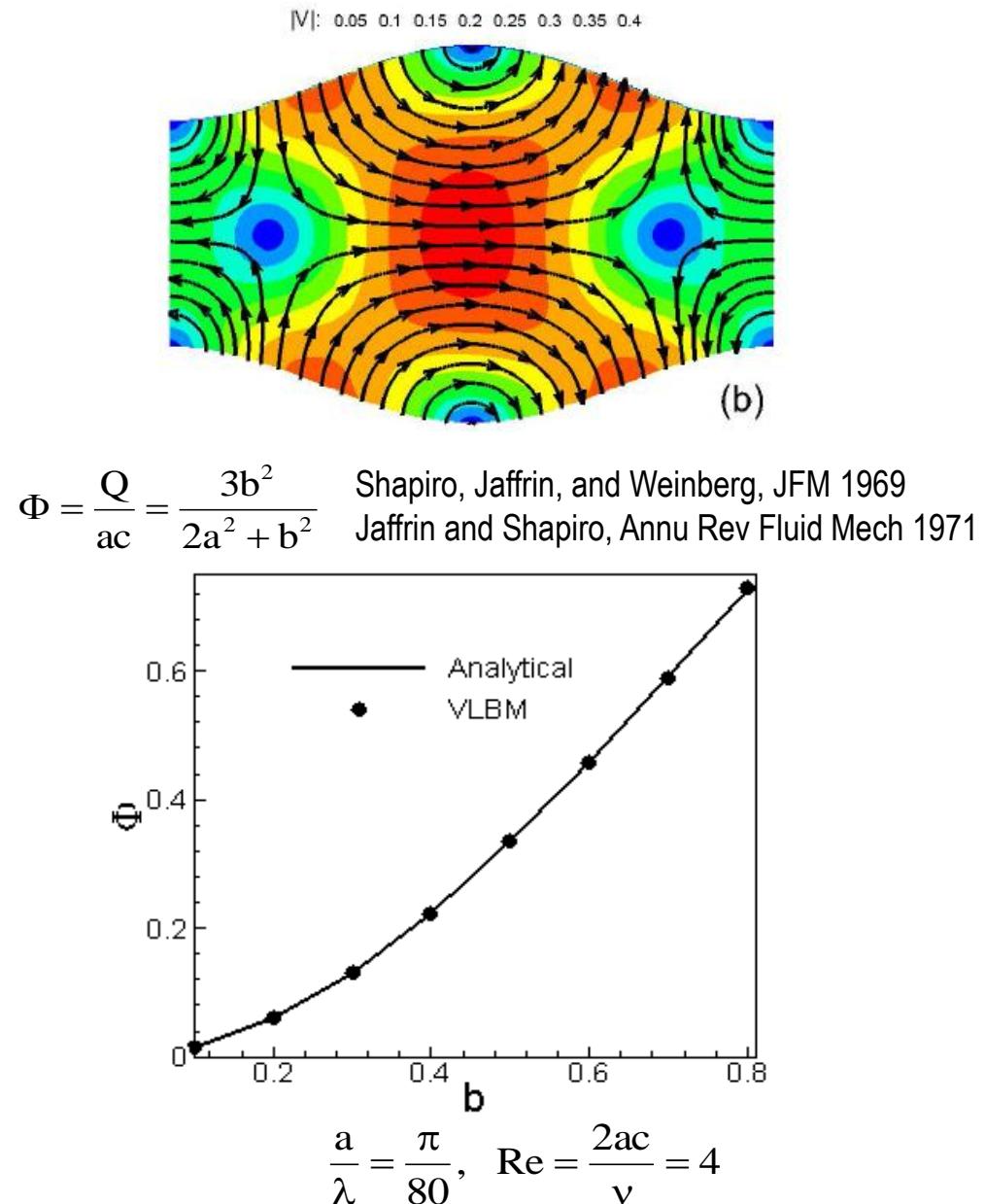
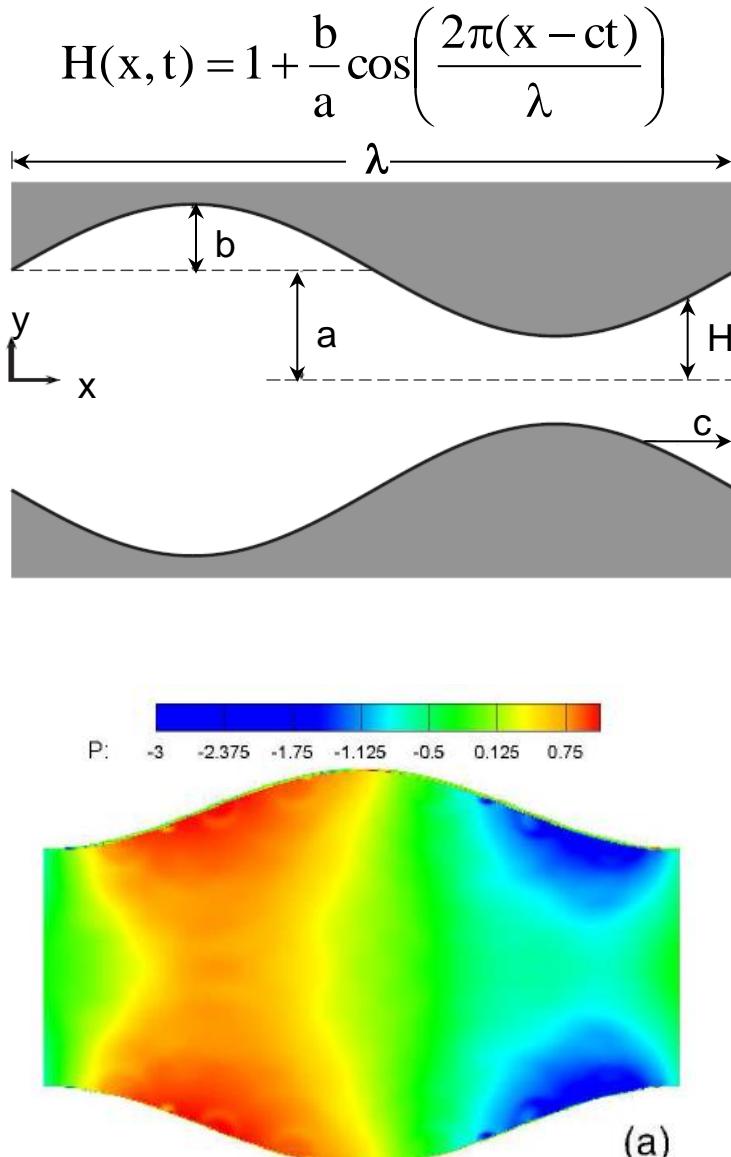
$$\frac{\partial^2 u_y}{\partial x^2} + \frac{\partial^2 u_y}{\partial z^2} = -\frac{1}{\mu} \frac{dp}{dy}$$

$$u_y(x, z) = 2u_p \left( 1 - \frac{x^2 + z^2}{R^2} \right)$$

$$u_p = \frac{1}{8R^2} \left( \frac{1}{\mu} \frac{dp}{dy} \right)$$



# Peristaltic Flow

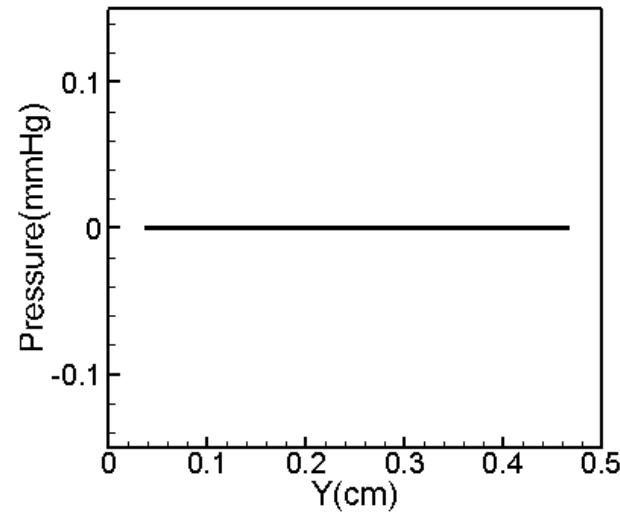
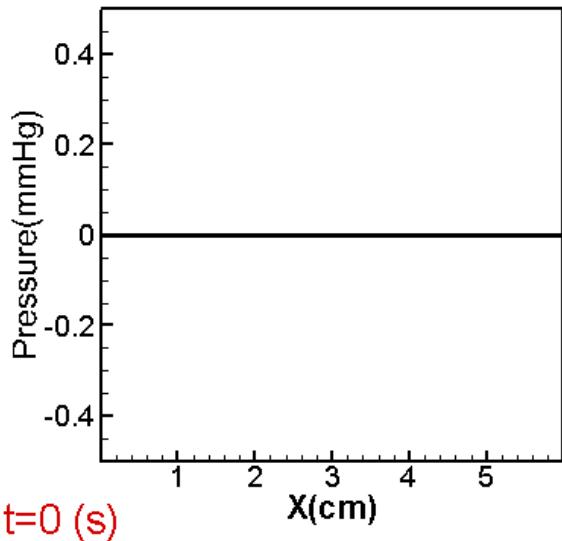
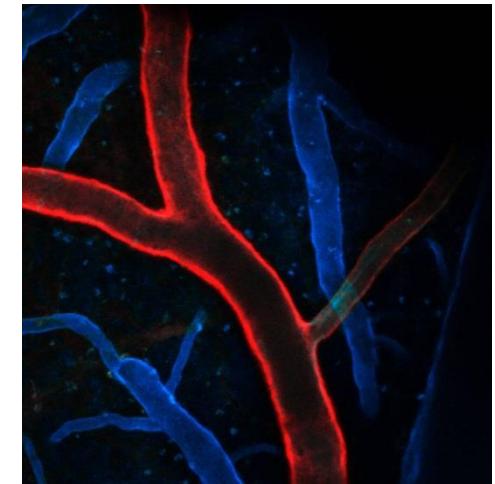
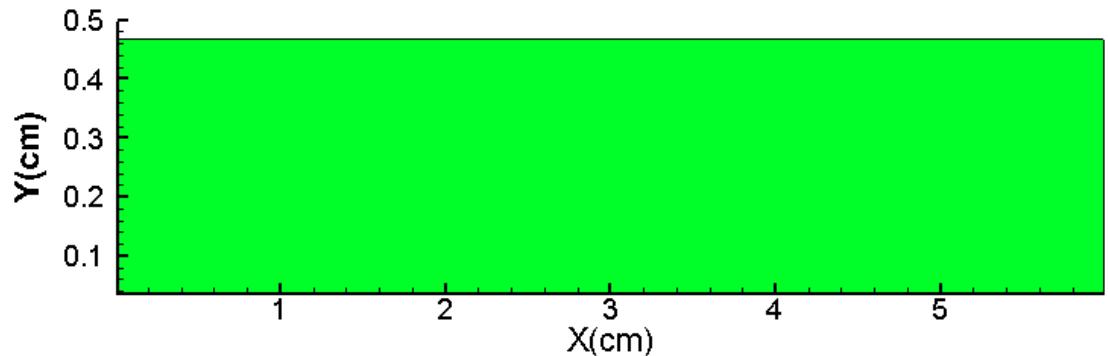


# Artery Wall Motility

Artery walls in the brain



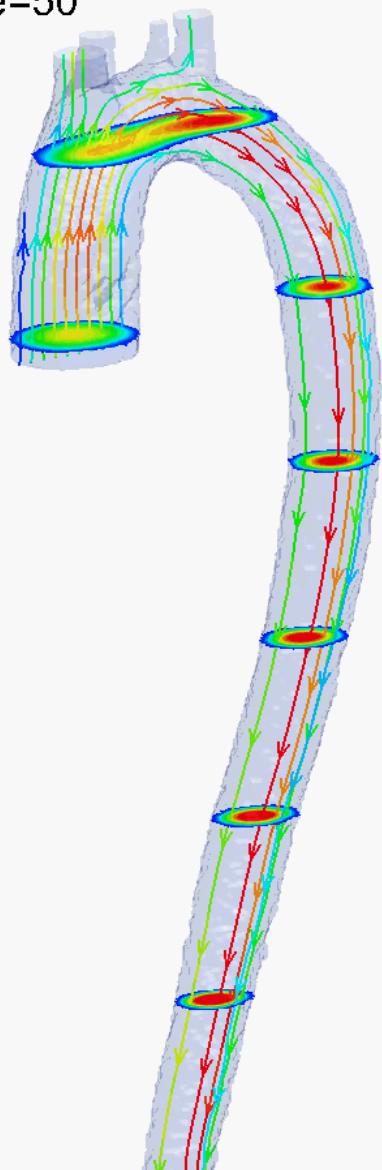
Pressure(mmHg): -0.1 -0.08 -0.06 -0.04 -0.02 0 0.02 0.04 0.06 0.08 0.1



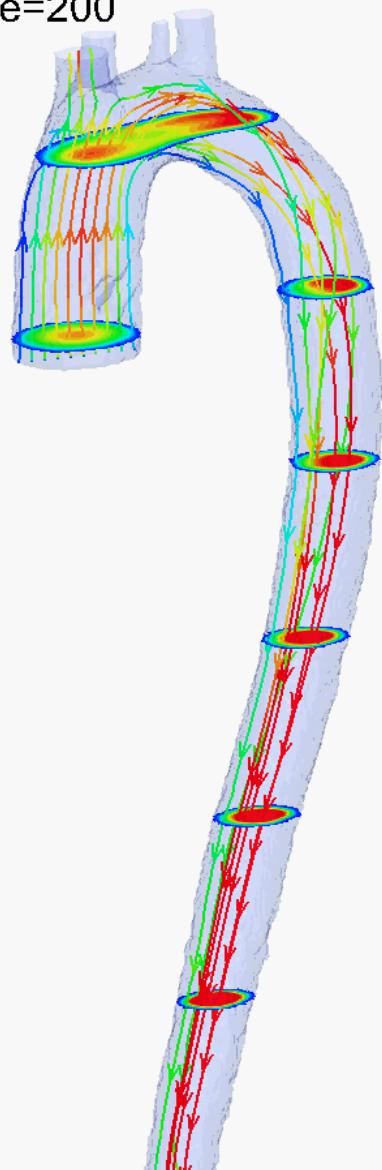
# **Preliminary Results of Hemodynamics in Healthy and Diseased Aortas**

# Healthy, Streamlines

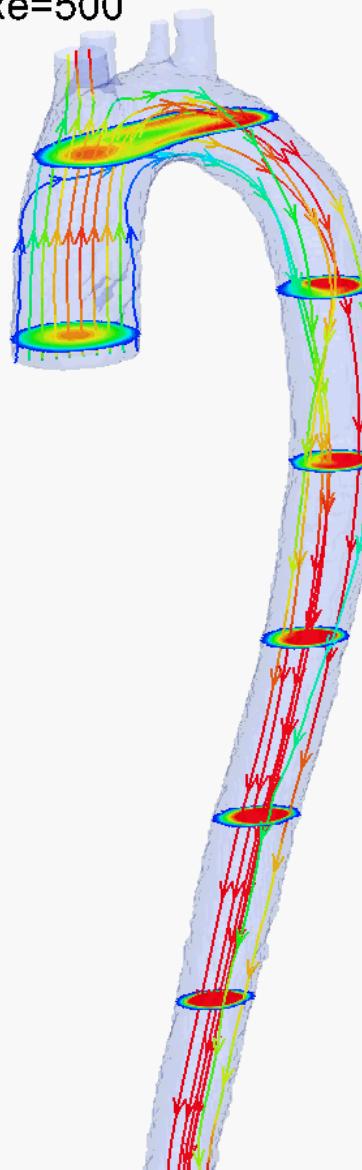
Re=50



Re=200

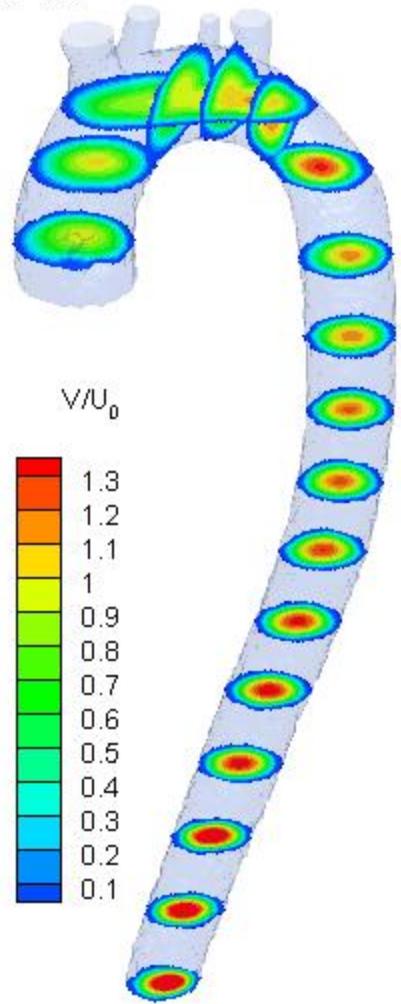


Re=500

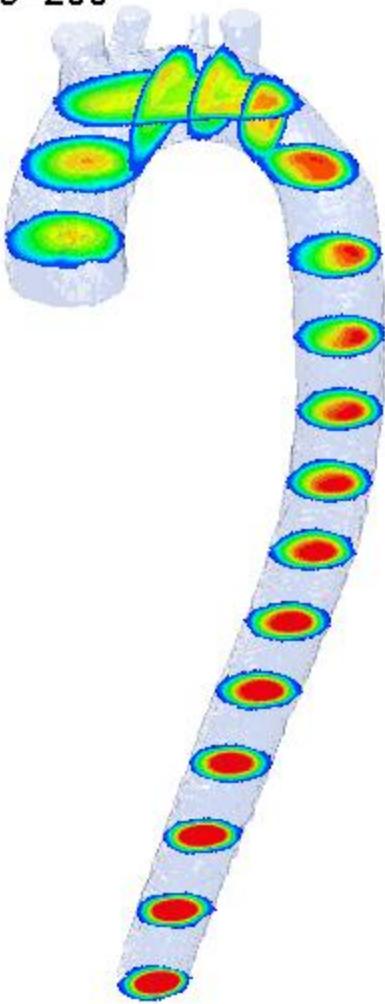


# Healthy Velocity

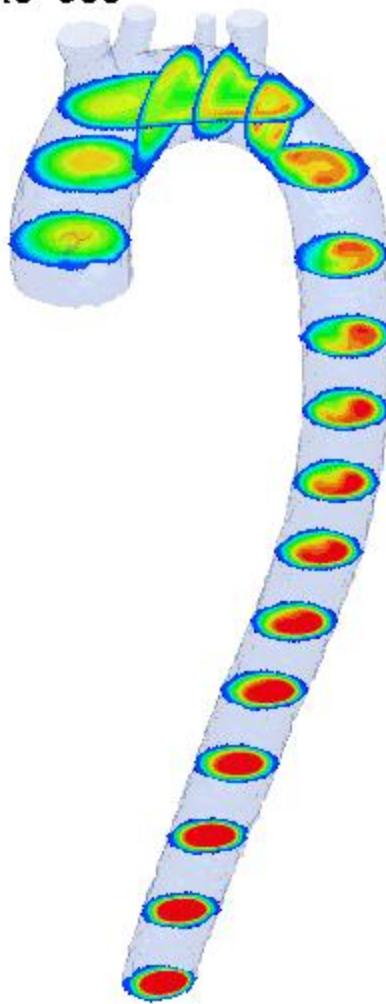
Re=50



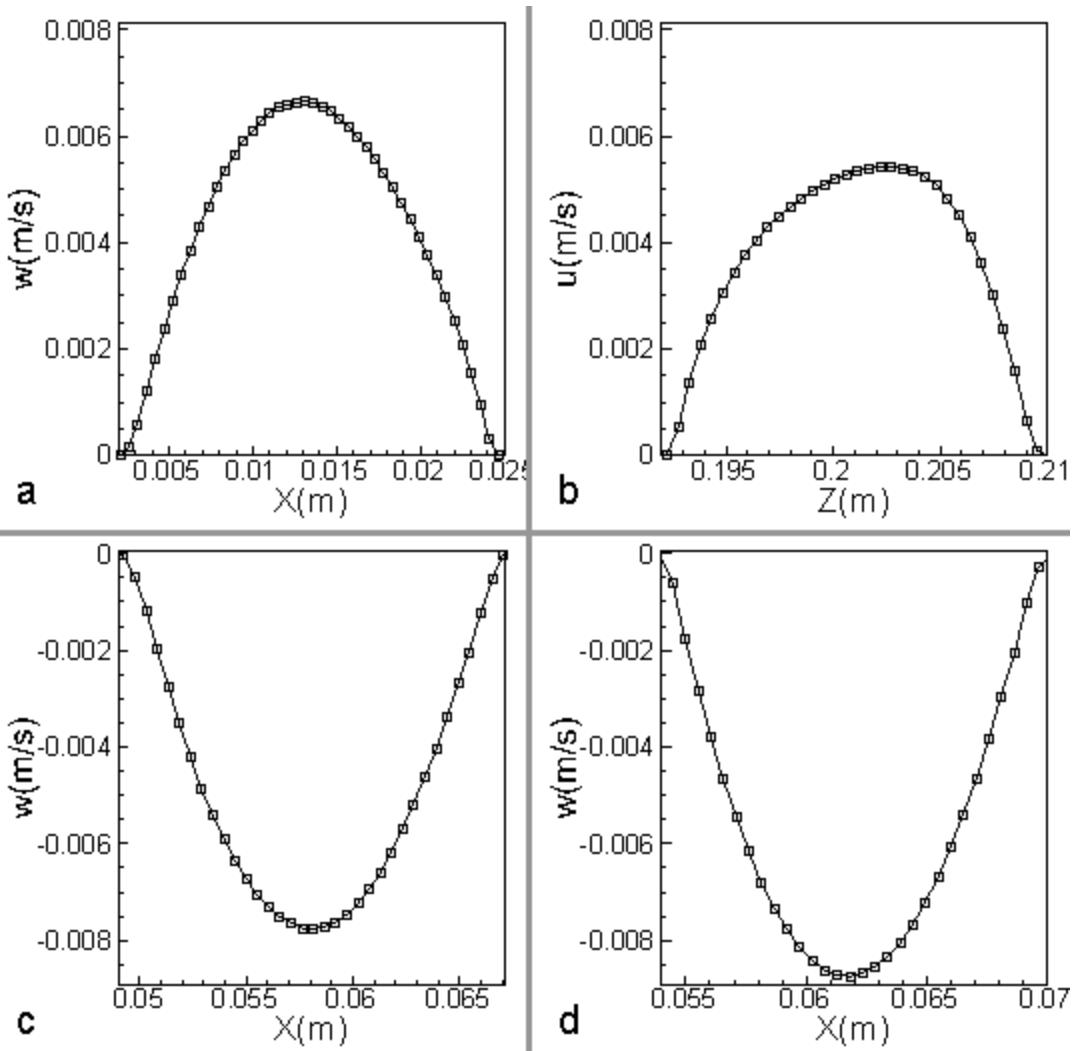
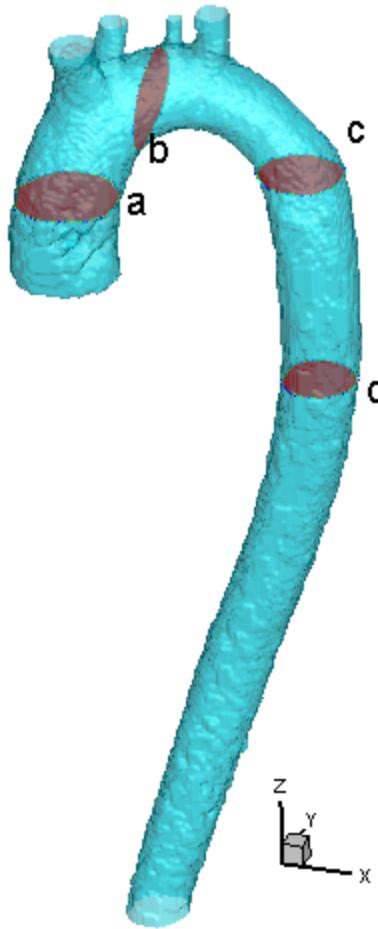
Re=200



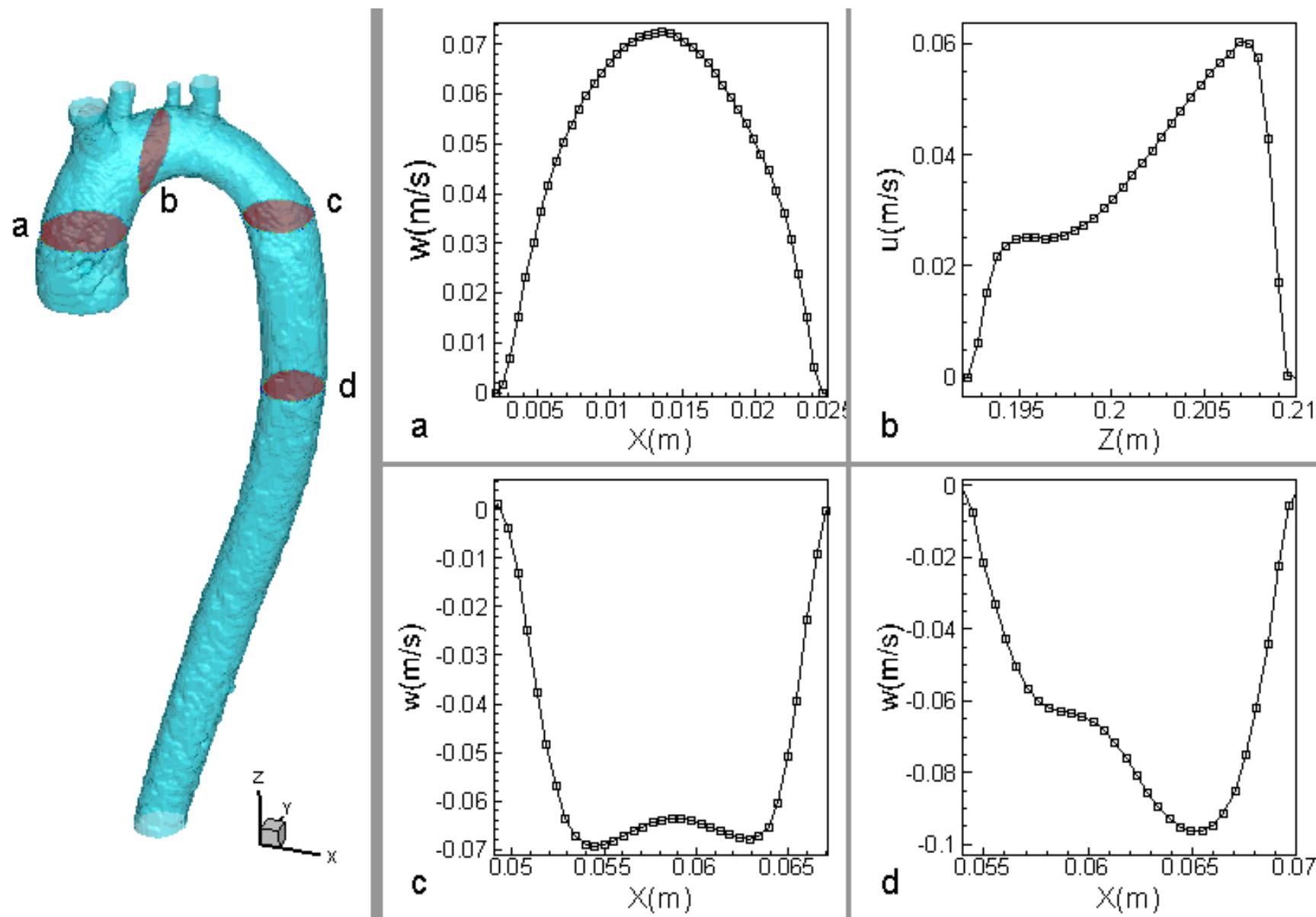
Re=500



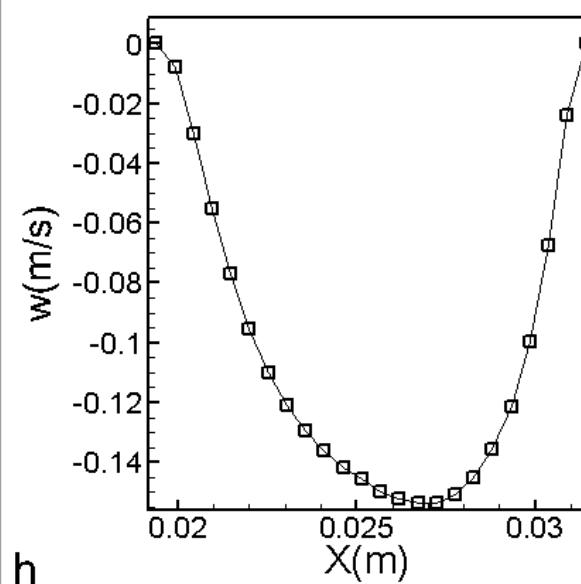
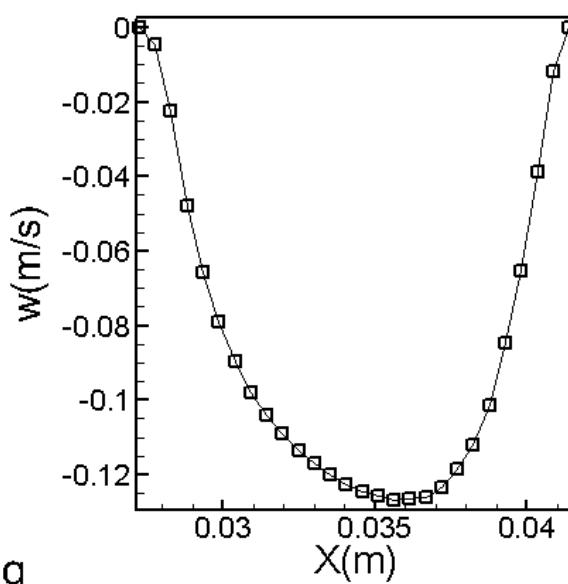
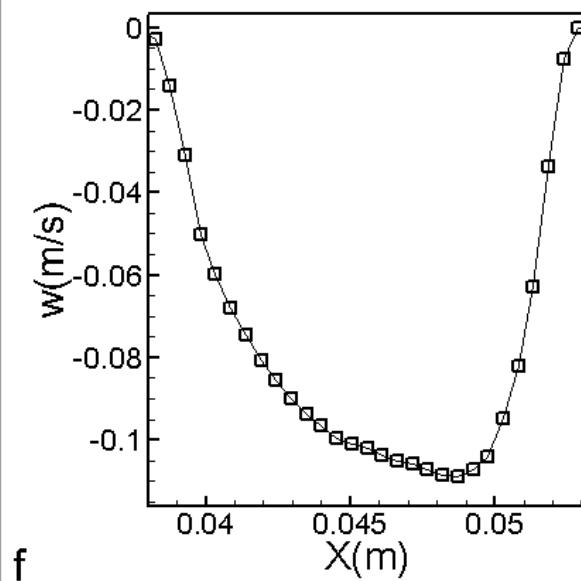
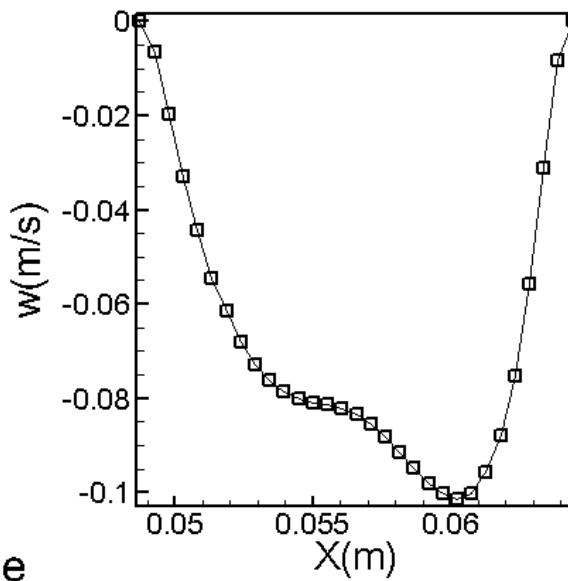
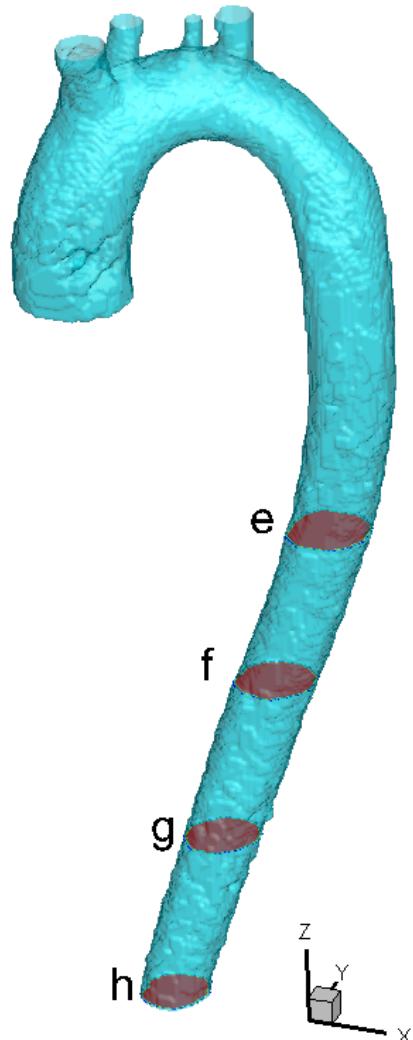
# Healthy Velocity , Re=50



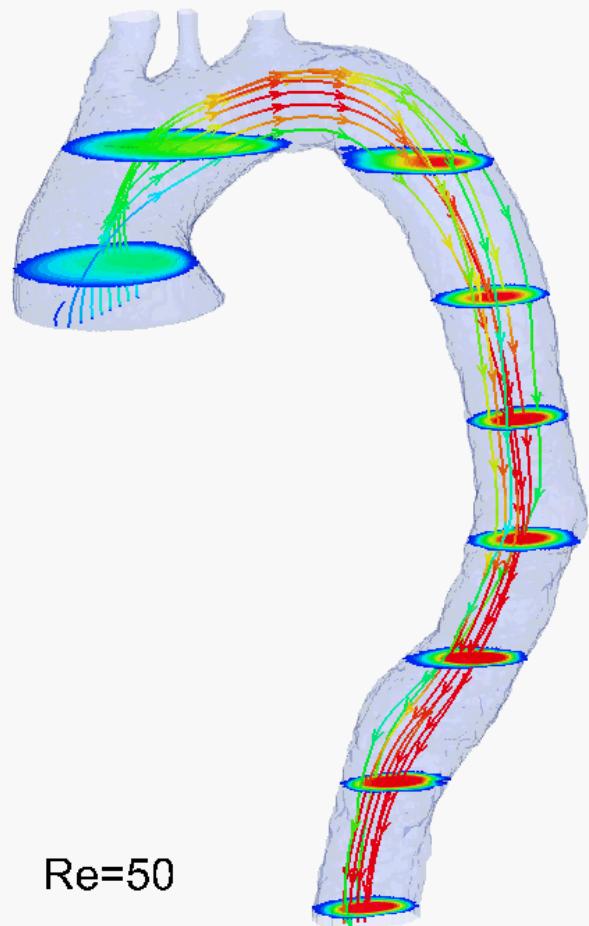
# Healthy Velocity, Re=500



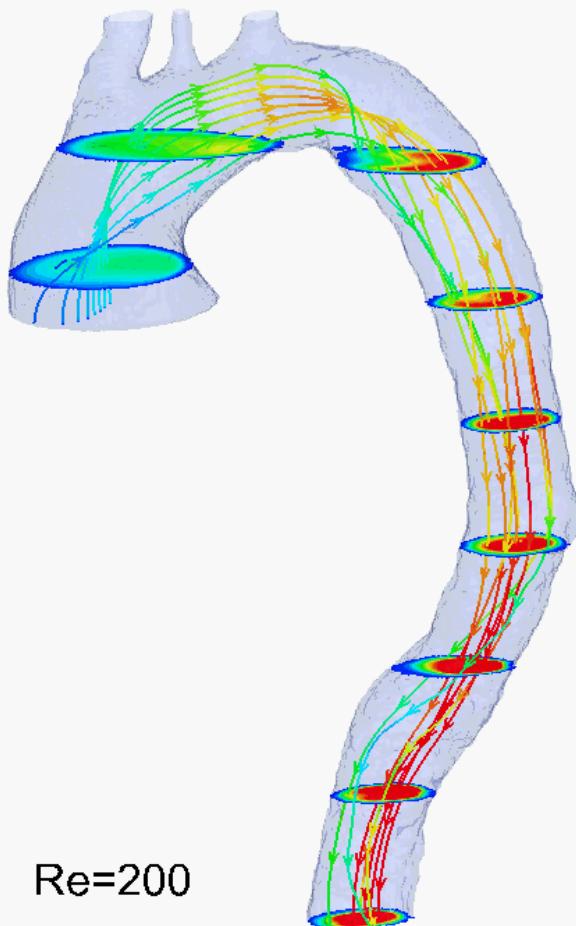
# Healthy Velocity, Re=500, cont'd



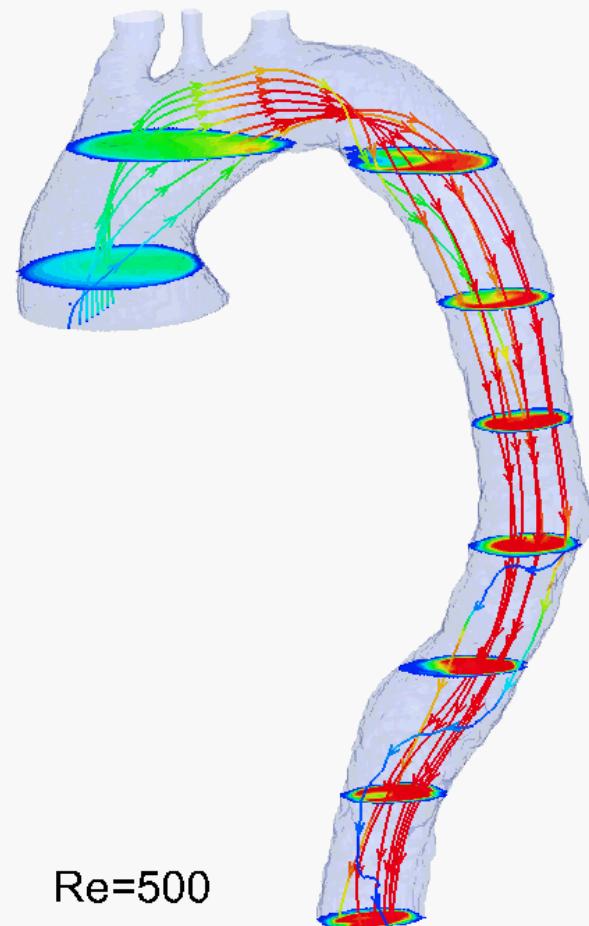
# Dilated, Streamlines



Re=50

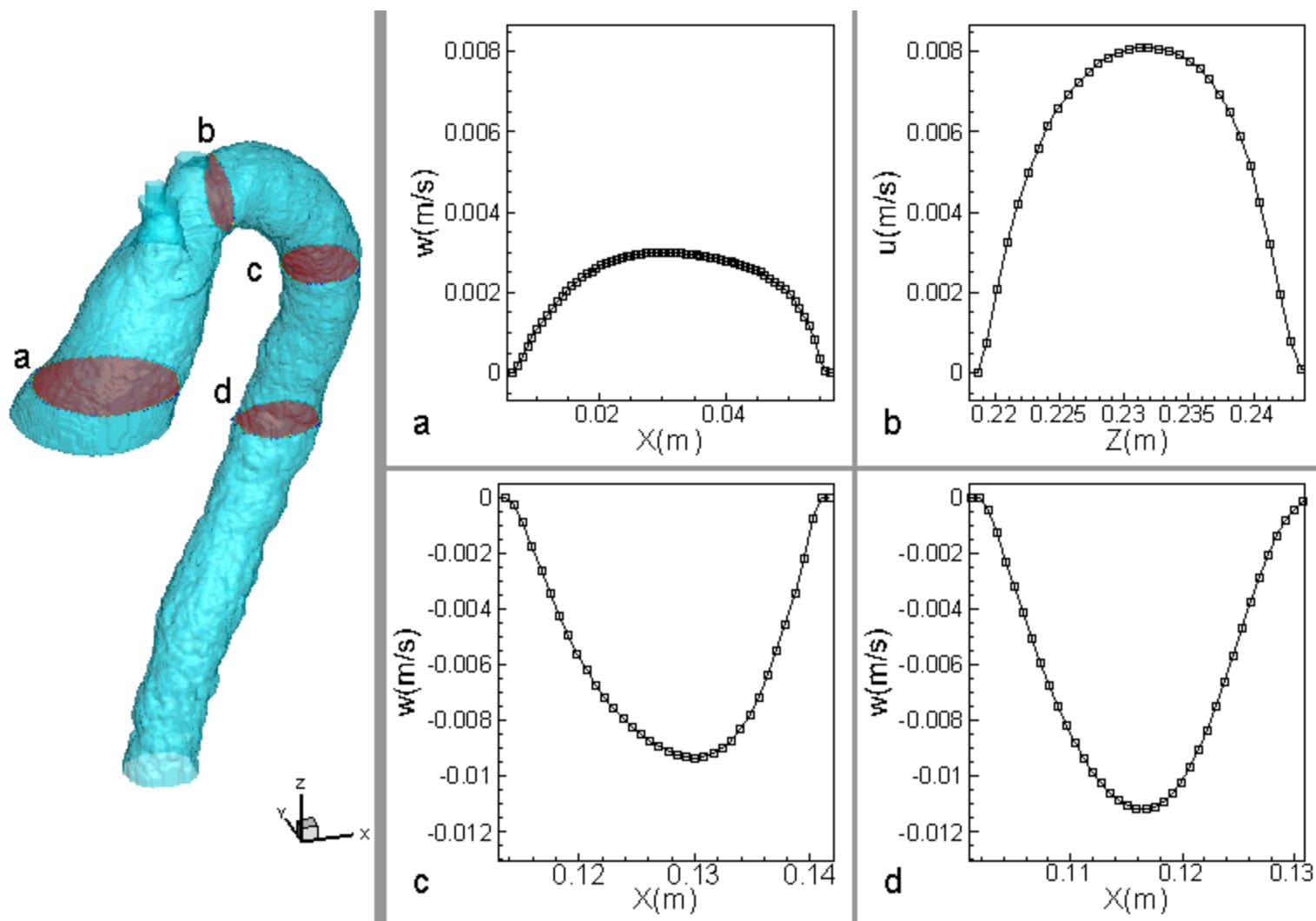


Re=200

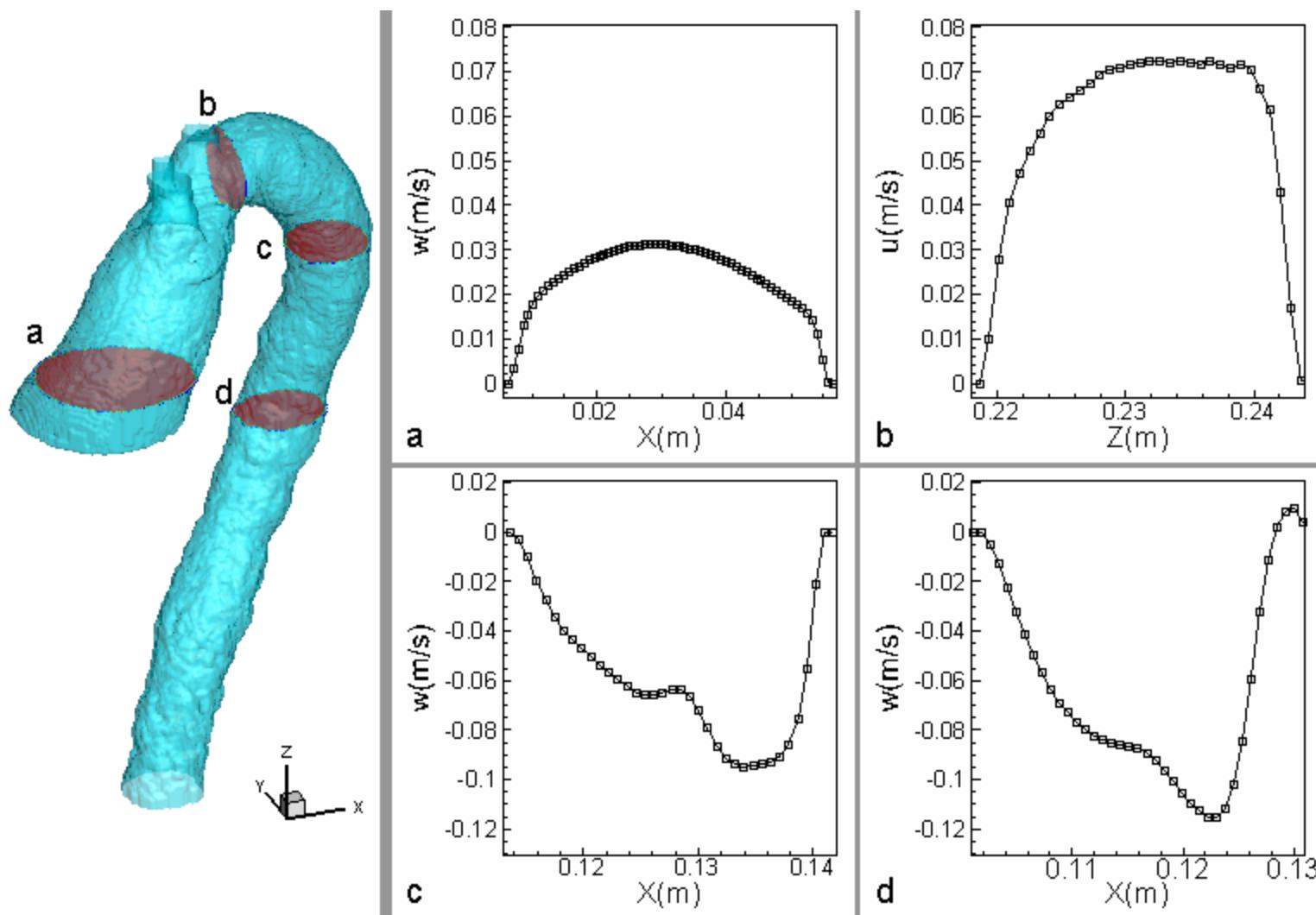


Re=500

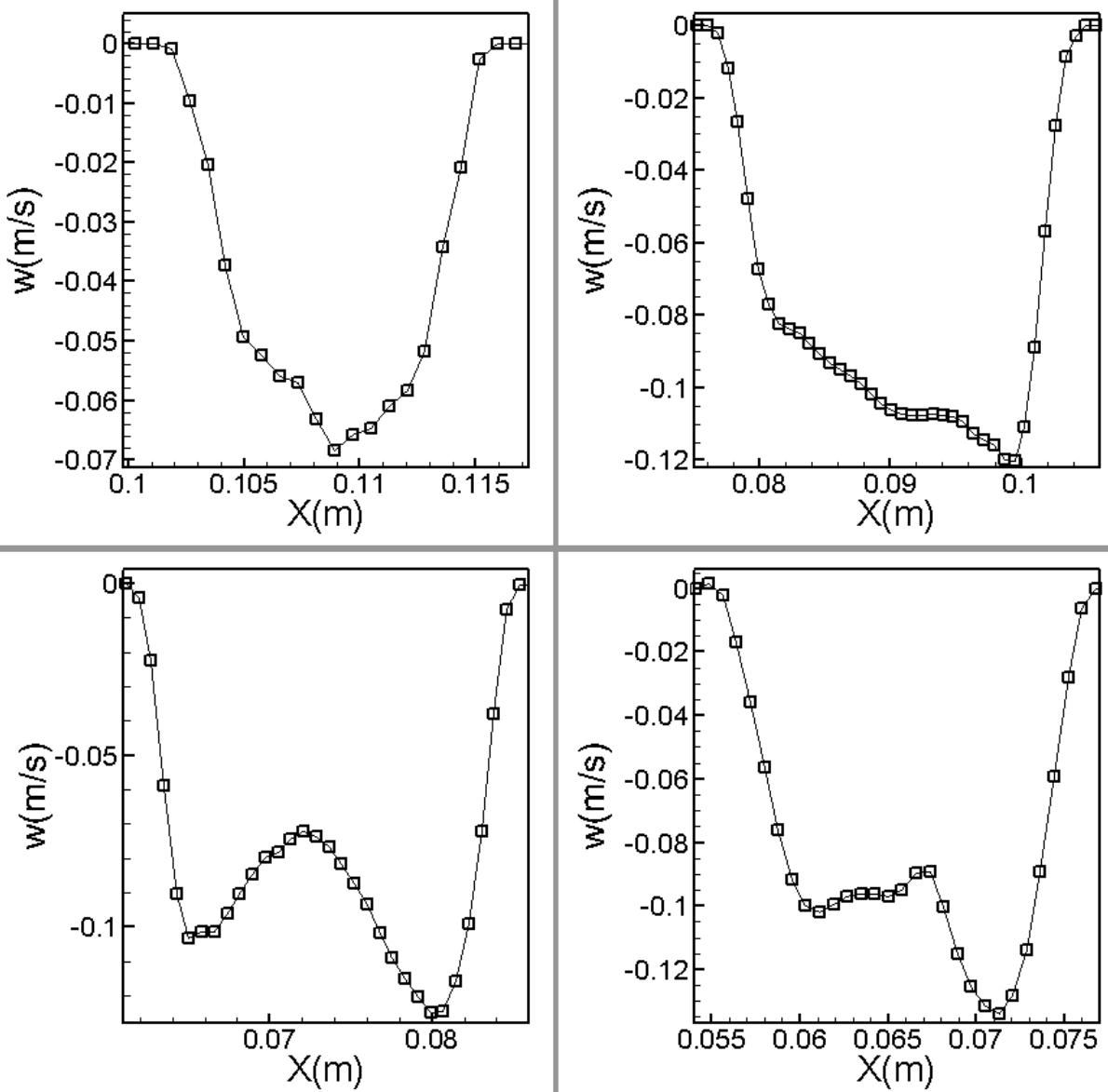
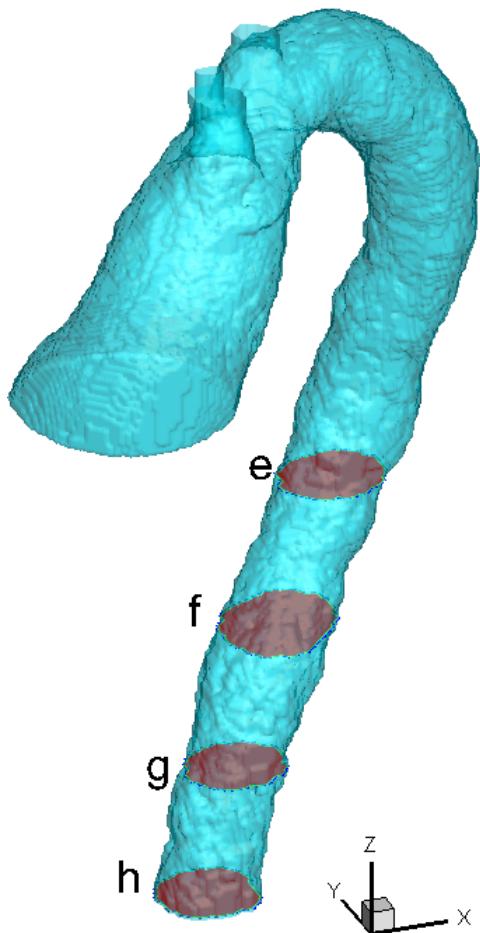
# Dilated Velocity, Re=50



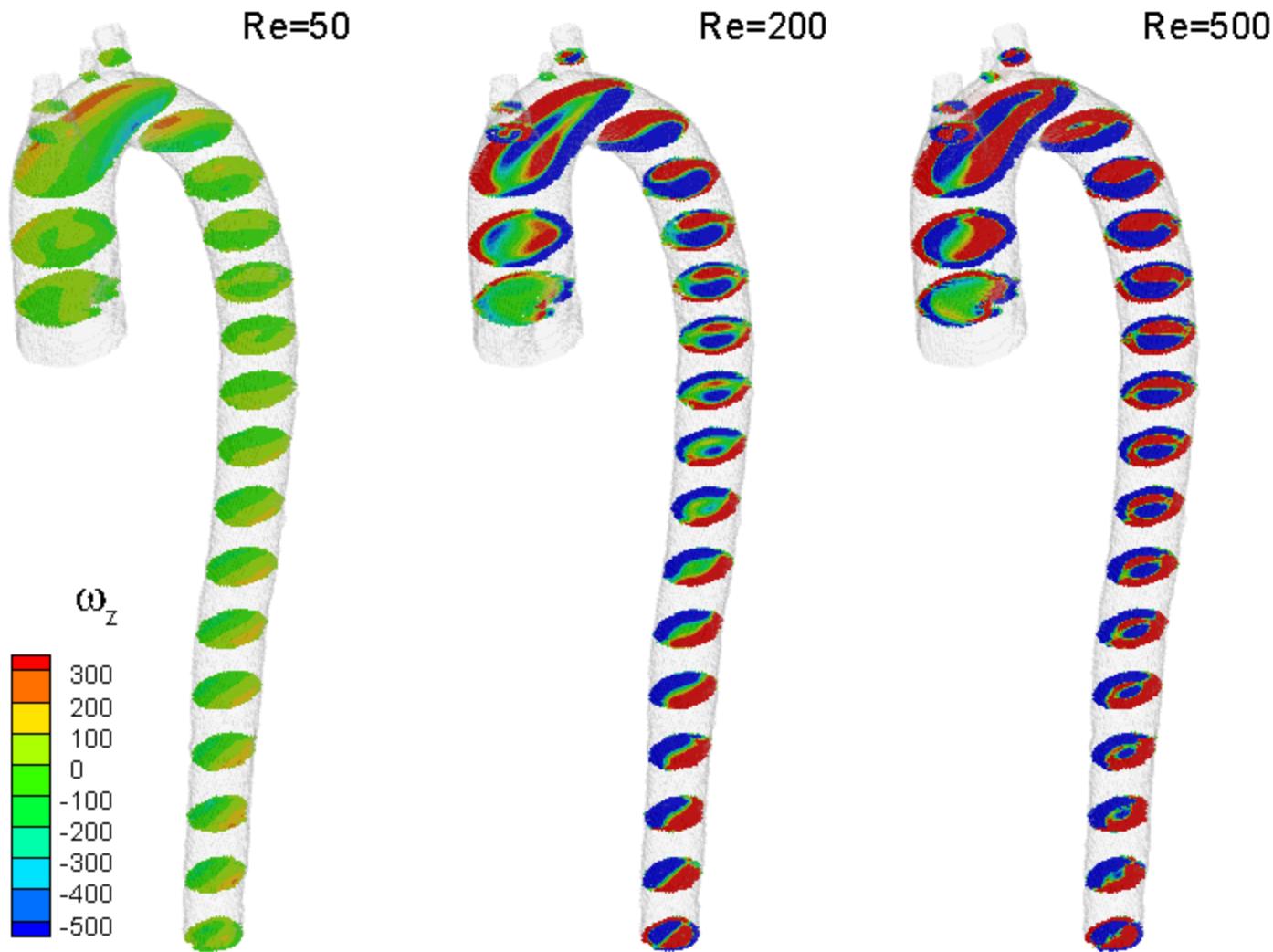
# Dilated Velocity, Re=500



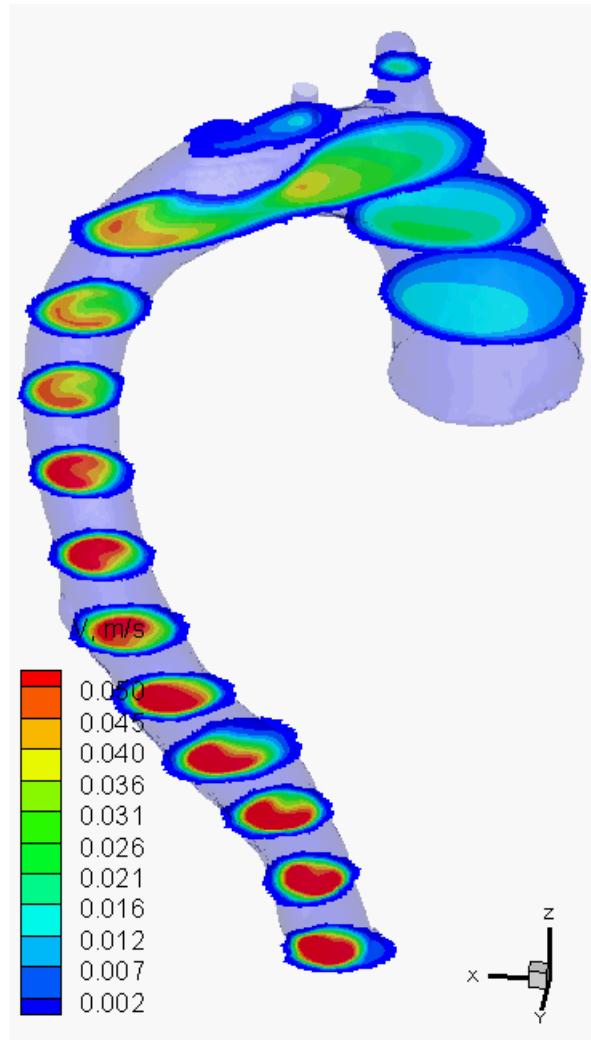
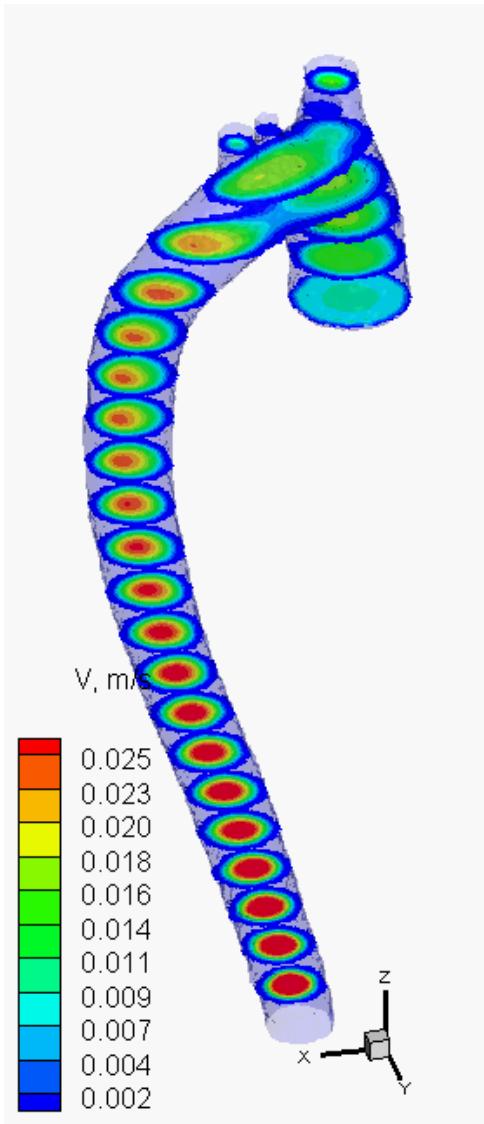
# Dilated Velocity, Re=500, cont'd



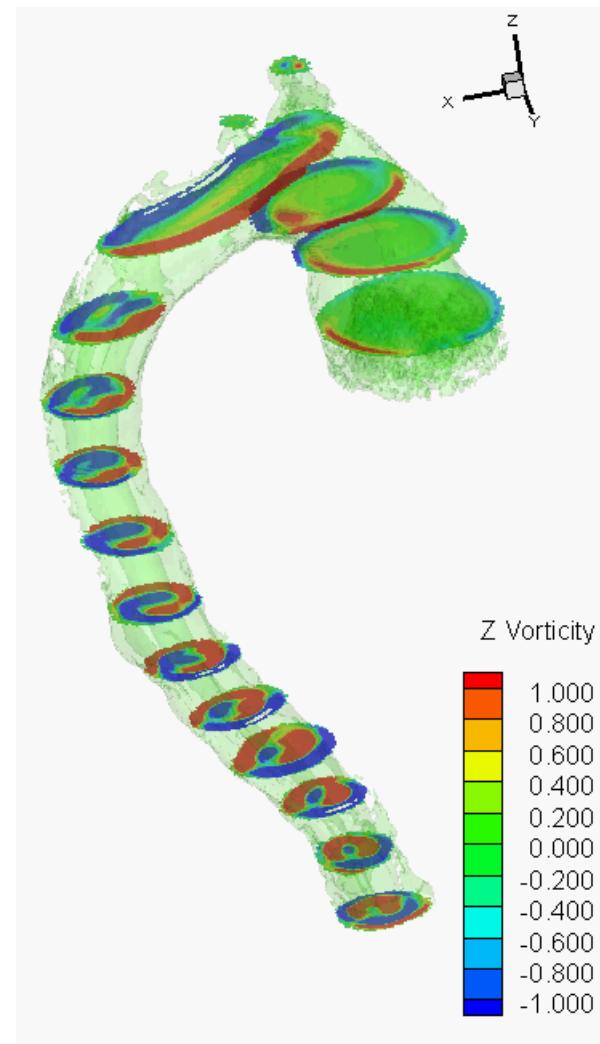
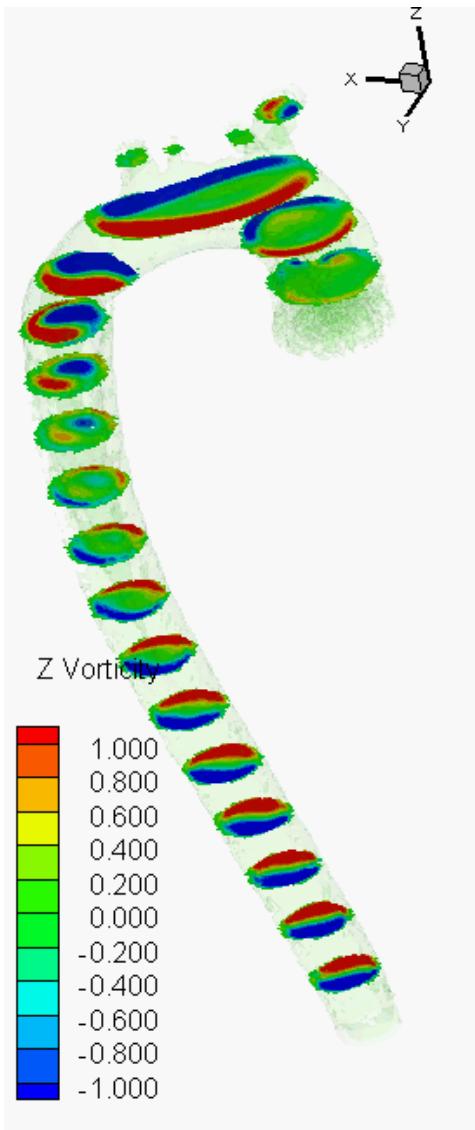
# Healthy, Vorticity



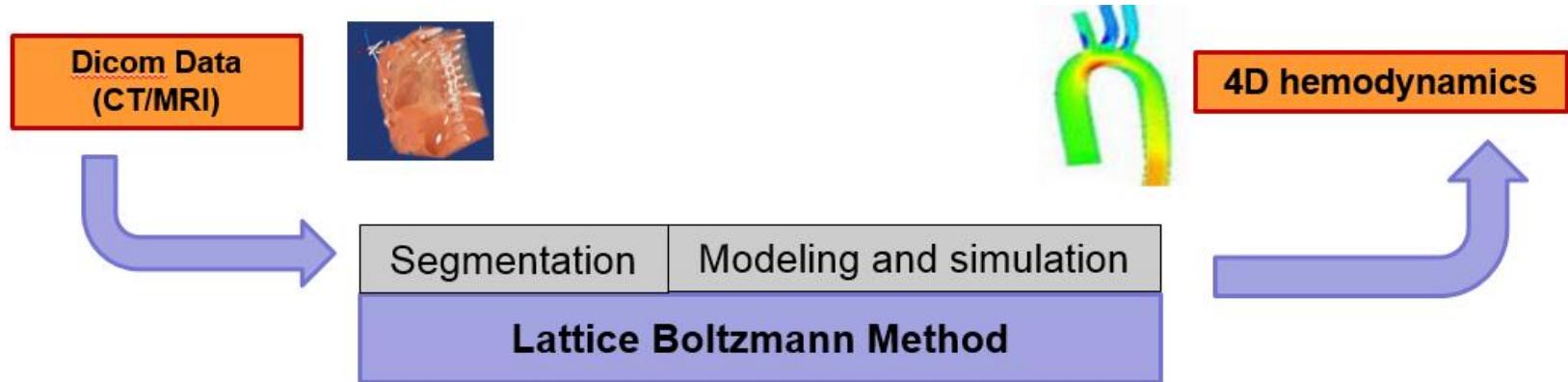
# Healthy vs. Dialyzed, Velocity



# Healthy vs. Dilated Vorticity



# Take-Home Messages



## Unified computation platform

1. Good for patient-specific flows in human organs
  - Cardiovascular blood flow in coronary, aorta, carotid --- heart attack, stroke
  - Peristalsis in stomach, esophagus, urine --- cancers
2. Pulsatility --- Laminar, transitional, turbulence
3. Non-Newtonian --- multiphase
4. GPU parallel computation

## Medical focus

1. Patient-specific hemodynamics in carotid artery --- Hemodynamic indicators to distinguish symptomatic and asymptomatic carotid stenosis to stroke
2. Supplemental device to CT/MRI to reveal real-time hemodynamics in diseased human organs.